DESIGN, CONSTRUCTION AND TESTING OF A COMPUTERIZED IGNITION CIRCUIT FOR AN INTERNAL COMBUSTION ENGINE

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Approval of the thesis

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ABSTRACT

DESIGN, CONSTRUCTION AND TESTING OF A COMPUTERIZED IGNITION CIRCUIT FOR AN INTERNAL COMBUSTION ENGINE

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In this study, an ignition unit was designed and constructed for a new design engine with eight cylinders and sixteen pistons. The ignition coils with two high voltage outputs were used to ignite sixteen spark plugs on the system. They were driven by PIC16F628A based igniter circuits triggered with digital signals. The igniter circuits receive ignition signals in a square wave form from a main control circuit; they open or close primary voltage of the induction coils to ignite spark plugs. This main control circuit is based on PIC16F877A; and there are two of them. The duty of main control circuit is to determine ignition advance according to engine speed and cooling water temperature, and send proper ignition signals to the igniter circuits. This main control circuit receives engine speed from the other main circuit (secondary control circuit) with serial communication and reads cooling water temperature and then it reads advance value from external eeprom memory according to engine speed and temperature. The main control circuit receives cylinder position signals from the secondary control circuit and adds advance value on them to form ignition timing signals which triggers igniter circuits. The secondary control circuit reads engine speed and determines cylinder positions with two magnetic pick-ups and LM2907 circuits on a gear wheel. This gear wheel was used to

simulate disks on the crank shaft of the cars, and driven with an electric motor. The ignition unit was tested for different engine speeds, and its proper working was proved.

Keywords: Electronic ignition, microcontroller based ignition, internal combustion engine

İÇTEN YANMALI MOTORLAR İÇİN MİKROİŞLEMCİ TABANLI ATEŞLEME DEVRESİNİN TASARIMI, YAPIMI VE TEST EDİLMESİ

Çakmak, Nevzat Yüksek Lisans, Makina Mühendisliği Bölümü Tez Yöneticisi: Prof. Dr. A. Demir Bayka

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Bu çalışmada, yeni bir tasarım olan, sekiz silindir ve on altı pistonlu bir içten yanmalı motor için elektronik atesleme ünitesi tasarlanmış ve test düzeneği haline getirilmiştir. Sistem üzerinde bulunan on altı adet bujiyi ateşlemek için çift çıkışlı indüksiyon bobinleri kullanılmıştır. Bu bobinler PIC16F628A tip mikrokontrolcü tabanlı bir ateşleme devresi vasıtasıyla sürülmüştür; bu ateşleme devresi dijital sinyallerle tetiklenebilmektedir. Ateşleme devreleri ateşleme sinyallerini kare dalga şeklinde bir ana kontrol devresinden alır, aldığı sinyale göre indüksiyon bobinlerinin primer voltajını açar ya da kapatır. Ana devre PIC16F877A tip mikrokontrolcü tabanlıdır ve sistemde bu devreden iki adet bulunmaktadır. Bu ana devrenin görevi devir ve sıcaklığa gore ateşleme avansını belirlemek ve uygun ateşleme sinyallerini ateşleyici devrelere göndermektir. Bu ana devre devir bilgisini diğer ana devreden seri iletişim ile alır, sıcaklığı üzerinde bulunan analog kanal vasıtasıyla ölçer ve bu iki bilgiye gore önceden belirlenmiş ve harici eeprom belleğe yazılmış avans bilgisini okur. Diğer ana devreden aldığı silindir posizyon sinyalleri üzerine okuduğu avans bilgisini ekleyerek ateşleme sinyallerini oluşturur ve ateşleyici devreleri tetikler. Diğer ana devre silindir pozisyonlarını ve motor devrini iki adet manyetik sensör ve frekans voltaj çeviriciler vasıtasıyla dişli bir disk üzerinden tespit eder. Bu disk, piyasadaki mevcut motorların krank mili üzerinde bulunan dişli diski simüle etmek

için kullanılmıştır ve bir elektrik motoru vasıtasıyla sürülmüştür. Tasarlanan ateşleme ünitesi değişik devirlerde test edilmiş ve doğru ateşleme noktalarında ateşlemeyi gerçekleştirdiği görülmüştür.

Anahtar Kelimeler: Elektronik ateşleme, mikroişlemci tabanlı ateşleme, içten yanmalı motorlar

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NOMENCLATURE

R _S	: Source Impedance
R _{SS}	: Switch Impedance
R _{IC}	: Interconnect Resistance
C _{HOLD}	: Charge Holding Capacitor
T _{ACQ}	: Acquisition Time
T _{AMP}	: Amplifier Settling Time
T _C	: Holding Capacitor Charging Time
T _{COFF}	: Temperature Coefficient
T _{OSC}	: Oscillator Period
F _{OSC}	: Oscillator Frequency
V_{REF}^{+}	: Upper Limit of the ADC Reference Voltage
V _{REF}	: Lower Limit of the ADC Reference Voltage

CHAPTER 1

INTRODUCTION

Since the first day of mankind, people had been using tools to save their lives, these tools had always been advanced and this advance had affected the whole life, this simple rule will be always valid in human life, any advance in any area is going to affect the whole human life in social, economical and technological way. Advance process is the same in internal combustion engines, any advance in electronics, physics or material science have always affected internal combustion engines.

There has been a continuous progress in internal combustion engines because of the competitive nature of the automotive industry, and the progress is based on economical reasons; because as a commercial product, the internal combustion engine is an excellent trade object. For the last decades, some additional factors influencing progress in internal combustion engines have appeared; these factors are environmental regulations stated by governments. The aim of these regulations is to reduce effect of internal combustion engines on nature and to slow the decrease in fossil fuel reserves. After these regulations, automobile manufacturers have had to make various modifications in the operation of their engines. For example, to reduce NOx emissions car manufacturers started to use exhaust gas recirculation; this method works as follows. A certain amount of exhaust gas is sent into the cylinder with air gasoline mixture; this reduces peak temperatures which initiates NOx production during combustion. In the past, lead addition into gasoline was used against knock. However, concern over air pollution forced car manufacturers to abandon this method; and they started to use sensors and microcontroller based systems to avoid knock initiation. One of the issues which are regulated by rules is exhaust gas emissions. To reduce exhaust gas emissions to desired levels, manufacturers started using various sensors such as air/fuel ratio, ignition timing, valve timing, etc. to get efficient combustion. As a result, fully microcontroller based engine operating systems became popular; and most of the operations which were controlled mechanically, were controlled electronically by engine control units. One of the most important operations which are controlled electronically is ignition timing; because ignition timing affects combustion process directly; and poor ignition timing control results in ineffective engine operation and increase in exhaust gas emissions. Environmental considerations are not the only reason to use fully electronic ignition systems; use of such ignition systems also reduces maintenance costs and increases reliability and efficiency.

This study is based on a special kind of engine; it has 16 pistons, 8 cylinders and 2 axial cams which apply torque on a central shaft. The working principle of the engine is different than the engines which are assembled on the cars in the market. This ignition system is designed for this special kind of engine. Some ignition systems in the market may be modified to work with this engine, but there are some difficulties as follows. New generation ignition systems are fully electronic and microcontroller based, and also manufacturers make them so complicated because they do not want their rivals to copy them, so to design an ignition system may be easier way. An old fashioned ignition system which is designed for an engine with eight cylinders may be used, but to test a new design engine with an old fashioned mechanically triggered ignition system would not be satisfying. During designing a new ignition system for the engine, the working principles of old fashioned and new generation ignition systems were considered; advantages and disadvantages of them were examined. These ignition systems and their features are going to be given in the following parts.

1.1 Historical Background

The automotive industry had always been competitive, so it is too hard to follow the changes in this industry. The first reliable ignition system is magneto ignition system. Several inventors are credited with developing magneto ignition, but Siegfried Marcus held a patent in 1883 as magneto ignition electric ignition system [28]. In 1902, the double coil magneto ignition system was designed by Bosch. In this form of spark ignition system, a magneto supplies the ignition voltage for spark discharge independent of a battery or generator. The working principle of this system is that a time-varying magnetic flux is set up in the ignition armature as the rotating permanent magnets generate a current in a closed primary winding, this primary current is interrupted by breaker system to provide the magnetic flux to collapse rapidly to generate high voltage pulse in the winding which is connected to the spark

plug electrode, this high voltage jumps to the ground electrode of the spark plug as a spark. Since the flux generated by the rotating pole wheel depends on engine speed, the magnitude of the ignition voltage varies with speed for this reason and combination of necessity, weight, cost, and reliability reasons this type of ignition system is not used in modern engines, it is used in small engines such as in mopeds or chainsaws.

To start an engine with a magneto ignition system hand cranking method was used and it was very hard. After the availability of large batteries to provide a constant source of electricity, magneto systems were abandoned and battery operated ignition systems were used. In this system, an ignition coil (transformer) was used to step the battery voltage up to necessary levels for ignition and a distributor to direct the high voltage pulse to the right spark plug at the right time. The first battery operated ignition system was developed by Charles Kettering [24] in Dayton Engineering Laboratories Co. and introduced in the 1910 Cadillac. By this method, starting the engine was brought into the push-button realm. This ignition system is the primitive version of conventional coil ignition system which is still used in engines.

1.2 Modern Ignition Systems

1.2.1 Mechanically Timed Coil Ignition Systems

The breaker operated inductive ignition system has been used in automotive engines for many years. The system includes a battery(1), main switch(2), breaker(6), condenser(5), induction coil(3), distributor(4), spark plugs(7) and necessary wiring, and it is based on Kettering`s ignition system principle. Figure 1.1 shows schematic view of mechanically timed coil ignition system. The working principle of the system is as follows. When the breaker point is closed; the current flows from battery through primary winding of the ignition coil, breaker point and to ground (chassis of vehicle). This flowing current generates a magnetic field with in the iron core of the induction coil. When the ignition is required, the distributor cam touches the breaker and opens the contact; this action interrupts the current flow in the primary winding and results to decay of magnetic flux. This decay of magnetic flux induces high voltage in the secondary winding because of common iron core and winding number. The voltage induced in the secondary winding is routed by the distributor to correct spark.

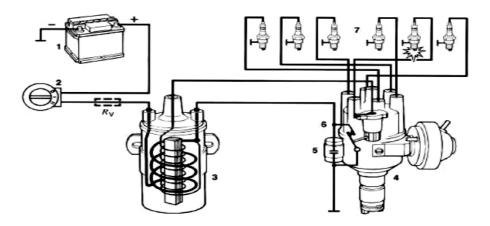


Figure 1.1: Schematic view of conventional mechanically timed ignition system to generate the spark

Mechanically timed coil ignition systems are used for many years, and they provide a useful introduction to ignition system design and operation. As it is stated before, any changes in electronics, material science and physics affects structure of engine and its control principle, such a change occurred in early 1950's, transistor is produced in Bell Labs. The transistor is the key active component in all modern electronic applications. Many scientists consider it as one of the greatest inventions of the 20th century. The invention affected all aspects of life, ignition systems were affected, too. Mechanically timed coil ignition system was replaced with transistorized coil ignition systems with the usage of transistor in automotive applications.

1.2.2 Mechanically Timed Transistorized Ignition Systems

In previous version of ignition systems, the primary current is controlled with a mechanical contact; it has some disadvantages as follows. After a working period, because of metal-metal contact wearing occurs and affects engine performance. In low engine speeds, higher current flows through mechanical breakers and shortens the working life of mechanical contacts; also this higher current induces high voltage in the secondary winding and shortens the working life of spark plugs. In starting

engine, mechanical contacts open and close slowly; it affects ignition in bad way. For the reasons stated above, transistor is used to eliminate metal-metal contact. In 1960's, mechanically timed transistorized ignition system was started to be used. In mechanically timed transistorized ignition system, there is an additional transistor compared to conventional mechanically timed coil ignition system as seen in Figure 1.2 [25], and its working principle is the same with that ignition system.

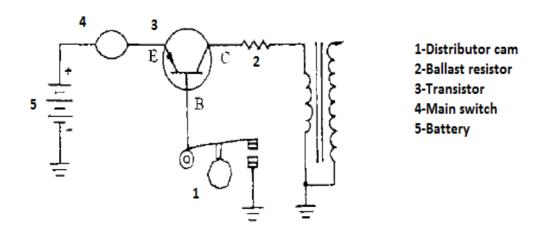


Figure 1.2: Schematic view of mechanically timed transistorized ignition system

In this ignition system, mechanical breaker controls the base current of the transistor so low current flows through mechanical contact; it means longer working life of mechanical contacts. The transistor also limits current flowing through the primary winding, so in low engine speeds high voltage does not induce in secondary winding; it provide longer spark plug life, better ignition timing, better ignition and better engine performance compared to conventional ignition systems. There are many transistor ignition types which were developed by big companies. Figure 1.3 shows a transistor ignition system which is developed by Courtesy of Ford Motor Co. [24]

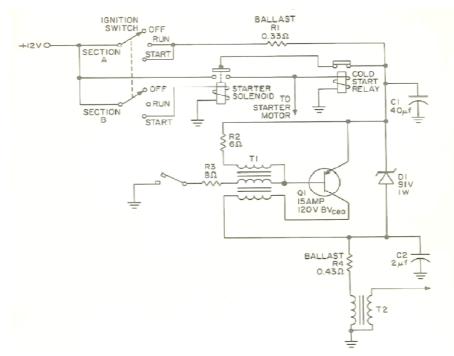


Figure 1.3: Using a pulse transformer to improve transistor-cutoff time (Courtesy of Ford Motor Co.)

1.2.3 Sensor Triggered Transistorized Ignition Systems

In automotive applications, the need for much reduced maintenance, extended spark plug life, improved ignition reliability, and increased ability to control resulted in usage of electronic circuits to control ignition process in 1980's. Figure 1.4 shows sensor triggered transistorized ignition system [25], in this system the distributor points and cam assembly of the conventional ignition system are replaced by a magnetic pulse generator or an optical sensor which detect the distributor shaft and sends signal pulses to electronic control module. This module switches off the flow of current to the primary winding of ignition coil and initiates the ignition. In older versions of this ignition system, mechanical advance system is in the distributor as in conventional ignition systems, but in newer versions advance is adjusted by control module. Also in former versions, signal pulses which are coming from magnetic or optical sensor directly trigger the transistor and initiate the ignition.

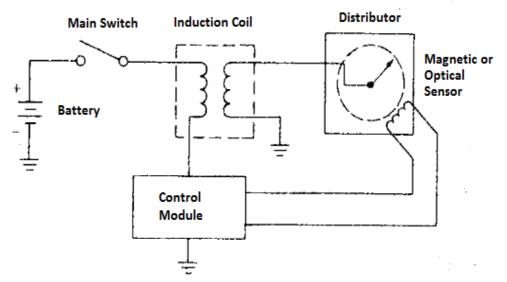


Figure 1.4: Schematic view of sensor triggered transistorized ignition system

1.2.4 Capacitive – Discharge Ignition(CDI) Systems

With this type of ignition system, a capacitor rather than an induction coil is used to store the energy necessary for ignition; this is the main difference of the system. Commercial development of CDI happened around the mid 1960's and it was tested on a 90cc Kawasaki motorcycle, but application in automotive was introduced by Bosch with "Bosch Motronic" in 1979. The system includes charging device, pulse shaping circuit, control unit, thyristor and ignition transformer. The working principle of the system is as follows. The transformer in charging device steps up the battery voltage to 400-600 volts and charges main capacitor. When control unit receives ignition timing signal, the capacitor is discharged rapidly via thyristor, voltage of primary winding of the ignition coils rises up to 400-600 volts, this voltage induces high voltage, around 40 kV in the second winding this is the necessary voltage for spark generation. Because of fast capacitive discharge, the spark is strong but short. This can lead to ignition failure at operating with very lean or dilute. This type of ignition is widely used in outboard motors, chainsaws, motorcycles and racing cars.

1.2.5 Distributorless Ignition Systems

Ignition systems with a distributor have been used for many years; but advances in semiconductors allow people to construct small chips to control most of the operations which was controlled mechanically in the past. After the replacement of mechanical or vacuum advance assembly in distributor with a microcontroller based operation, the size of distributors got smaller. To eliminate voltage losses during distribution, increase the accuracy of ignition point and decrease the cost, the distributor is replaced with control circuit and position sensors in 1980's, this type of ignition systems are called distributorless ignition systems(DIS). As it is seen in Figure 1.5, engine control module receives the position signals from camshaft and crankshaft position sensors and it uses these signals to detect cylinder positions and ignite the right cylinder at the right time, there is an igniter circuit this circuit works as follow. It receives ignition timing signal and number of ignition coil which will be ignited from engine control unit and ignites related spark plugs. There are various sensors such as engine load, cooling water temperature and knock sensor, engine control unit receives all the outputs of these sensors to control injection, advance etc. In the ignition systems with distributor, there is one ignition coil and all spark plugs are ignited from this coil, but in distributorless ignition systems there is one ignition coil for each spark plug or one ignition coil for two spark plugs.

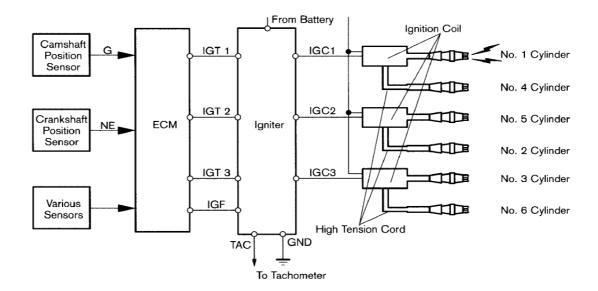


Figure 1.5: Schematic view of distributorless ignition system

There are many distributorless ignition systems in the market, for example General Motors Corporation held a patent related to distributorless ignition system [15], it is one of former versions. In this ignition system, there are two gear wheels on the crank shaft and two magnetic sensors. One of the gear wheel has only one tooth, this gear wheel is used to sign reference position, the other gear wheel has many teeth according to cylinder number as a choice and it is used to determine crank shaft angle, one of the sensor is used to count the teeth on this gear wheel and determine engine speed, and the other one is used to detect reference point. Firstly, the control circuit of the system detects reference position and determines position of the first cylinder (reference cylinder) signal then it counts the teeth with binary counters and determines position of the other cylinders. The system determines cylinder positions as mentioned above, it determines advance and dwell angle by using registers which was already adjusted according to engine speed on itself.

1.2.6 Direct Ignition Systems

Nowadays, this is the most popular ignition system. Operational principle of this system is the same with distributorless ignition system, but the place of ignition coils is different. Ignition coils are directly mounted on the spark plugs in this ignition system. By this way, ignition cables and electromagnetic interference caused by ignition cables are eliminated. In distributorless wasted spark ignition systems, the working life of spark plugs is shorter compared to direct ignition systems. In some direct ignition systems, igniter circuit is integrated on ignition coil. Figure 1.6 shows schematic view of positions of ignition coils in direct ignition system.

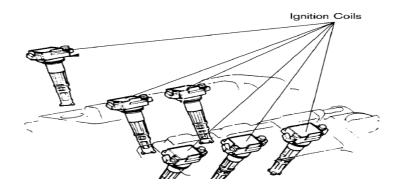


Figure 1.6: Positions of ignition coils in direct ignition system

There are many patents about direct ignition systems which are held by big companies, one of them is held by Fiat Auto S.p.A.[19]. In this system, to generate ignition sparks in the correct sequence, there is a need to get a stage signal which defines the stroke of selected cylinder as seen in Figure 1.7. This stage signal is supplied by a sensor associated with a timing member; the timing member is inletexhaust valves operating shaft. This stage sensor (7) may be placed anywhere, but important point is that for a 4 stroke cycle engine the shaft on which the stage sensor is assembled shall have a rotation ratio 1/2 according to crank shaft. In Figure 1.7, there is a phonic wheel with part number 7, this wheel is used to detect engine shaft rotation and determine top dead center of cylinders. As seen in Figure 1.7, the phonic wheel (7) has four regularly arranged notches and two notches; because this system is related to five cylinders engine, and two notches give the top dead center position of reference cylinder and the other four notches give the top dead center position of the other cylinders. Top death center position does not give the stroke of a cylinder it may be compression or exhaust, so to differentiate strokes, engine control unit use stage signal. If the system use wasted spark method, there is no need to look at the stage sensor, because the control module initiates spark for all of the cylinders which are at the top dead center position, combustion takes place in the cylinder which is at the compression stroke, the other cylinder will be at the exhaust stroke and spark will not affect anything.

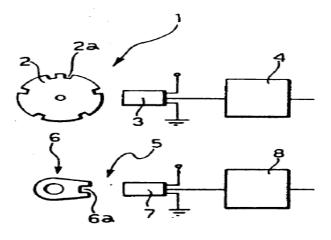


Figure 1.7: Sensors and disk used to determine cylinder positions in Fiat direct ignition system

This ignition system uses wasted spark ignition, too. To overcome the disadvantage of extended starting times due to the fact that sparks are generated during the first revolution of the engine and until correct stage of the ignition occurs, wasted spark ignition method is used during starting the engine, then control unit of the ignition system detects stage signal when correct stage signals start to come, control module shifts ignition system to direct ignition method.

There is another patent which is held by another big company, Robert Bosch GmbH [20]. The operating system of this ignition system is the same with the ignition system which is told above, the only difference is that a hall sensor is used as a stage sensor instead of a magnetic sensor.

CHAPTER 2

THE NEW DESIGN ENGINE

This thesis was studied to design and construct a microcontroller based electronic ignition system for a new design engine. So, the first step of our study is examining the new design engine. To understand its working principle and advantageous sides; firstly, we should learn the possible ways to optimize engine efficiency which are not used in conventional internal combustion engines and its different sides than similar engine designs.

2.1 Some Possible Ways of Optimizing Efficiency

2.1.1 Constant Volume Combustion

Many studies were conducted on position of spark plugs, shape of combustion chamber and swirl angle of intake charge to increase combustion efficiency in the cylinder. But, there is another way to increase thermal efficiency, this is constant volume combustion. This way is based on keeping constant the volume of combustion chamber during combustion; if you can keep the volume of combustion chamber constant, you can get higher combustion pressures. Actually, Otto cycle considers constant volume combustion, but it assumes combustion process is so rapid and piston does not move during combustion. Figure 2.1 shows ideal Otto cycle pressure versus volume diagram. As it is seen in Figure 2.1, ideal Otto cycle proposes constant volume combustion (2-3). The shaded area of figure gives the useful work which is converted from available energy during combustion process as it is given by the formula in the figure, so it is a representation of thermal efficiency. If we can increase this shaded area we increase thermal efficiency of process.

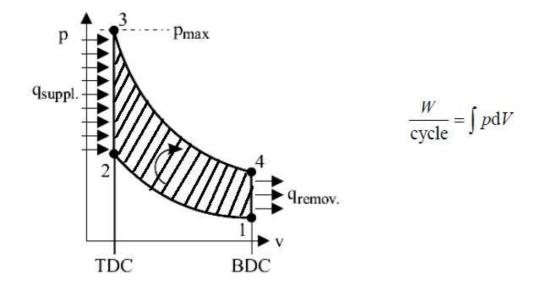


Figure 2.1: P-V diagram of ideal Otto cycle

The peak pressure at point 3 in Figure 2.1, can be increased by keeping volume constant during combustion process, so it will increase the shaded area and the work done during combustion will increase. But this is too difficult with conventional crank shaft engines. Because, the crank shaft rotates continuously, and staying at TDC of pistons is too short and dependent on engine speed. At higher engine speeds, the volume of combustion chamber increases faster, so combustion pressures cannot reach their theoretical peak pressures.

Figure 2.2 shows a piston path for a conventional crank shaft engine; as it is seen in the figure the piston stays at TDC and BDC for too short time interval, so constant volume combustion process is valid for very short time interval.

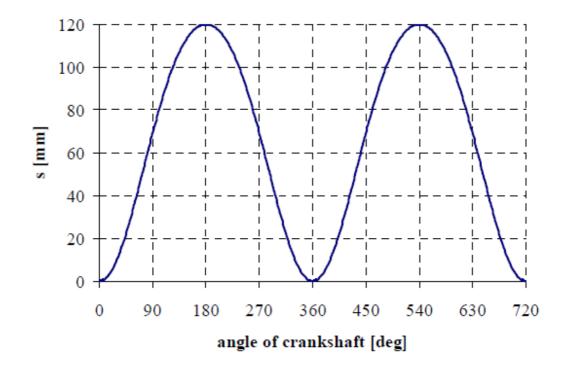


Figure 2.2: Path of a conventional crank shaft engine piston

As it is stated before, to achieve constant volume combustion with conventional crank shaft engine is not possible, there is a study about constant volume combustion in the literature it will be helpful to understand physics of achieving constant volume combustion, it is based on changing kinematic of conventional IC engine crank shaft and giving pause or dwell at the top dead center (TDC) and bottom dead center (BDC) while crank shaft still rotates about 20°. With this dwell at TDC, the author proposed to have constant volume for combustion, so higher combustion pressures and higher thermal efficiency. The piston path of this unconventional engine is shown in Figure 2.3, as it is seen in the figure, piston position stays at the same position while crank shaft keep rotating, so this provides condition for constant volume combustion.

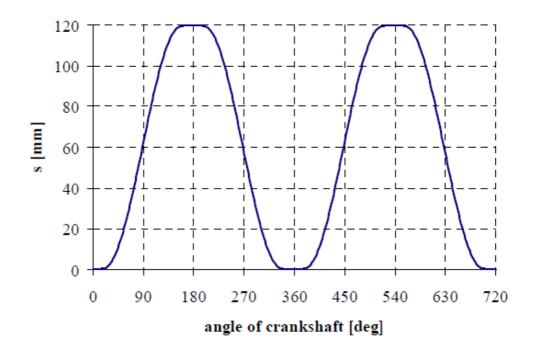


Figure 2.3: The piston path of engine with modified kinematic

This modified engine had been simulated for full throttle conditions to prove the effect of constant volume combustion on efficiency, the result is shown in Figure 2.4. As it is seen in the figure, higher combustion pressures and efficiency were realized.

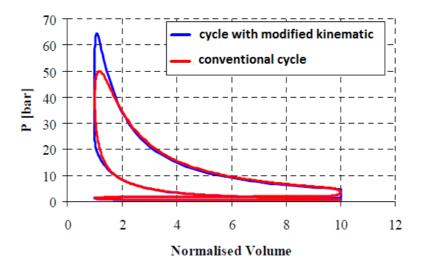


Figure 2.4: Comparison of conventional cycle and cycle with constant volume combustion

Constant volume combustion is one of the most effective ways to increase combustion efficiency, but it also has some drawbacks. The temperatures during constant volume combustion increases with increasing pressure and efficiency and it triggers formation of NO_x emissions, because NO_x formation increases with high temperature, so you may need extra exhaust gases treatment. The compression ratio can be reduced to eliminate high temperature caused by constant volume combustion; it also reduces the compression work, frictional losses and temperature and mechanical wear caused by friction, so the useful life of the engine is increased. Also, tendency to spark knocking increase with constant volume combustion, so to avoid knocking the swirl of air/fuel mixture should be satisfying. Also, ignition timing should be arranged to avoid knocking and back pressure on the piston.

2.1.2 Hyper-Expanded Cycle

As it is stated in previous part, to increases thermal efficiency we should expand the shaded area in Figure 2.1. One of the ways to expand the area is to apply constant volume combustion as stated before; there is another possible way, hyper-expanded cycle. The point 4 in Figure 2.1 is the end of expansion stroke, and as it is seen in the figure, the pressure at point 4 is relatively high; it is around 3 atm [27], it means: there is a potential to produce useful work. The common way to use this relatively high exhaust pressure is to use a turbocharger. In naturally aspirated engines, intake air goes into cylinder by vacuum of downward motion of piston, but the cylinder is not filled fully. The ratio of gas flow into the cylinder to the theoretical mass of gas that can be inducted in ideal conditions is called as volumetric efficiency. The aim of using turbocharger is to increase volumetric efficiency by increasing the mass of intake air by increasing pressure so the density, by compressing intake air. To operate this compressor (turbocharger), the exhaust gas is used. Another way to utilize relatively high exhaust pressure is to increases the length of expansion stroke, so the relatively high exhaust pressure at the end of expansion stroke of a conventional crank shaft engine can keep doing work against the piston; this process is called the hyper-expanded cycle. But this may be impossible with conventional crank shaft engines which have the same compression and expansion stroke, because high compression ratio increases tendency to knocking, so this limits compression

stroke and expansion stroke. The hyper-expanded cycle can be shown as in figure 2.5; the work result of conventional crank shaft engine cycle is the area within the points 1-2-3 and 4', the work result of hyper-expansion cycle is the area within the points 5-2-3 and 4'. The area so the useful work of hyper expansion cycle is bigger than conventional crank shaft engine cycle, it means higher thermal efficiency. The hyper-expansion cycle was applied in some engines in the past, although the method decreased fuel consumption and increased thermal efficiency; the overall result was not satisfactory because of following reasons: in hyper-expansion cycle piston travels longer strokes compared to conventional cycle, so hyper-expansion cycle takes longer time it may cause lower power. Actually, for some throttle conditions exhaust pressure at the end of expansion stroke may drop below ambient pressure and it may produce negative work on the piston. So an optimum point for hyper-expansion should be selected.

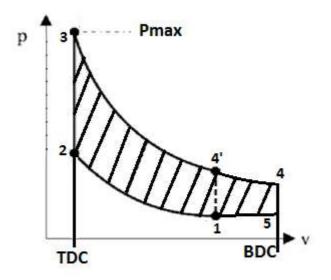


Figure 2.5: Hyper-expanded cycle

2.1.3 Modification Of Gas Exchange Process

There is another point which will be considered to optimize engine performance and used a design point in our new design engine; it is modification of gas exchange process. In conventional engines, the piston moves within the same limits and when it reaches to its upper limit, the TDC, for exhaust stroke, there is still remaining volume as seen in Figure 2.6. At the end of exhaust stroke, there will be exhaust gas in that volume, and this residual exhaust gases will try to prevent fresh air/fuel mixture to go into cylinder in intake stroke and decrease the density of the gas entering the cylinder by heating it. And this will cause to decrease in volumetric efficiency.

There are some studies in the literature about this residual gas problem; one of them is valve overlap method. When the piston reaches to the upper limit, TDC, both of the two valves are open and exhaust gas with relatively low pressure helps fresh air/fuel mixture with relatively high pressure to goes into cylinder; the pressure difference between intake and exhaust manifolds initiate gas flow and helps residual gas to flow out of cylinder, but it may cause some amount of fresh air/fuel mixture to escape into exhaust manifold and increase in fuel consumption, and to create pressure difference between intake and exhaust manifolds, there is need to design special massive manifold systems [27]. There are some engine designs in the literature to eliminate residual gas at the end of exhaust stroke by mechanically such as Atkinson engine. In that engine design, piston moves further position than a conventional engine by a special linkage mechanism and there is a little amount of residual exhaust gas at the end of exhaust stroke it means there is larger free volume for fresh intake charge and increase in volumetric efficiency.

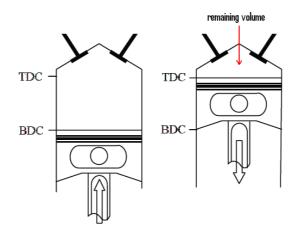


Figure 2.6: Piston working limits in a conventional engine

2.1.4 Alternative Valve Systems

Another point, which will be considered in new design engine to optimize efficiency, is valve system. In conventional internal combustion engines, poppet valve system is used. As seen in Figure 2.7, a conventional poppet valve blocks the port and the flow itself; as a result quality of swirl, which is very important effects on combustion efficiency, decreases [27]. There are some alternative valve systems in the literature as follows: rotary valves, slide valves and sleeve valves. One of them may be used to attain greater flow area and better gas dynamics, but they have also some drawbacks.

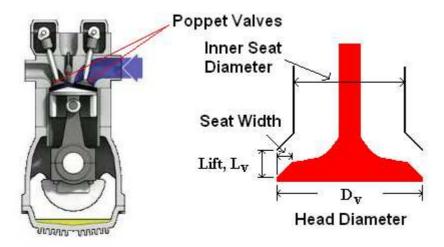


Figure 2.7: IC engine with poppet valve and a poppet valve in port

Figure 2.8 shows the rotary type valve system, in this system the valve block is driven by the crank shaft at a constant ¹/₄ of crank shaft speed and rotates around the axis of the ball bearing shown in the figure. As seen in the figure, the ports are fully open and there is not any part of valve system to block or disturb the gas flow. One of the most important drawback of the system is the friction surface is larger than poppet valve system, so lubrication is a problem. Also, to avoid gas leakage the system needs highly satisfactory sealing because of large contact surface. In poppet valve system, high exhaust and compression pressures act on poppet seats and help to avoid gas leakage, but in this system all pressures act on valve system this is another disadvantage of the system.

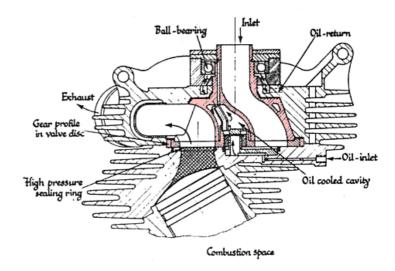


Figure 2.8: Rotary valve system

Another alternative valve system is sleeve valve system, in this valve system a sleeve, having inlet and outlet holes on itself, locates between cylinder wall and piston. And the inlet and exhaust ports of the cylinder are at the side of the cylinder different than conventional poppet valve system. The sleeve is driven by camshaft and it slides and opens inlet or exhaust port according to stroke. The same drawbacks except pressures acting on the valve system and advantages which are stated in rotary valves are valid in this valve system, too. Figure 2.9 shows a drawing of a sleeve valve system.

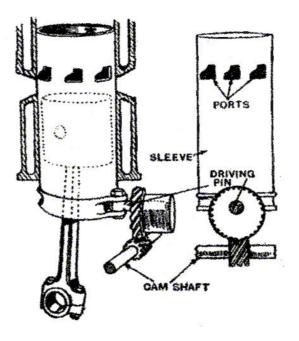


Figure 2.9: Sleeve valve system

The other alternative solution for the valve system is slide valves, this valve system has the same working principle, advantages and drawbacks with sleeve valve system, but slide valve does not cover all cylinder surfaces; so it has less friction surface than sleeve valve, this may be stated as an advantage over sleeve valves. Figure 2.10 shows slide valve system.

As stated above, with alternative valve systems higher volumetric efficiency, better gas dynamics and as a result higher combustion efficiency can be attained, but they have important drawbacks such as high friction, difficulty in sealing and lubrication problems.

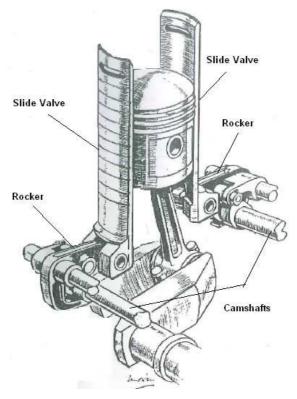


Figure 2.10: Slide valve system

2.2 Engine Designs Similar With the New Design Engine

There are some engine designs which have used the methods to optimize efficiency, mentioned above. To look at that designs and examine their advantages and disadvantages will be helpful to understand the new design engine, but this part will not cover all engine designs similar with our new design engine.

In conventional Otto engines, the compression and expansion strokes are the same, and tendency to knocking limits compression stroke and expansion stroke, so the hyper-expanded cycle which plays an important role on engine efficiency is not applicable. But in 1882, Atkinson introduced its four-stroke engine with hyperexpansion concept for the first time which has higher thermal efficiency than Otto cycle. The first version of Atkinson engine was composed of two opposed pistons. The four strokes of the operation are occurred for the one revolution of crank shaft by the help of complex linkage mechanism. The most important feature of the engine is that the engine has different stroke lengths by the help of its complex linkage mechanism; this eliminated the effect of knock tendency on hyper-expanded cycle which is stated before, and increased thermal efficiency by utilizing relatively high exhaust gases at the end of expansion stroke of conventional Otto engines. Also, by the help of increased exhaust stroke, there is negligible amount of residual exhaust gas in the cylinder; it means more free volume for fresh air/fuel mixture, so increased volumetric efficiency. The Figure 2.11 shows Atkinson engine, its linkage mechanism and strokes with different lengths. As seen in the figure, the engine completes its cycle for the one rotation of crank shaft.

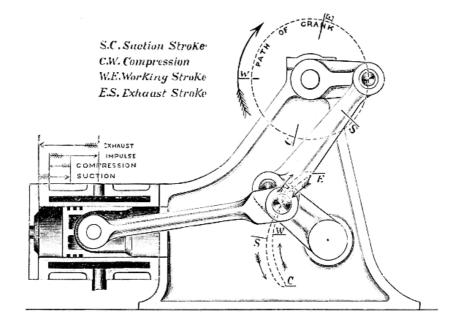
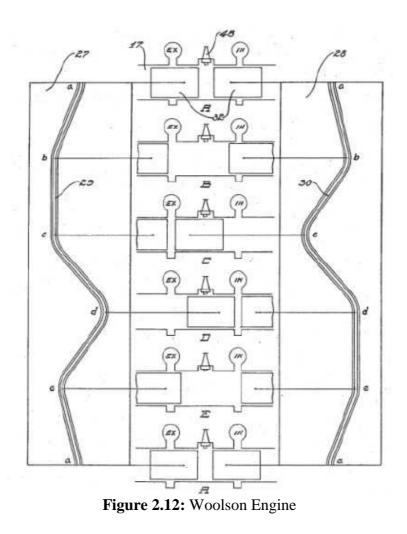


Figure 2.11: Atkinson engine

Although Atkinson engine had higher thermal efficiency, it was heavy, complex and its speed was limited compared to four-stroke Otto cycle engine. So, it couldn't find wide commercial application. Another design which is similar with Atkinson's opposed piston engine, was introduced by Woolson in 1931. In this design, two cams are used to operate the opposed pistons which are located in common cylinders. Fresh air/fuel mixture is taken into cylinders from the inlet port located on one end of the common cylinder and compressed between two pistons, and exhaust gas is sent to exhaust port located on the other end of common cylinder after expansion. In the engine operation, two pistons are used to create one combustion volume. Higher volumetric efficiency is proposed in this design, but any change on the cycle is not introduced. This engine design is important, because axial cams are used to operate pistons for the first time. The Figure 2.12 shows drawing of Woolson engine, its strokes and its two cams which operates the pistons.



Another engine design which is axial cam operated is Tibbets engine. Operation of this engine looks like Woolson engine, two opposite pistons are operated by two

axial cams in a common cylinder and the gas exchange process is held by ports on the cylinders. There are two inlet ports and one exhaust port for each cylinder, the exhaust port is located in the middle of the common cylinder. There are two combustion volumes which are created by combination of two opposed pistons and engine completes two cycles for each revolution by the help of different axial cam profile. Figure 2.13 shows drawing of Tibbets engine. Another engine design which has axial cam operated opposed piston in a common cylinder is Kristiansen engine, this engine design was introduced in 1986. This design is the most similar engine design to our project engine [27], it introduces hyper-expanded cycle and constant volume combustion which are mentioned as ways of optimizing engine efficiency in Part 2.1. Hyper-expanded cycle was also introduced by Atkinson, this engine differs from Atkinson's because the expansion to compression ratio is adjustable in this design. The pistons are driven by axial cams and the movements of pistons dependent on cam profiles, so the movements of pistons and expansion to compression ratio can be adjusted by changing the cam profiles. In this design, there are one common inlet port, one common exhaust port and one ignition point. There are some engine designs with axial cams which are stated above, but operation of Kristiansen engine is different. In this design, the axial cams are stationary and the block containing the cylinders with two opposed pistons rotates around the centerline of axial cams. The rotating parts have big inertia compared to the other engine designs, so the forces acting on cylinder surfaces result of centrifugal forces during rotation is too much, and this can damage the engine. Also, the gas dynamics in cylinders and combustion efficiency may be affected by high centrifugal forces.

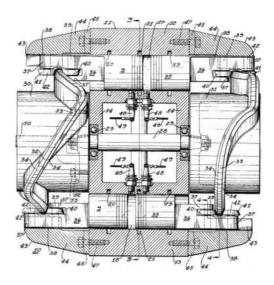


Figure 2.13: Tibbets engine

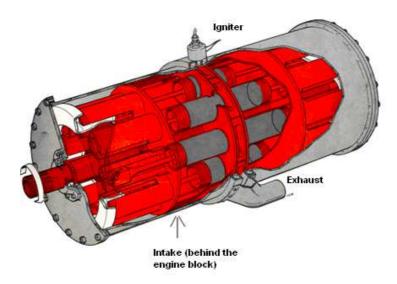


Figure 2.14: Kristiansen engine

2.3 Features of the Project Engine

The similar engine designs are stated above; the ways to increase engine efficiency which are mentioned in previous parts are tried on those engines. For example, hyper-expanded cycle and modification of gas exchange process are stated in Atkinson engine, constant volume combustion and hyper-expanded cycle were stated in Kristiansen engine, also alternative valve systems instead of conventional poppet valve were stated. As stated before, to increase engine efficiency using alternative crank shaft system is necessary, alternative crank shaft system is used in the engines given above as similar engines. The mostly mentioned method to drive pistons instead of conventional crank shaft engine is to use two axial cams to drive pistons. Also, axial cams to drive piston are used in our project engine, too. Figure 2.15 shows drawing of such type of engine. As you see in the figure, there are two cams which are mirror twin of each other. The opposed pistons travel on the special profile of opposed cams, while traveling on the profile the pistons come closer or go further, and initiate four strokes of engine. Profile of the cams determines the piston paths, so to change the piston path or keep the piston stationary during combustion (constant volume combustion) is possible with this kind of piston drive method, this may be stated as the most important advantage of axial cams.

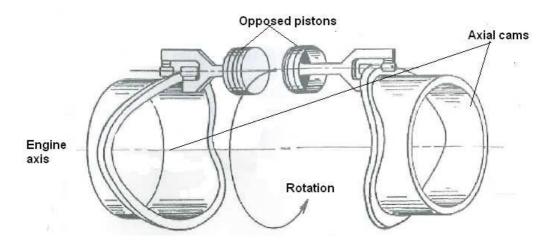


Figure 2.15: Drawing of an engine with axial cams and opposed pistons

The axial cams which are used in our project engine look like the cams in the figure, but they are mounted with 180° difference, so the same stroke is initiated by the pistons which located 180° difference on the engine and all strokes take place for all pistons in each revolution of the engine; it means all strokes take place in 180° revolution of engine for one piston. The project engine contains 16 pistons, 8 cylinders and 2 axial cams. Two opposed pistons work in a common cylinder and these pistons are driven with rotating axial cams. The Figure 2.16 shows the axial cams in the project engine and stroke positions on the cam. As it is seen in the figure, the axial cams are mounted with 180° difference and all strokes are completed in 180° .

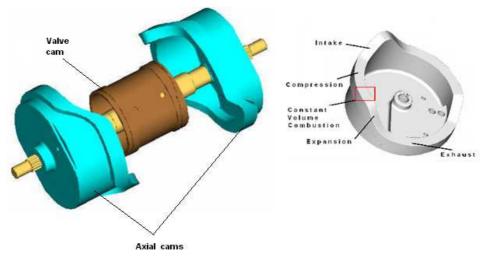


Figure 2.16: The axial cams, stroke positions on the cam and valve cam of the project engine

As stated above, there are 8 common cylinders, and 2 opposite pistons are located in a common cylinder. The positions of common cylinders can be shown as in Figure 2.17. By the help of special design 2 axial cams, there are two complete cycle in all common cylinders. And there are two combustions at the same time, so there are 8 combustion points. The combustions which are at the same time, take place in the cylinders located 180° difference. The positions of pistons and combustion points can be shown as in Figure 2.18.

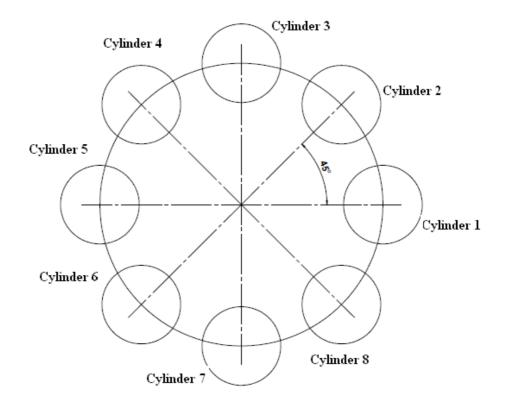


Figure 2.17: Locations of the common cylinders on the engine block

The cylinder pairs which are located with 180° difference are cylinders 1-5, 2-6, 3-7 and 4-8. The same strokes take place in cylinder pairs as it is seen in Figure 2.18.

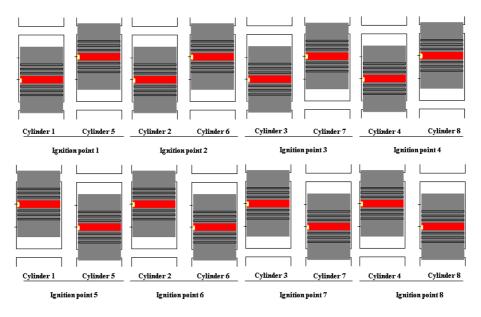


Figure 2.18: Ignition points and positions of the pistons.

To complete the cycle in 180° is initiated by combination of motions of the two axial cams, to examine the cycle for a piston stroke by stroke will be helpful to understand their working principle and visualize the motion of opposed pistons in the common cylinder. Figure 2.19 shows four strokes of a piston (the piston and axial cam on the left side in the figure are called as piston 1 and cam 1; the other piston and axial cam are called as piston 1' and cam 2) and the position of the pistons and axial cams. In the intake stroke, the profile of axial cam makes piston 1 travel to the axial cam 1 side of engine and create vacuum to let the fresh air/fuel mixture come into the cylinder while piston 1' is staying stationary. In the compression stroke, while the piston 1 is traveling on the flat part of the cam profile and staying stationary; the cam 2 pushes the piston 1' and makes it to travel to cam 1 side of engine and compress the air/fuel mixture. After compression stroke, both pistons stay stationary that means constant volume for combustion which is one of the most effective ways to increase efficiency. In expansion stroke, the expanded volume in the combustion chamber makes piston 1 travel to axial cam1 side of the engine while the piston 1' is traveling on the flat surface of the axial cam 2 and stays stationary in horizontal direction. At the end of expansion stroke, the piston 1 stays stationary, and the cam 2 pushes piston 1' against piston 1 and makes exhaust gases flow to atmosphere. As it is seen, the strokes of a piston is completed by combination of two piston motions, so it creates a chance to complete all strokes in 180° for one piston.

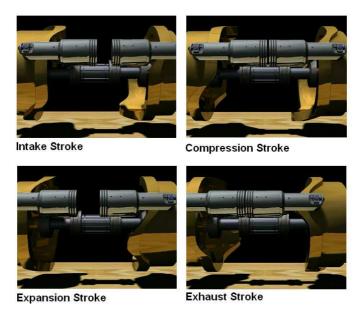
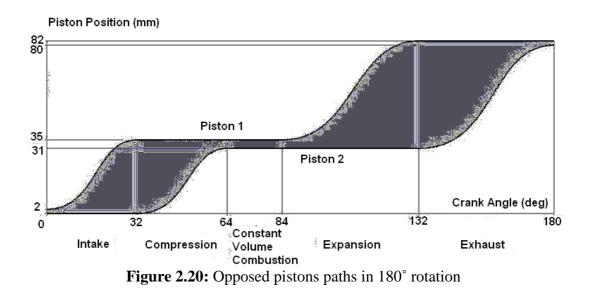


Figure 2.19: Four strokes of a piston in the project engine

In part 2.1.1, the effects of constant volume combustion on engine efficiency are given and a study from the literature [29] is given. In that study, the conventional motion of crank shaft and connecting rod is modified and pauses are created at the end of compression and expansion stroke while the crank shaft keeps rotating as seen in Figure 2.3, plot of piston path. Also, the increase in engine efficiency is stated in that study. It is possible to plot such a graph for our pistons and examine piston motion, constant volumes and gas exchange process. As it is seen in the Figure 2.20, there is 20° difference between the end of compression stroke and the beginning of expansion stroke with constant volume; this area is given as "constant volume combustion" in the figure. The ignition process can be initiated at any point of this area, but this ignition point should be determined after some calibration tests. But it is obvious that the project engine is able to initiate constant volume combustion easily by the help of its axial cams with special profile.



Another way to increase engine efficiency is hyper-expanded cycle. With this cycle, we can use relatively high pressure exhaust gas at the end of expansion stroke of a conventional crank shaft engine. In conventional crank shaft engines, all stroke lengths are the same, so if you increase expansion length the compression length increases, too. But knock tendency is increases with increasing compression ratio; this is a limiting factor to apply hyper-expanded cycle in conventional crank shaft engines. In Atkinson engine, a complex linkage mechanism is used to apply hyper-expanded cycle; in that engine all stroke lengths are different, so knock tendency is

eliminated. In Kristiansen engine and our project engine, piston motion is dependent on profile of the axial cams and stroke lengths do not need to be the same, so we can arrange the piston path and stroke lengths by changing profile of the cams easily. To apply hyper-expanded cycle, the profile of the cams is designed to have 50% longer expansion stroke than compression stroke. The hyper-expanded cycle can be seen in figure 2.20; in compression stroke the piston 2 travels from 0 to 31 mm while the other piston is stationary, but in expansion stroke, piston 1 travels 47 mm, from 35 mm to 82 mm, while the other piston is stationary, it is about 50% longer than compression stroke (31 mm). Another point which is considered in the project engine design is modification of gas exchange process. As it is stated in part 2.1.3, piston works within some limits TDC and BDC as in Figure 2.6. And there is a remaining volume, which piston cannot reach to, at the end of exhaust stroke. Some residual exhaust gases stay at that volume and reduce the volume which will be filled with fresh air/fuel mixture, so it causes to drop in volumetric efficiency. In Atkinson engine, piston goes further than a conventional crank shaft engine by the help of its complex linkage mechanism and decreases the volume of residual gas in the cylinder, and increases volumetric efficiency. The profile of axial cams is designed to reduce the volume at the end of exhaust stroke to eliminate residual gas and drop in the volumetric efficiency in the project engine. This feature of the project engine can be seen in the exhaust stroke in Figure 2.20, there is 2 mm difference between pistons (about 5.7 cc for 60 mm inner diameter of cylinder) at the end of exhaust stroke.

Another issue to be considered in the design of project engine is valve system. In conventional engines, poppet valves are used as inlet valves and exhaust valves. In poppet valve systems, gas leakage or sealing is not a problem because the pressurized gas in the cylinder pushes the valves against the valve seats and tries to close the valves; this situation may be stated as an advantage of poppet valve system. Also, poppet valve system some disadvantages as stated in part 2.1.4. As it is seen in Figure 2.7, poppet valve stays in front of the port and blocks the flow and disturbs the swirl even it is fully open. This may cause poor swirl, poor combustion and low volumetric efficiency. The conventional poppet valves are driven by a cam shaft, the sinusoidal motion of cam driven system causes the valves to open or close slowly. They come to fully open condition at the middle of the stroke; this causes a drop in

the volumetric efficiency or drop in the useful work. In the project engine, an alternative valve system seen in Figure 2.21 is used. As it is seen in the figure, there are two slots: exhaust and intake slots. This valve can move 8 mm forward or backward, and opens the cylinder to exhaust port or intake port by using those slots according to stroke. The flow area of these valves is 35% larger than a conventional poppet valve and it can open or close 4.7 times faster than a conventional valve. The positions of exhaust and intake slot are different, so two cylinders can use the same intake or exhaust ports on the engine block. There are compression rings on the piston heads, and these rings are located between piston and valve, so they avoid leakage from cylinder to ports via the slot.

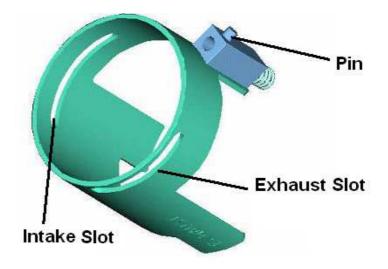
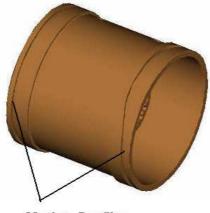


Figure 2.21: Valve used in the project engine

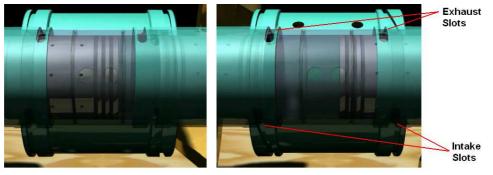
The philosophy behind the motion of these valves is similar with the motion of pistons. As seen in Figure 2.16, there is a valve cam, which is a hollow cylinder, mounted on the axis of the engine. This part is used to move valves and, arrange the exhaust and intake timing. To move the valves, the cam has motion profiles which are specially designed to move the valves according to piston stroke and arrange valve timing; the pin of the valve seen in Figure 2.21 travels on this profile.



Motion Profiles

Figure 2.22: Valve cam of the project engine

To understand the working principle of these valves, we should see them on the pistons. Figure 2.23 shows the condition of these valves during intake and exhaust stroke. As seen in the picture on the left hand side of the figure, piston 1 is at the beginning of the intake stroke and the intake slot is fully open to intake port, the same situation is valid for exhaust stroke. As it is stated before, conventional poppet valve comes to fully open condition at the middle of stroke, but the valve system used in the project engine is fully open at the beginning of stroke, this is one of the most important advantages of the valve system.



Beginning of Intake Stroke

Beginning of Exhaust Stroke

Figure 2.23: Position of valves during intake and exhaust stroke

Some possible ways to increase engine efficiency are stated in part 2.1 and some engine designs which try to apply those possible ways are also stated. In our project

engine, all of those possible ways are considered and applied on the engine as mentioned above. Besides, it also has some advantages by the help of its working principle and geometry. In conventional crank shaft engines, component of the force, which is applied by crank shaft on connecting rod and piston head, acts on the cylinders wall; this affects compression rings and oil film between piston head and cylinder wall. But in the project engine, the pistons are driven with axial cams, and these axial cams apply force on pistons perpendicularly, so there is no force component acting on the cylinder wall, this will increase useful life of compression rings and engine. Conventional crank shaft engines work with vibration and noise because of the nature of crank shaft and connecting rod motion; but in the project engine, the pistons travel on the smooth profile of the axial cams, so there is no vibration caused by motion of pistons and cams. Also, combustion takes place in the cylinders with 180° difference, so the engine is in balance in radial direction. As it is stated before, the pistons travel on the profile of the axial cams, there is not a connecting rod or the other parts which are used in conventional crank shaft engines to assemble the piston to crank shaft, so the pistons used in the project engine are lighter than the pistons in conventional crank shaft engines; this is a factor which can affect engine efficiency. The engine blocks of conventional internal combustion engines are commonly manufactured with casting process. But the block of project engine can be manufactured by a CNC milling machine. Also, the components of the engine can be assembled easily. These features of the project engine can be stated as its advantageous sides.

CHAPTER 3

EXPERIMENTAL SETUP

In this chapter, the designed and constructed test set-up for special engine that was mentioned in previous chapter will be introduced. Each subcomponent in the set-up and their working principle will be told step by step. Figure 3.1 shows the overall test set-up.

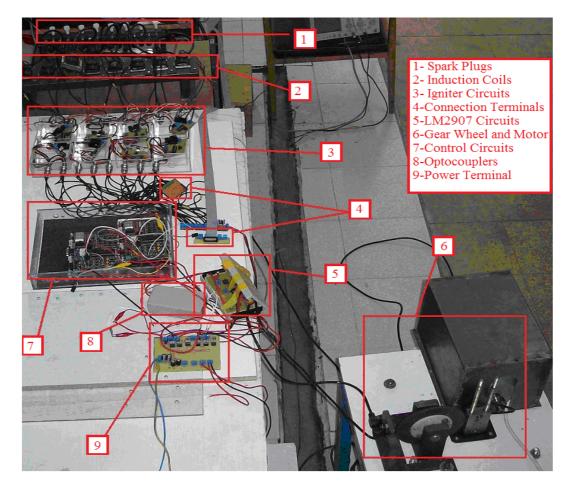


Figure 3.1: Experimental set-up

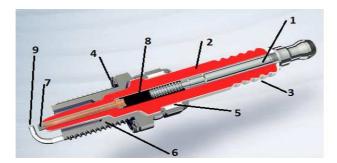
3.1 Induction Coils, Ignition Cables and Spark Plugs

3.1.1 Spark Plugs

There are many ignition types which are used now or was used in past, they can be grouped by their high voltage creation or their voltage distribution. Whatever ignition type is, spark plug plays vital role in petrol engine. It is responsible for ignition of air-fuel mixture. The quality of ignition directly affects several factors which have great importance for both quality of the driving experience and the environment. This includes starting, smooth running, general engine performance and efficiency as well as reduction of harmful emissions. When we consider a spark plug must ignite air-fuel mixture between 400 and 4000 times per minute, it becomes clear how difficult the spark plugs job is and how important the contribution of spark plug technology is for adherence to current emission standards and to the reduction of fuel consumption.

A spark plug is composed of different parts as seen in Figure 3.2: Connection terminal, insulator, current leakage barriers, gasket, inner seals, metal shell, centre electrode, resistor and ground electrode. Connection terminal is the top part of the spark plug, it is a barrel shaped or 4mm thread. The high tension ignition lead or pencil coil is plugged onto the terminal. This connection allows the high voltage to be transferred to firing end of spark plug. The ceramic insulator has two tasks. The main function is to provide a high degree of electrical insulation preventing the high voltages discharging to earth externally via the engine block to other components. It also allows efficient transfer of the heat of combustion from the firing end to cylinder head. The current leakage barriers on the outside of the insulator prevent the leakage of electrical energy to the vehicle body earth. They do this by increasing the length of the path that the current would travel to reach the earth point provided by the metal shell. This in effect is like having a significantly taller insulator section ensuring that electrical energy takes the path of least resistance through the centre electrode. The gasket ring prevents any possibility of combustion gas leaking past the spark plug due to the extremely high combustion pressures. In doing this it prevents any cylinder pressure losses. Another important function is that provides good conduction of heat to the cylinder head. The inner seals create a gas-tight connection

between insulator and metal housing. The seal is made from talcum ring enclosed between two additional stainless steel sealing rings. During production of spark plug the talc ring is compacted tightly ensuring a perfect gas tight seal. The metal housing or shell also plays an important role in the thermal conductivity of the spark plug as it is part of the mechanism of transferring heat away from the insulator to the cylinder head. The centre electrode of a standard spark plug is comprised mostly of a nickel alloy. From the end of this electrode the spark must jump over to the earth electrode. Some spark plugs have a copper core, which significantly improves the thermal conductivity preventing overheating. The resistor is used to limit high voltage to ensure electromagnetic compatibility (EMC). And thus the fault-free operation of the onboard electronics, a ceramic resistor is used inside the spark plug as an interference suppression device. This resistor is composed of carbon and glass compounds which form a solid component within the spark plug. The last part is ground electrode, this part is made of a special nickel alloy, it provides opposite electrical pole to central electrode and high voltage jumps over this part.



1-Connection terminal 2-Insulator 3-Current leakage barriers 4-Gasket 5-Inner seals 6-Metal shell 7-Centre electrode 8-Resistor 9-Ground electrode

Figure 3.2: Parts of a typical spark plug

In our system, standard NGK spark plug is used. This is spark plug of choice in millions of vehicles, because of its consistent performance and OEM quality. Figure 3.3 shows the spark plug which is used in our system.



Figure 3.3: Standard NGK spark plug which is used in our system.

3.1.2 Ignition Cables

Another main component of ignition systems is ignition lead. It is responsible for conducting necessary voltage for spark to spark plug connection terminal as little loss as possible. Since the ignition voltage rises up to 36000 volts which is very high voltage range, the ignition leads have to be protected accordingly against over voltage. The ignition voltage must never flow to ground, since this could cause misfiring, so there should be good insulation. As any component on the engine, they should be designed to resist hard working environment. They should be resistant to becoming brittle and cracked even at high temperatures and in contact with oil or petrol. The parts of ignition cable can be shown as in Figure 2.4 there are some kinds of ignition cable in the market, they have different color, resistive material, insulation, but they have the same principle. Ignition leads are connected to ignition coil and spark plug with its two terminals, its metal contacts touch the contact of ignition coil and connection terminal of spark plug; and high voltage flows through the core of ignition cable. There are a inner insulation used to prevent high voltage to jump to ground, a metal bread to eliminate magnetic field and a outer jacket to protect ignition lead from working conditions and provide extra insulation.

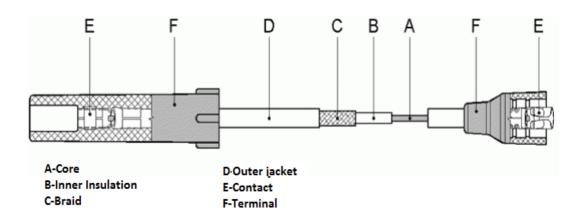


Figure 3.4: Parts of an ignition cable

As mentioned in the part related to spark plugs, electro-magnetic compatibility is an issue should be worked on in ignition cables, too. Wherever electric current flows, electromagnetic fields are formed, as for example in mobile phones and radio waves. Such electromagnetic fields also occur during ignition. They increase considerably in intensity at the time of each "spark breakaway" on the center electrodes of spark plug which results in strong voltage peaks along the lead. However, since strong electromagnetic fields can cause disturbances in electronic devices-such as the radio, engine or transmission control units or the ABS-they have to be kept within a non-damaging range, to lower electromagnetic field magnitude, the ignition leads are equipped with electrical resistors, to limit voltage peaks during spark breakaway and discharge of the ignition coil. The new design engine which is used in our test set-up is suitable for the direct ignition system, so the usage of ignition cable and electromagnetic interference caused by the ignition cables can be eliminated.

There are different types of ignition leads, they differ according to the materials used for the conductor and the type of resistor required for interference suppression. As seen in Figure 3.5, there are kinds of NGK ignition leads, they are copper ignition leads with interference suppression resistor in the connector, carbon resistor ignition leads and ignition leads with inductive resistor.

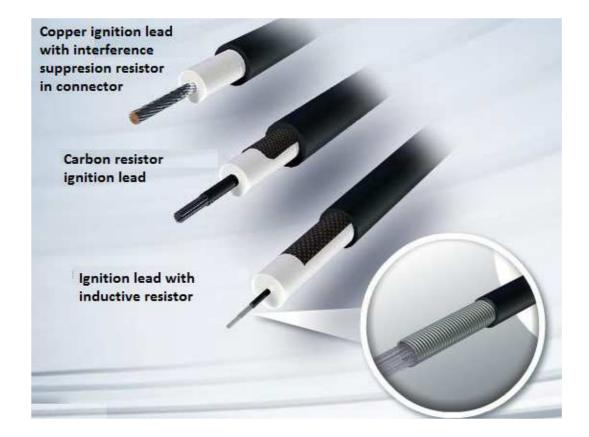


Figure 3.5: NGK ignition lead types

In the ignition leads with copper core, the copper formed as tin-plated, this form protects the copper from oxidation. The core is enclosed in a silicone shell for increased electrical insulation to prevent misfiring. The outer insulation increases insulation and protects the lead against temperature, oil and petrol. These types of ignition leads are not equipped with their own interference suppression resistor, but it contains a resistor in the spark plug and coil connector. Its resistance is between 1 and 6.5 k Ω . Another ignition lead type is carbon resistor ignition lead. Inside of this type ignition leads; there is braided carbon impregnated fiberglass. This fiberglass core is surrounded by two silicone layers and fiberglass fabric. The inner insulation made of silicone provides for stability and electrical insulation. The fiberglass fabric increases the tensile strength, the outer insulation which is made of silicone can withstand high temperatures and resistant to petrol and oil. This type of ignition leads have interference suppression resistance is usually between 10 k Ω -23 k Ω per meter. The last ignition lead type is ignition lead with inductive resistor. This type of ignition leads also have a fiberglass core, over the fiberglass core there is a

conductive and magnetic silicone layer, around which stainless steel wire is wound. As in a coil, inductive voltage occurs here; the coil wire picks up and delivers energy. As a result the inductive voltage is internally cancelled through the lead. And they have silicone and fiberglass layers to increase electrical insulation; they also have outer insulation to withstand high temperature, oil and petrol. This type of ignition leads have 1,8 to 2,2 k Ω suppression resistance range.

In our system, Bougicord Class B ignition leads are used. The properties of our ignition lead is black color, \emptyset 7mm outer diameter, maximum working temperature 100 °C, minimum working temperature -30 °C, silicone outer jacket and 5,6 k Ω resistance. This type of ignition lead is used for general applications and easy to find in the market. The properties are pretty good and enough for our application.

3.1.3 Induction Coils

A spark can arc from centre electrode to ground electrode only if a sufficiently high voltage is applied. In a typical spark discharge, the electrical potential across the electrode gap is increased until breakdown of intervening mixture occurs. Ionizing streamers then propagate from one electrode to the other. The impedance of the gap decreases drastically when a streamer reaches the opposite electrode; and the current through the gap increases rapidly. This stage of the discharge is called as "breakdown phase". The next main phase is "arc phase", in this phase thin cylindrical plasma expands largely due to heat conduction and diffusion and, with inflammable mixtures; the exothermic reactions which lead to a propagating flame develop. The final phase is "glow discharge", in this phase the ignition coil dumps its energy into the discharge circuit. There are also some minor phases; such as predischarge and transition phase. As it can be easily understood, they are transition phases between main phases. The figure below shows voltage current variation simply during spark discharge, too small time interval for the phase. The glow discharge phase has the lowest power level (~10W), but the highest energy (30 to 100 mj), due to its long discharge time.

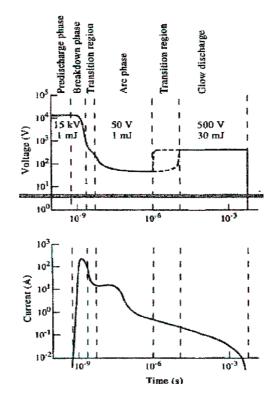


Figure 3.6: Variation of voltage and current during spark generation

As seen in the Figure 3.6, there is a need of high voltage around 18000 to 24000 volts to initiate spark discharge. To achieve this high voltage there is a special part, induction coil. An induction coil is formed by two coils of insulated copper wire wound around a common iron core. The first coil, called "primary winding" is composed of around few (tens or hundreds) turns of coarse wire. The second coil called "secondary winding" is composed typically of many (thousands) turns of fine wire.

Their working principle is based on Faraday's Law. According to the law, any change in the magnetic environment of a coil of wire will cause a voltage(emf) to be induced in the coil. No matter how the change is produced, the voltage will be generated. If any current flows through the primary winding, it creates a magnetic field. Because of the common core, most of the primary's magnetic field couples with the secondary winding. The primary winding behaves as an inductor, storing energy in the associated magnetic field. When the primary current is suddenly stopped, the magnetic field rapidly collapses. This change in the magnetic field cause a high voltage pulse to be developed across the secondary terminals through electromagnetic induction. Because of the large number of winding turns in the secondary

coil, the secondary voltage pulse is typically many thousands of volts compared to the first winding. Figure 3.7 below shows an old fashioned ignition coil.

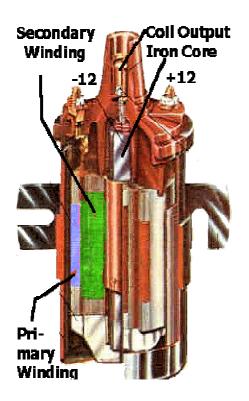


Figure 3.7: Old fashioned Ignition Coil



Figure 3.8: Delphi Pencil Coils

As you see in the figure, primary winding is on the outside; the secondary one is on the inside and has a longer length. And there is a common center core with two open ends; it also increases magnetic flux losses. This ignition coil is an old fashioned one, now there are many types of ignition coils in the market. All of them have different shapes according to their design considerations, but all of them are based on the same working principle. In modern ignition systems, the ignition coils are getting smaller to achieve more compact engine sizes. These new generation ignition coils can be directly mounted on spark plug while eliminating ignition leads; they are called pencil coils and plug top coils. These types of coils have some benefits such as magnetic noise reduction, increases reliability, high accuracy, lower mass and sizes etc. These ignition coils on the left side, Figure 3.8 are example of new generation ignition coils; their design consideration is taking advantage of unused space found above conventional spark plug.

Their compact size enables them to fit on spark plug hole which varies between 22mm to 29.1 mm. Their energy rates also changes between 35 mj to 80 mj according to their sizes. Another new generation ignition coil type is plug top coil. This type of coil is designed to be used when packaging constraints prevent the use of pencil coils (spark well inside diameter <22 mm), also their energy ranges are higher than pencil type coils, between 35 mj to 100 mj. Figure 3.9 shows plug top coils.



Figure 3.9: Delphi Plug Top Coils

These two types of new generation coils are good example to understand design consideration of new generation ignition coils. Another design consideration is ease of control of the system, in wasted spark systems; one coil serves two spark plugs (Two coils for 4-cylinder engines; three coils for 6-cylinder engines.). In this arrangement the coil generates two sparks per cycle to both cylinders. The fuel in the cylinder that is nearing the end of its compression stroke is ignited, whereas the spark in its companion that is nearing the end of its exhaust stroke has no effect. The wasted spark system is more reliable than a single coil system with a distributor and less expensive than coil-on-plug. Where coils are individually applied per cylinder, they may all be contained in a single molded block with multiple high-tension terminals. This is commonly called a coil-pack, Figure 3.10 shows an example coil pack designed for a 4-cylinders engine with wasted spark ignition system.



Figure 3.10: Delphi Waste Spark Pencil Coil Pack

In our test set-up we have used wasted spark ignition coil, they had been designed to serve two spark plugs at the same time. Our ignition system is not a wasted spark ignition system but we have two cylinders at compression cycle at the same time so we need two sparks simultaneously. The ignition coils which are used in our system are Mako ignition coil is used, as in the Figure 3.11 it is designed for wasted spark ignition systems. There are some materials which are used in ignition coils to provide insulation; this ignition coil is filled with epoxy resin to provide insulation. This ignition coil is used in the system because it is widely used in automotive industry, so it is cheap and easy to find in the market.



Figure 3.11: Mako ignition coil which is used in our system

3.2 Igniter Circuits

As mentioned before, ignition coils are composed of two coils, they are primary and secondary windings. When a current flows through the primary winding, it creates a magnetic-field; if the current s suddenly stopped the magnetic field rapidly collapses. This change in the magnetic field cause a high voltage pulse to be developed across the secondary terminals through electromagnetic induction, this is the working principle of our ignition coils. To suddenly stop the current, we need a breaking system. Though there are different types of ignition system, the use of a breaking system is consistent.

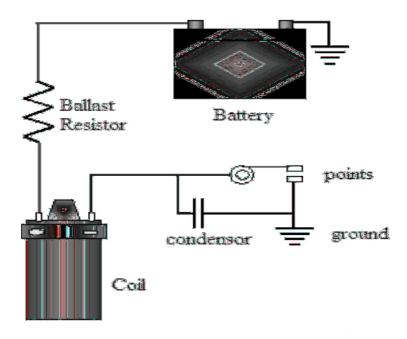


Figure 3.12: Typical point type ignition system

The Figure 3.12 is a typical point type ignition. The conventional breaker point-type ignition system has been in use since the early 1900s. In this system primary circuit of the ignition coil receives power from the battery through a resistor. The power is grounded through closed ignition points in the distributor. Current flows through the windings of the primary coil, creating a magnetic field. When the points are opened by the distributor cam. By touching of the distributor cam, the current's electrical circuit is broken, collapsing the magnetic field. The force from the collapse crosses the windings of the secondary coil and creates an electrical current within them. The current flows into the distributor cap and eventually into the spark plugs, all in a split second. As it can be understood from the Figure 3.12, the early ignition systems uses mechanical contacts to stop the current in the primary winding, there are some disadvantages of this system such as maintenance, difficulty in adjustment; wearing caused from arc and mechanical contact, poor ignition timing and unreliability. For this reason advance in the ignition systems have replaced mechanical contacts with various sensors, such as camshaft position sensor and crankshaft position sensor and some dedicated IC's. Figure 3.13 shows a schematic view of a new generation distributorless type ignition system working principle.

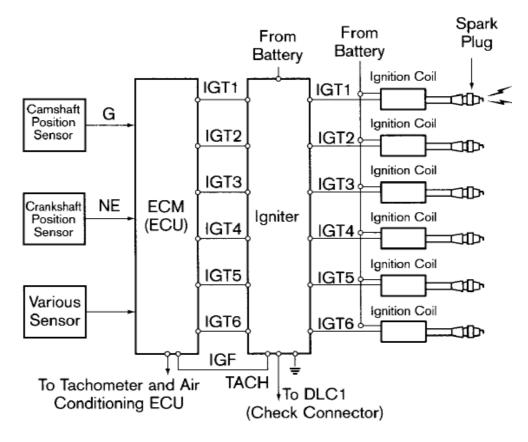


Figure 3.13: Toyota 1 MZ-FE 94 Direct Ignition System (DIS).

As seen in the Figure 3.13, there is a circuit called igniter, it receives ignition timing signals from ECU for each ignition coil and open or close the current to primary winding of ignition coil. The igniter circuits use transistor, mosfet or dedicated IC's to trigger primary voltage of the ignition coil. In our system, the igniter circuit is based on microcontroller, PIC16F628A and the other main components are mosfet, IRF540N and optocoupler, 4N35. The commercial igniter circuits have duties such as receiving ignition timing signals from ECU, drive ignition coils and ignition detecting, for these purposes to use a microcontroller will be beneficial. Some properties of PIC16F628A are important for our application, it have such properties: 20MHz maximum operating frequency, 2048 words flash program memory, 224 bytes memory, 128 eeprom memory, 3 timer modules, 2 comparators, 1 capture/compare/PWM module, USART serial communication protocol, 10 interrupt sources and 16 I/O pins [2], these properties are given in Table 3.1. The most important properties of optocoupler for our application is turn-on and turn-off time, they are typically 7 us (max 10 us), Table 3.3. The properties of IRF540N related to

our application is: continuous drain current at 10 volts gate-source voltage is 33 A, turn on delay time is typically 11 ns, turn-off delay time 39 ns and rise time 35 ns [3] as given in Table 3.2. These properties are pretty good for our application.

Max.	Flash	RAM	Timer	Capture/	Serial	Interrupt	I/O	Eeprom Comparator	
Freq.	Memory			Compare/	Com.	Sources		Memory	
				PWM					
20	1024	224	3	1	USAR	10	16	128	2
MHz	Words	Bytes			Т			Bytes	

Table 3.1: The related features of PIC16F628A

Table 3.2: The related features of IRF540N

Continous Drain	Turn-on Delay Time	Turn-off Delay Time	Rise Time	
Current(Vgs @10V)				
33 A	11 ns(typ.)	39 ns(typ.)	35 ns(typ.)	

Table 3.3: The related features of 4N35

Turn-on Time	Turn-off Time
10 us (max)	10 us(max)

There are eight igniter circuits in our ignition system, they receives ignition timing signal from the main circuit. The ignition timing signal is in the form of 0-5V square wave and the igniter circuits are triggered on the rising and falling edges of the signal. To create a spark, the ignition coils should be charged for a while this is our dwell time, it begins with the rising edge of the ignition timing signal ends with the falling edge. The triggered mcu, PIC16F628A, uses the optocoupler to drive the mosfet, so we can isolate the microcontroller from high voltage driving mosfet. The igniter circuit which is used in the system is shown in Figure 3.14

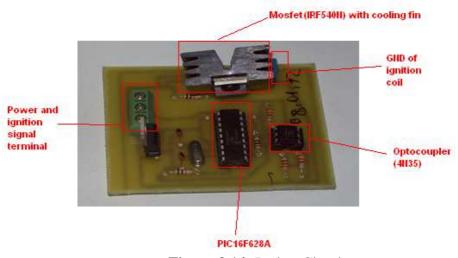


Figure 3.14: Igniter Circuit

Figure 3.15 shows the schematic view of igniter circuit which is designed with ORCAD 9.0; it will be beneficial to understand working principle of the circuit. The microcontroller unit which is soldered on the igniter circuit is programmed to detect ignition timing signal on pin B5 continuously. When it detects the high state of pin B5 (it means it is the start of ignition), it can trigger the optocoupler to drive the mosfet, pin B0 is used to drive optocoupler via 330 Ω resistor. It keeps pin B5 at high state until the falling edge of the ignition timing signal. Optocoupler works as follows. When enough current flows through the anode and cathode pins, it lets the current flow from the collector pin to the emitter pin. The current which should flow through the anode and cathode pins is so small, so a microcontroller unit can supply this current. This working principle of optocoupler is used to supply 12V to the base of the mosfet which is required to drive the mosfet. The collector pin of the optocoupler is connected to 12V; and when the current flows through anode and cathode pins (this current is supplied by PIC16F628A via pin B0), 12V flows to base of the mosfet (pin 3 in the Figure 3.15) via collector and emitter pins of the optocoupler, and this is the starting point of the spark generation process. The induction coils which are used on the system are connected as in Figure 3.14. Positive terminal of the primary winding is directly connected to +12V; and ground of the primary winding is controlled by the igniter circuit with mosfet. When the required voltage which is 12V in the igniter circuit, is applied to base of the mosfet, it lets current flow through the primary winding. As seen in Figure 3.15, the igniter circuit has a connector to connect the GND terminal of the induction coil; the connector is connected to the drain pin (pin 1 in Figure 3.15) of mosfet and when the mosfet is triggered, it will let the current from drain pin to GND of the system [4]. This flowing current is relatively high so a cooling fin is assembled on the mosfet as seen in Figure 3.15. And, the PCB layout of the igniter circuit is given in Figure 3.16. (The figure is the bottom layer and board edge of the PCB and the PCB is one sided.)

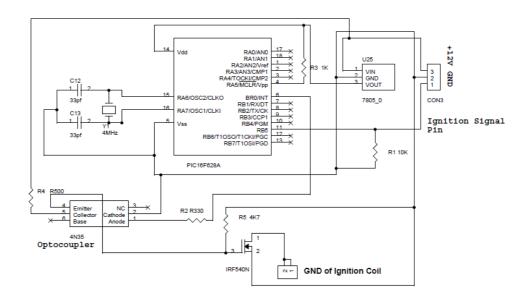


Figure 3.15: Schematic view of igniter circuit

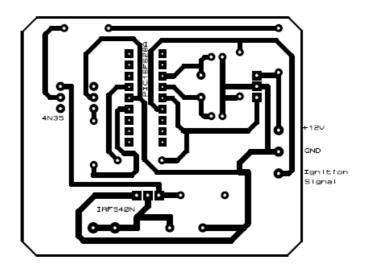


Figure 3.16: PCB layout of the igniter circuit

3.3 Control Circuits

As it is understood, the igniter circuits are slave circuits, they start ignition when an ignition signal comes from the main circuit (ECU) as seen in Figure 3.13, Toyota 1 MZ-FE 94 Direct Ignition System (DIS). In our system, we have a PIC16F877A based master circuit, to control the other slave circuits. The most important component of the circuit is PIC16F877A, it is a high performance risc cpu by Microchip [1], and it is very popular it means there are thousands of source codes related to this microcontroller on the internet. The important specifications of the mcu for our application are given below in Table 3.4.

Max	Flash	Data	EEPROM	Interrupts	I/O	Timers	Serial	10-
Operating	Program	Memory	Memory		Ports		Communication	bit
Frequency	Memory	(bytes)	(bytes)					ADC
20	4K	368	256	15	Ports	3	MSSP, USART	8
MHz					А, В,			
IVIIIZ					C, D,			
					Е			

Table 3.4: The features of PIC16F877A

As seen in the Table 3.4, it can work at 20 MHz frequency it means 5000000 cycle/second (200 nanosecond instruction executions). Also it has five I/O ports, serial communication modules and eight analog to digital conversion channels, these features are enough for our application.

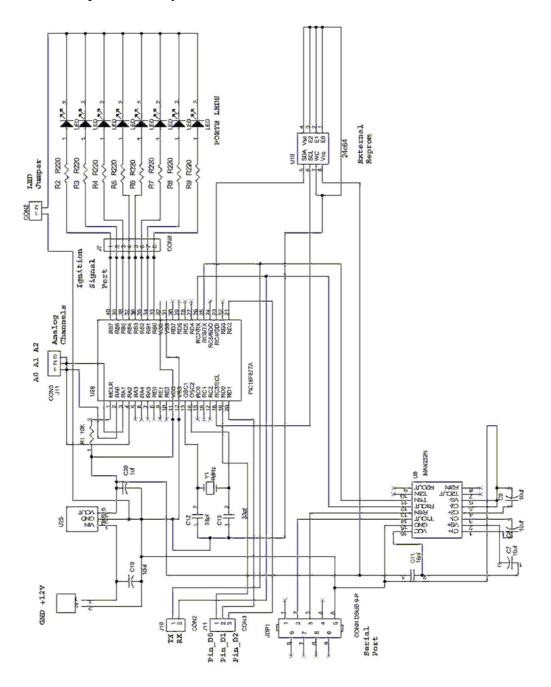
In our system, the rpm value and cooling temperature will be used as inputs to determine advance angle and initiate ignition. These values will be read in analog forms, so the main circuits should have connections for analog channels. The control circuits will communicate with each other via master slave serial communication, so the control circuits will have RX and TX connections. (RX and TX pins of microcontrollers are used for serial communication) [26]. Also, those pins should be connected to RS-232 port via max232, because we may need to communicate the control circuits with PC to upload advance angle data. The igniter circuits will be triggered by logic ignition timing signals of control circuits, so the control circuit

should also contain I/O pin connections and light emitting diodes to debug the source codes which are written for control circuits. Engine control circuits have external eeproms to store advance angle data, so the control circuits should have an external eeprom memory. In the light of required features which are stated above the control circuits are designed, there are two identical control circuits (they are designed identically to reduce cost and time required for designing), but their duty, so their source codes will be different (these control circuits will be called as main control circuit and secondary control circuit according to their duty). Figure 3.17 shows schematic view and Figure 3.18 shows PCB layout of the control circuits. As seen in the Figure 3.17, there are three analog channels; these channels will be used to measure analog rpm value and cooling water temperature. The circuit has max232 and serial communication port which may be used to communicate with PC; and has RX and TX pin connections, these pins will be used to communicate the control circuits with each other. The circuits have external eeprom memories which are used to store advance angle data as look-up table. In our system, 24C64 series eeprom is used to load look-up advance table, the 24C64 eeprom provides 65536 bits electrically erasable and programmable read only memory, it means we can write 8 bit advance data to 8192(13 bit) addresses. Also, it supports I2C and SPI communication protocols. Main circuit uses cooling water temperature and rpm value as inputs to figure out the advance angle. The cooling water temperature is measured via one of the analog input pins shown in Figure 3.17 and converted into digital form by 10-bit analog to digital conversion module of the main control circuit. The source code of main control circuits is written to read rpm value in 8-bit digital format via serial communication, so there is a need for a circuit to measure rpm value and format it into 8-bit form. Our secondary circuit is dedicated to measure rpm and formats it into 8-bit form. The secondary control circuit sends rpm value to the main circuit via serial communication with RX and TX pins, the mcu PIC16F877A has Universal Synchronous Asynchronous Receiver Transmitter (USART) module which is one of the two serial I/O modules. (USART is also known as a Serial Communications Interface or SCI.) [26]. This module can be configured as a fullduplex asynchronous system that can communicate with peripheral devices, such as CRT terminals and personal computers or it can be configured as a half-duplex synchronous system that can communicate with peripheral devices, such as A/D or

D/A integrated circuits, serial EPROMs, etc. In our system synchronous mode communication is used, this is a one way communication because the secondary circuit receives no data from the main circuit. When we look at the communication mode, the main circuit is set as slave, the secondary circuit is set as master, and it means secondary circuit transmits data, the main circuit receives that data, but this communication starts whenever the main circuit sends a ready signal to the secondary one.

Actually, the main circuit and the secondary circuit have the same hardware except 24C64 eeprom, because reading advance angle value from a look-up table is the duty of the main control circuit(secondary control circuit also has connections for 24C64, but it will not use the eeprom memory during operation). As seen in the Figure 3.18, the external eeprom is connected to PIC16F877A with its SDA and SCL pins. SDA is serial data I/O pin and SCL is serial clock input of the external eeprom [26]. Those pins are connected to pin C4 which is used as serial data I/O and pin C3 which is used as serial clock output of PIC16F877A. The connection which is given above will be used to read data from external eeprom memory via I2C protocol of MSSP module. The secondary control circuit will count the square wave output of position sensors to determine crank shaft angle and receive ready signal from the main control circuits, so the D0, D1 and D2 pins which is seen in figure 3.17 will be used for these purposes. The control circuits have connection port for PORTB and light emitting diodes connected to PORTB. The PORTB of main control circuit is used to send ignition timing signals to igniter circuits. The leds connected to this port will be used to simulate ignition timing signals and debug the source code.

The PCB layout of control circuits is given in Figure 3.18; these control circuits are manufactured by ironing method (commonly used by amateurs to manufacture circuit board). These circuits are also used to test control codes to check if they succeeded, but for the final design more professionally assembled and manufactured PCBs may be used. The PCB layout which is given in Figure 3.18 can be manufactured by professionals or standard PIC16F877A development circuits can be used. There is such a PIC16F877A development board (Altas yayincilik) in the market as seen in figure 3.19. The development board has all the necessary pins, connections, leds and external eeprom connection which we need in the control



circuits. To use this development board as control circuit will be beneficial because this circuit is professionally assembled and tested.

Figure 3.17: Schematic view of the main control circuit

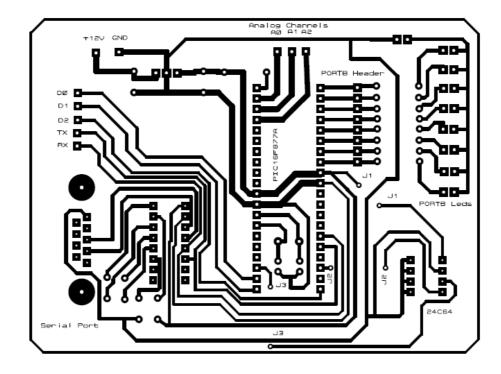


Figure 3.18: PCB layout of the main control circuit

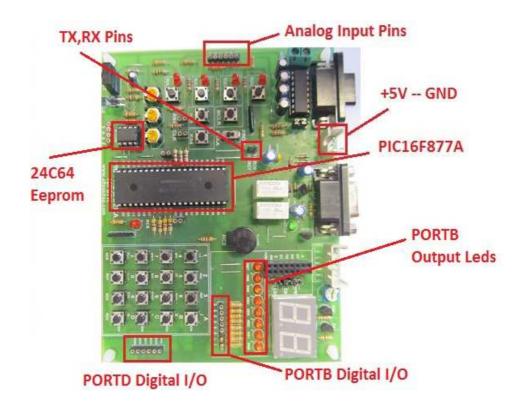


Figure 3.19: Main control circuit

3.4 Speed Measurement and Cylinder Identification

3.4.1 Magnetic Pick-up

The rpm value is measured with a sensor which is a variable reluctance magnetic pick up, Figure 3.20, it is a commercial product and it can be found easily as a spare part in the market.



Figure 3.20: Magnetic pick-up which is used in our system

This sensor is widely used in automotive industry because of its enduring structure and easy working principle. As seen in Figure 3.21, it is composed of a permanent magnet, a pole piece metal and a coil, the working principle is if a metal piece closes to the pole piece part it causes a change in the magnetic field and it induces a voltage in the coil, this induced voltage is observed with the signal wires as a AC form [30].

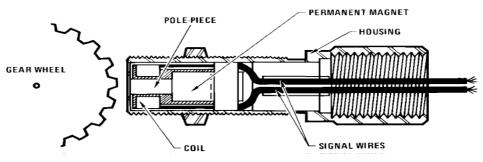


Figure 3.21: Typical Magnetic Pick up

3.4.2 Frequency to Voltage Converter Circuit

As stated before, the output of magnetic pick-up sensor is a useless ac signal, so to use the output you should shape it into square wave form or you should use frequency to voltage converter to get an analog signal. There is an integrated circuit in the market which is called LM2907, frequency to voltage converter; it is an 8-pins small integrated circuit. This integrated circuit is widely used in the automotive industry to get analog signal from the ac output of the magnetic pick up sensors. Figure 3.22 shows an example circuit of frequency to analog signal converter [30], this example circuit is the same with the circuit used in our application. After converting the ac signal to analog signal, the secondary control circuit converts it into 8-bit digital form by using A/D conversion module.

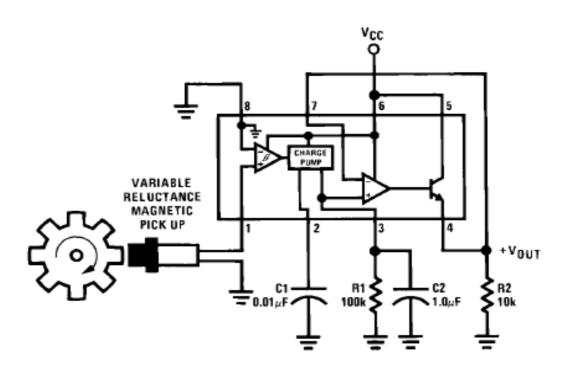


Figure 3.22: Basic Frequency to Voltage Converter.

Sensor, power, capacitor and resistor connections are shown in Figure 3.22, but the output voltage will be different for different capacitor and resistor combinations in the datasheet of LM2907 this situation is defined with an equation as follows [30]. $V_{out}=V_{cc} x f_{in} x C1 x R1 x K$ (K is the gain constant and typically 1) Eqn. 3.1 In frequency to voltage converter design, the resistor, capacitor and supply voltage is chosen to keep output voltage within 0-5V. So, according to Eqn. 3.1 circuit is designed in ORCAD 9.0 as in figure 3.23. The maximum output voltage is calculated around 4.8 V for 3000 rpm (4000 Hz for gear wheel with 80 teeth) in the design. This designed frequency to voltage converter circuit is manufactured with the PCB layout which is given in Figure 3.24 with ironing method.

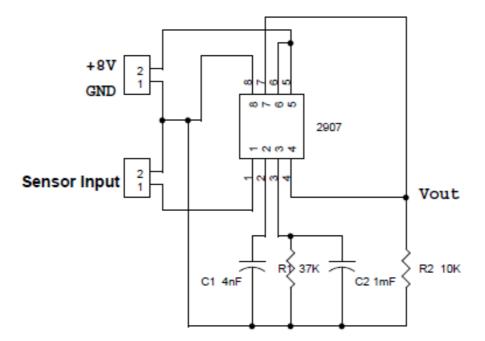


Figure 3.23: Schematic view of frequency to voltage converter circuit

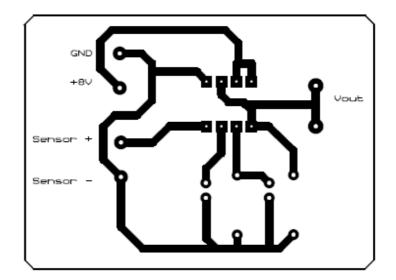


Figure 3.24: PCB layout of frequency to voltage converter circuit

3.4.3 Generation of Cylinder Position Signals

Another duty of the secondary control circuit is to send cylinder position signal to the main circuit, to do this job there are 2 secondary LM2907 circuits, these circuits converts the ac output signal of the magnetic pick up sensor to square wave, then the secondary control circuit easily counts square waves to determine crank shaft angle. There are two secondary LM2907 circuits which convert AC signals to square wave in our system; one of them is used to determine crank shaft angle as stated above and it is called secondary LM2907 circuit 1; the other one is used to detect first piston position and it is called secondary LM2907 circuit 2. The application circuit of LM2907 to convert AC signals to square wave [30] is shown in Figure 3.26.

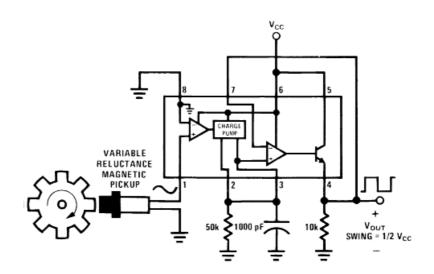


Figure 3.25: Square wave signal generator circuit (secondary LM2907 circuit)

As it is understood from the Figure 3.25, the magnitude of square wave is dependent on supply voltage. So the secondary LM2907 circuit is designed to have 0-5V square wave as in Figure 3.26.

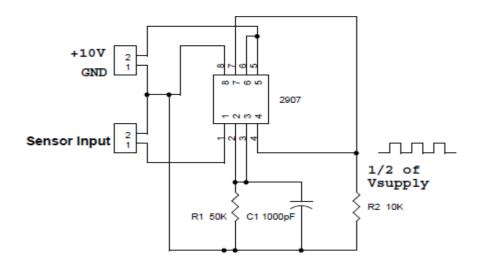


Figure 3.26: Secondary LM2907 circuit

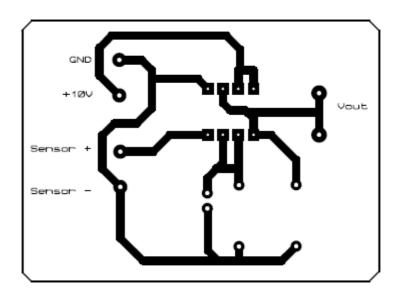


Figure 3.27: PCB layout of the secondary LM2907 circuit

There is a gear wheel which triggers the magnetic pick-up sensor as you see in figure 3.28, this gear wheel is used to determine engine speed and piston positions, the gear wheel which has eighty teeth to simulate an actual engine, and it means ten teeth per cylinder. There is a metal part mounted on the gear wheel it is an additional tooth and it is used to determine first piston position.



Figure 3.28: Gear wheel and driving system figure

The frequency to voltage converter circuit which is told in part 3.4.2 uses this gear wheel and outputs of crank shaft position sensor in Figure 3.28 as input. As seen in figure 3.28, gear wheel is driven with a belt and a motor, this motor is 0.36 kW AC motor and it is driven by Delta VFD 004L11A series ac motor driver. It is very useful for laboratory works because it has many parameters to change control settings and gives the operator permission to change these settings. For example you can control this driver with its digital keypad, its potentiometer, 0-10V input voltage, 4-20 mA input current or RS-485 communication port. Among these options to control motor speed, 0-10V input voltage option is suitable for us because we have a data acquisition card having analog output channels.

3.5 Data Acquisition and Control System

3.5.1 Data Acquisition Card and Its Accessories

One of the most important parts of the experimental set-up is data acquisition and control system. It contains a computer, control software, Advantech PCI 1716 data acquisition card, Advantech PLC-10168 wiring cable, PLCD-8710 wiring terminal board and a transmitter/receiver circuit.

The computer in the experimental set-up is a standard personal computer, we don't need a special computer for this set-up, all we need is a computer which it can run Delphi 4.0 software and has a PCI bus. The data acquisition card on the set-up is Advantech PCI-1716 100kS/s, 12-bit, 16-ch Universal PCI Multifunction Card, it has

16 channels single-ended or 8 channels differential or a combination of analog input, 12-bit A/D converter with up to 100 kHz sampling rate, programmable gain, automatic channel/gain scanning, onboard FIFO memory, 2 12-bit analog output channels, 16 channels digital input and 16 channels digital output and onboard programmable counter. These properties are acceptable for an experimental work.

The data acquisition card is a PCI type card, Figure 3.29, so we need special cable with connector and a terminal board for I/O connections. PCL-10168 cable and PCLD-8710 industrial wiring terminal board is used on the set-up, Figure 3.30. These are accessories for this card supplied by Advantech.

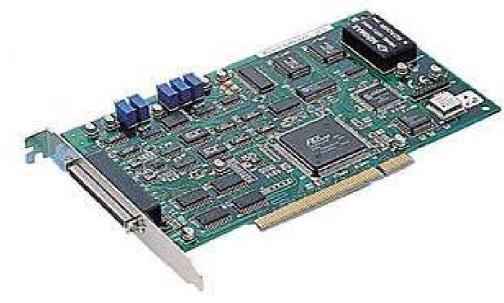


Figure 3.29: Advantech PCI-1716

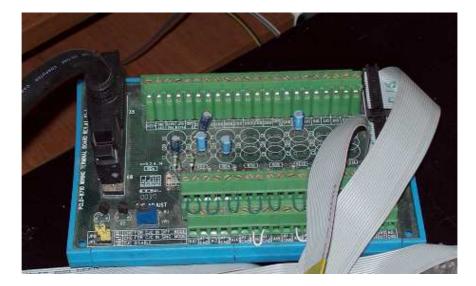


Figure 3.30: Connection terminal box and connector cable

The data acquisition card 16 digital outputs and 16 digital outputs as stated before, but to use these inputs and outputs in your experimental set-up you need another circuit because digital outputs are not enough to drive inductive loads and you should isolate digital inputs from bad signals, there is an interface circuit for this purpose. The circuit has four 74LS245 IC`s, this IC is a octal bus transmitter/receiver, they are used to isolate the data acquisition card from bad input signals. There are 16 relays on the circuit, they are driven by ULN2003A high voltage, and high current Darlington arrays each containing seven open collector Darlington pairs with common emitters. These interface circuits are triggered by output signals of the data acquisition card, with these interface circuit our data acquisition system have 16 isolated digital inputs and 16 relay outputs which is capable of driving inductive loads. Figure 3.31 shows interface circuit.

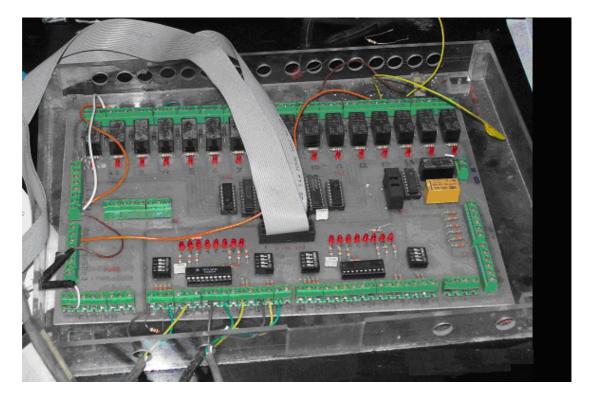


Figure 3.31: Interface circuit

Interface computer program which is necessary to control the hardware told above was developed with Delphi 4.0, this interface program is used for different experimental set-ups in the laboratory, so our program was added on the existing program. Figure 3.32 shows opening view of the program.



Figure 3.32: Opening view of the interface program

As it is used various experimental set-ups, there is a option to choose data acquisition card, our card is PCI-1716. The next step is choosing our experimental set-up; Figure 3.33 shows how we open our main page.



Figure 3.33: The next step to open our set-up page

Figure 3.34 shows how our main page looks like, we can control speed of the motor, scan digital inputs and play animation of our ignition system via this interface.

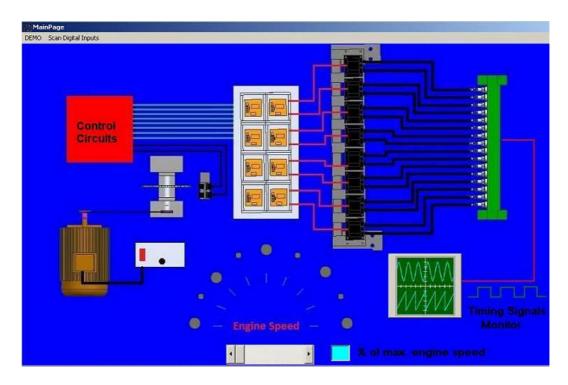


Figure 3.34: Main page of our control software

CHAPTER 4

EXPERIMENTAL METHOD

In this part of the thesis, experimental method and how the elements of the set-up which are told in previous chapter are used together will be stated. There are many circuits and their working principle, schematic view and PCB layout are given in the previous chapters, it will be helpful to review their working principles and duties in the set-up. There are 3 LM2907 circuits, one of them is designed as a frequency to voltage converter and the others are designed as square wave generator circuits. There are 2 position sensors; they are crank shaft position sensor and reference point sensor. The crank shaft sensor is connected to frequency to voltage converter LM2907 circuit; the aim of this connection is to measure engine speed as voltage. The crank shaft position sensor is also connected to one of the square wave generator LM2907 circuits. This connection is used to create 0-5V pulse for each tooth of the gear wheel in Figure 3.28. So, control circuits count the pulses and determine the crank shaft angle and identify the cylinder positions. We should have a reference point to start to count the pulses; this is held by reference point sensor and the other of square wave generator LM2907 circuits. Control circuits detect the output of that square wave generator circuit to start to count the pulses. The reference point is the position of the first cylinder. Secondary control circuit is dedicated to measure the speed by using output of the frequency to voltage converter circuit and send rpm value in 8-bit format to the main control circuit and identify cylinder positions (by detecting the reference point and counting the output pulses of square wave generator circuit) and send them to the main control circuit. The duty of the main control circuit is to detect the cylinder position signals (0-5V pulses) coming from the secondary control circuit and add advance angle value to the cylinder position signals and trigger the igniter circuits. The connections for all the circuits are given in Figure 4.6, and examining this figure will be beneficial for understanding the connections and duties of the circuits.

4.1 New Design Engine

It will be helpful to state important points of the study and test engine. This ignition system set-up is constructed for a special kind of engine, so the first step is to understand the working principle of the engine. The engine has 8 cylinders arranged radially on the engine, and there are 2 pistons for each cylinder it means there will be ignition at respective sides of common cylinders. The engine has 2 special axial cams at the each side of the engine. Another important point is ignition order of the spark plugs, each side of the cylinder has ignition for each revolution of the engine unlike a conventional four strokes one, because there is one ignition in a cylinder for every two revolutions in a conventional 4-stroke cycle engine as in Figure 4.2. In other words, crank shaft angle of the new design engine gives which piston is at which stroke. Figure 4.1 shows parts of our new special engine.

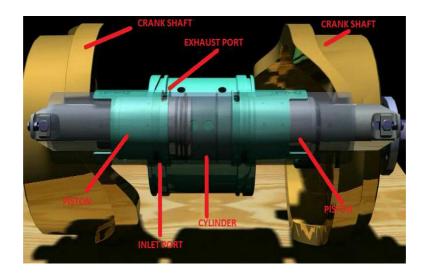


Figure 4.1: Engine for which the ignition system set-up was constructed

Figure 4.2 shows four stroke cycle of a conventional internal combustion engine, as shown in the figure it is impossible to determine the firing order with only crank shaft angle (except wasted spark ignition). For example, the crank shaft angles of compression stroke and exhaust stroke are the same in the figure. So to determine the correct ignition order there will be need to another sensor output.

Our study is based on a special type of engine and its firing order is different but physics of a combustion process is the same so the different part of our ignition system is about firing order and its determination.

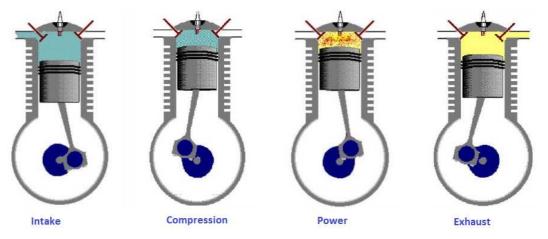


Figure 4.2: Four strokes of an internal combustion engine

4.2 Working Principle of the System

In this part of the thesis, the working principle of the system is going to be given. The duties of the circuits and their relations with the other circuits are going to be shown and told. The working principle is not going to be given operation by operation, the operations are going to be grouped according to the circuits realizing the operations, but it is going to be in an order. To follow the operations easily, it will be helpful to look at Figure 4.3 the flowchart of the control algorithm of the system.

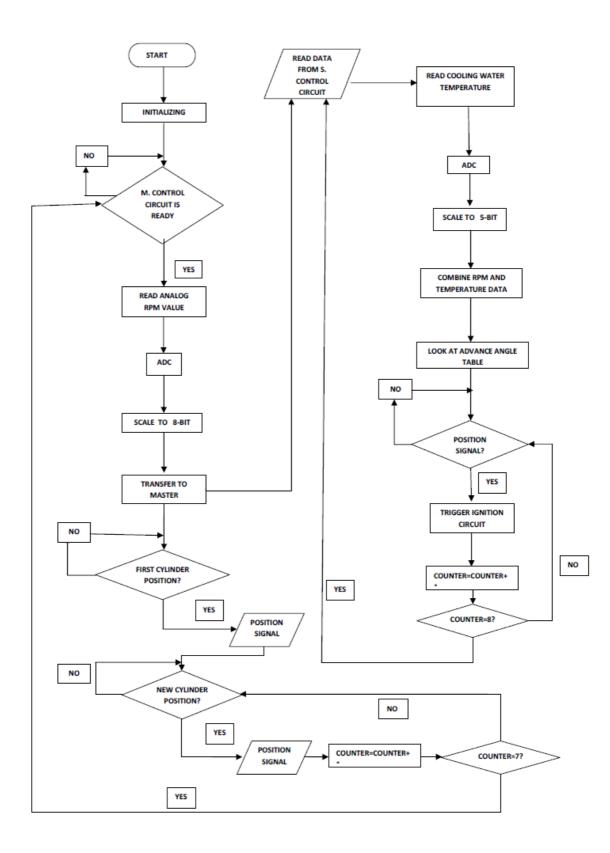


Figure 4.3: The flowchart of the control algorithm of the system

The connection diagram in Figure 4.4 shows the exact connection of the circuits, they are not symbolic connections. It will be helpful to understand the control algorithm, operation order and the circuits in relation.

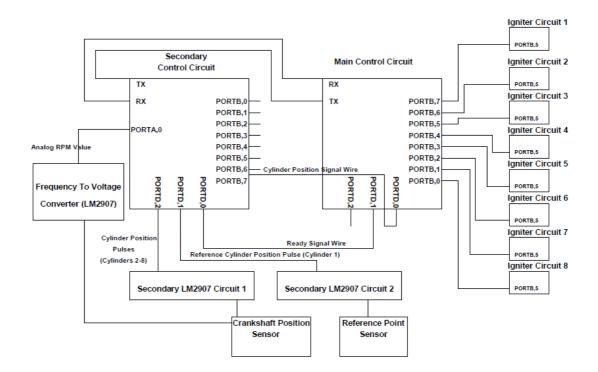


Figure 4.4: Connection diagram of the circuits

Figure 4.5 shows the operation order and the circuits realizing the operations. The system should be examined operation by operation, the operations and their order can be followed with Figure 4.5 and the algorithm of the operation can be seen in figure 4.3; and the wire connections for the operation can be seen in Figure 4.4, so the Figure 4.3, 4.4 and 4.5 should be examined together.

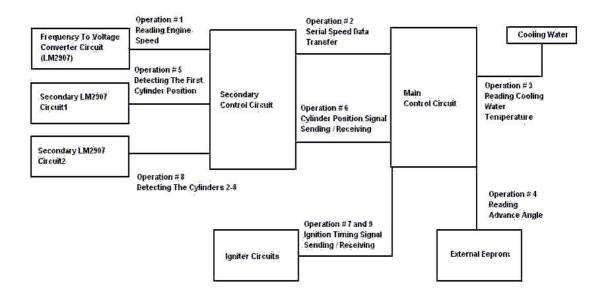


Figure 4.5: The operation order and the circuits realizing the operations.

4.2.1 Speed Measurement and Piston Position Determination

4.2.1.1 Position Sensors

Figure 4.6 shows a four stroke four cylinders combustion engine and its front view; there are a gear wheel with a missing tooth on the crank shaft and a pick-up coil type sensor. These components are used to determine position of the crank shaft and speed of the engine.



Figure 4.6: A Four cylinder demo engine and its front view

As stated before, the crank shaft position sensor is not enough to determine the correct ignition order, so we need another sensor output; this sensor is camshaft position sensor. Figure 4.7 shows typical outputs of crank shaft position sensor and camshaft position sensor in a conventional crankshaft engine.

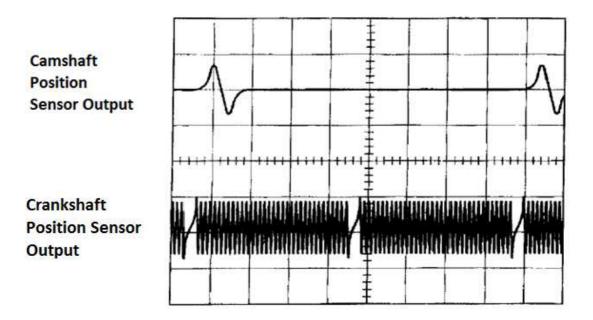


Figure 4.7: Typical outputs of position sensors

The periodic gap in the crankshaft position signal is because of the missing tooth in the gear wheel. The gap is used by control unit as a reference of the crankshaft position. When it is combined with the camshaft position signal, cylinder position and stroke can be determined. In our case, a missing tooth in the gear wheel will be enough to determine cylinder positions and strokes because the all strokes are completed in one revolution of the engine by the help of two axial cams, so the same operation is going to take place at the same crank angle in every revolution.

We have used an additional tooth instead of the missing tooth; the source code of control circuits will be simpler by this way. Figure 3.28 shows gear wheel, additional tooth and sensors. There are two sensors, crank shaft position sensor and reference point sensor. Outputs of position sensors in our system are shown in Figure 4.8, as you see in the figure there is no periodic gap in the crankshaft position sensor because we do not have any missing tooth. This signal is used to determine engine speed and crankshaft angle as told in the previous chapter.

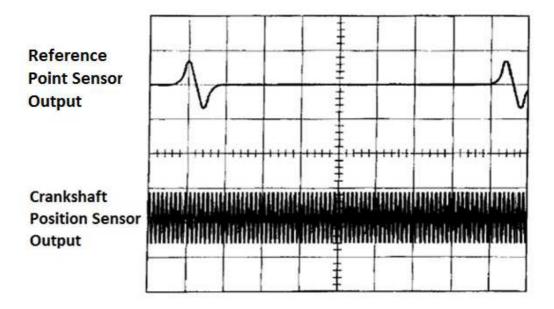


Figure 4.8: Outputs of position sensors in our system.

4.2.1.2 Speed Measurement

There are many steps in ignition process and, they repeat in each revolution of the engine. The first step is reading rpm (revolution per minute) and transferring it to the main circuit in required format, the output of crank shaft position sensor is used to read rpm value by using LM2907, frequency to voltage converter, based circuit as mentioned in previous chapter. Figure 4.9 shows typical application circuit of LM2907 to measure the engine speed. This circuit uses the crankshaft position sensor output as input, and converts it into voltage shown in Figure 4.9 as Vout.

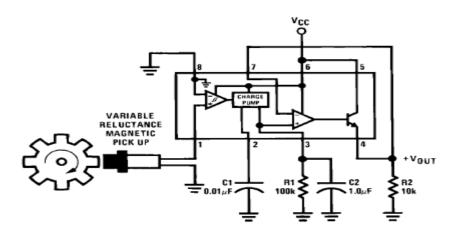


Figure 4.9: Typical application circuit of LM2907 to measure speed

The most important advantage of this circuit is that its output is in analog form, so whenever you want to read rpm the only thing to do is analog to digital conversion, you do not need to count any pulses or store any data to read speed. To determine speed of engine you may use sensors with digital output and count the teeth of gear wheel assembled on crankshaft, but you should count the teeth continuously it means another extra circuit. The main control circuit manages every operation in the system, so reading rpm voltage operation starts with ready signal of the main control circuit, the main circuit makes the pin high, PORTD,1 it means the main control circuit is ready for data transfer, after the secondary control circuit see the ready signal, it reads analog rpm signal (output of LM2907 circuit) and converts it into digital form, as given in the previous chapter the main and secondary control circuits are both based on PIC16F877A microcontroller, and it has 10-bit analog to digital conversion module, so analog to digital conversion of rpm signal gives two 8-bit variables. The main control circuit needs rpm value in 8-bit format, so the secondary control circuit makes required mathematical operations; they are 16-bit division and subtraction, to scale two 8-bit variables into one 8-bit form. Then the secondary control circuit sends 8-bit rpm data with USART synchronous master/slave communication with 500 kHz baud rate.

The main control circuit manages every operation in the system but during the serial communication it acts like slave because it just receives data. The serial communication takes place with the TX and RX connection as seen in Figure 4.3. The Figure 4.10 shows the operational view of the engine speed measurement

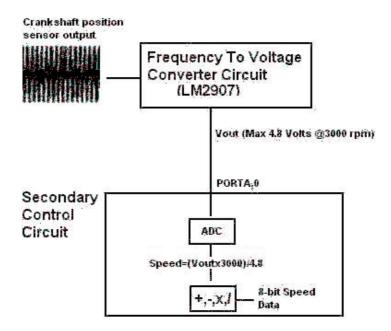


Figure 4.10: Operational view of the engine speed measurement

4.2.2 Piston Identification and Crankshaft Angle Measurement

The output of position sensors are low level analog signals, we shape it into square wave form to use them as a trigger signal in our microcontroller based secondary circuit. This job is done by secondary LM2907 circuits; this application of LM2907 is shown in Figure 4.11. There are two identical circuits in the system, one is for reference point sensor output, and another is crankshaft position sensor output which is also used to determine engine speed as seen in Figure 4.4.

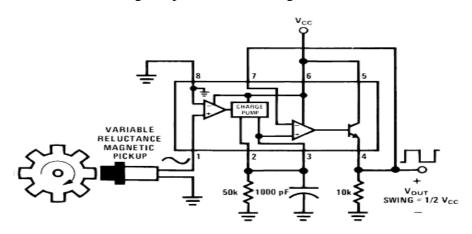


Figure 4.11: Secondary LM2907 circuit

The outputs of secondary LM2907 circuits are square form of the ac analog signals as seen in Figure 4.11. After the secondary control circuit sends the engine speed data to the main circuit in 8-bit format, it goes to the second step. This step is to find the reference point of the crankshaft and crankshaft angle, it starts with the reference point detection, because firing of spark plugs start with a reference point and continues sequentially. As stated before, reference point is our additional tooth and it is detected with reference point sensor. The pin PORTD,1 of the secondary control circuit is dedicated to detect reference point signal, when it receives the signal, the secondary control circuit makes PORTB,7 high for 20 µs this is first cylinder position signal; Pin PORTB,7 is connected to pin PORTD,0 of the main control circuit, as seen in figure 4.3 and it is triggered at the falling edge of cylinder position signal. Then secondary control circuit starts to count square waves of crankshaft position signal, PORTD,2 of the secondary circuit is dedicated for this purpose, if it counts ten pulses, ten pulses mean 45 ° rotation of crankshaft because the gear wheel has 80 teeth for 8 cylinders, it makes high PORTB,7 for 20 µs this is position of second cylinder, the secondary circuit repeats this process for seven times, then it goes to the initial point and wait ready signal from the main circuit for the next revolution. As it is told above, the main circuit communicates only with the secondary circuit for engine speed and piston identification.

Main control circuit uses cylinder position signals to create ignition timing signals. The gear wheel will be mounted on the engine as rotated 22.5° , it means the cylinder position signal gives the middle point of two cylinder. And the advance value will be added on this point to find the required position of the ignition. Figure 4.12 shows the operational view of the piston identification and crank angle measurement.

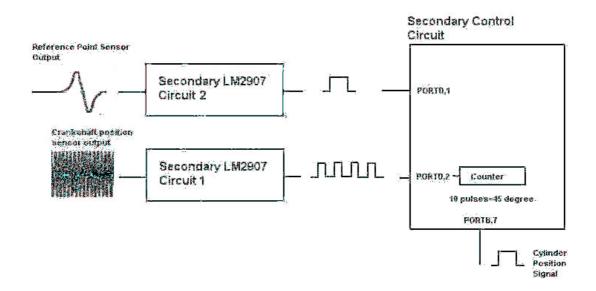


Figure 4.12: Operational view of the piston identification and crank angle measurement

4.2.3 Receiving Speed Data and Reading Cooling Water Temperature

There are many factors such as engine load, speed, temperature, richness of air-fuel mixture etc. which affect the combustion process in the cylinder. Ignition system shall be designed to adapt itself to changes in these variables; our ignition system setup is designed to use engine speed and temperature to arrange ignition point. There are many parameters which can be used as input to arrange ignition point such as pressure of the inlet manifold or exhaust gas temperature, but for the time being engine speed and cooling water temperature is enough to develop ignition control system for the laboratory.

The first thing which the main control circuit does after initialization is sending ready signal to the secondary circuit with its pin PORTD,1 and waiting for data transfer, if there is a problem in the secondary circuit or data transfer wiring, the main circuit will keep waiting for data transfer, but a timer can be used to limit waiting time for the data transfer and if there is not data transfer during that time, previously transferred data can be used. After receiving engine speed data, it reads cooling water temperature sensor output and it converts it into digital form by using analog to digital conversion module, this module has 10-bit resolution and our system uses

cooling water temperature in calculations as 5-bit format, so the main circuit makes necessary 16-bit calculations to scale digital cooling water temperature data into 5bit.

4.2.4 Selection of Advance Angle and Ignition Timing Signals

The main duty of the main circuit is to determine the ignition timing and send the ignition timing signals to the slave igniter circuits. The main control circuits receive cylinder position signals at pin PORTD,0 from the secondary control circuit. In our system, cylinder position signal shows the middle point of the two cylinders; this is our reference point to calculate ignition point. The ignition timing signals are advance angle added form of the cylinder position signals. Figure 4.13 shows the physical meaning of the advance angle value, the advance angle value is the required time to travel from the cylinder position to the ignition point. There are 16 ignition points in our new design engine, but the two ignitions take place at the same time, so we need 8 position signals as seen in Figure 4.13. The two ignitions taking place at the same time are generated by the induction coils with two high voltage output, so 8 igniter circuits and 8 induction coils are used in the system.

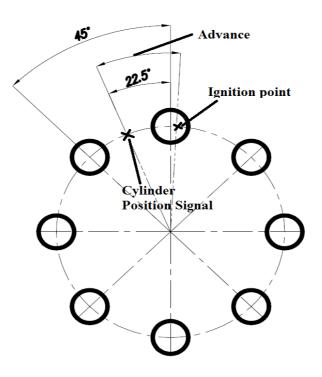


Figure 4.13: Advance angle value

Ignition advance is the number of degrees before or after top-dead-centre (TDC) that a spark occurs in conventional crank shaft engines. The reason for ignition advance is that the spark needs to be timed so that the point of peak combustion pressure is when the piston is just beyond TDC.

If the point of peak combustion pressure is too early and before TDC the pressure wave will slow down the speed of the piston traveling up towards it, and may cause detonation (knocking) which is very damaging to the engine. If the point of peak combustion pressure is too late, the pressure wave will chase the piston as it travels back down the cylinder in the combustion stroke and most of the energy will be lost. This advance angle changes during the engine operation due to engine load, engine speed, fuel, temperature etc., for example as the speed of the engine rises, the ignition advance angle needs to increase. The philosophy behind this: because the time to burn an unchanging air/fuel mixture is approximately constant. If the ignition advance angle were kept the same, the point of peak combustion pressure would move further and further into the combustion stroke losing more and more power. Therefore the ignition advance needs to be increased to bring the point of peak combustion to just beyond TDC. The ignition advance decreases while engine load increases, because the amount of time taken for a fuel/air mixture to burn mainly depends on the richness of the fuel mixture. When the engine is under low load with a lean air/fuel mixture the degree of ignition advance will need to be large to allow for the slow combustion of this mixture. Conversely when the engine is under load a richer air/fuel mixture is used to provide more power. This richer mixture has a faster combustion time so the degree of ignition advance needs to be reduced to keep the peak combustion pressure just beyond TDC, the temperature also do the same effect with the engine load. Those possible problems are valid for conventional crank shaft engines, because the combustion process in the new design engine takes place in constant volume, one of its advantageous sides, and the advance angle should be calculated to find the ignition point in the constant volume area. But, the parameters which affect the advance angle will also affect the advance angle of the new design engine.

As it is stated above, the ignition advance angle is dependent on a few variables; during the operation it is impossible to calculate advance angles due to these variables. So in modern engines look-up tables are used to select suitable advance angle for specific engine operation conditions. These look-up tables contain experimental advance data and they are loaded to eeprom memories. Figure 4.14 shows advance angle map which is dependent of engine load and engine speed.

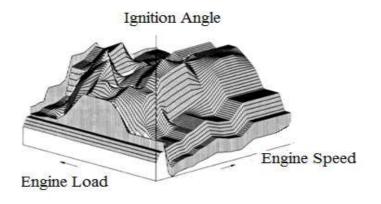


Figure 4.14: Advance angle map

In our system, 24C64 series eeprom is used to load look-up advance table, the 24C64 eeprom provides 65536 bits electrically erasable and programmable read only memory, it means we can write 8 bit advance data to 8192(13 bit) addresses, 13-bit address is divided as 8 bit + 5 bit in our application according to importance on advance. As seen in figure 4.15, the main circuit uses rpm value and cooling water temperature as eeprom address to select suitable advance angle from the look-up table, rpm value is the 8-bit address part (ADDRESSL) and cooling water temperature is the 5-bit address part (ADDRESSH) [26].

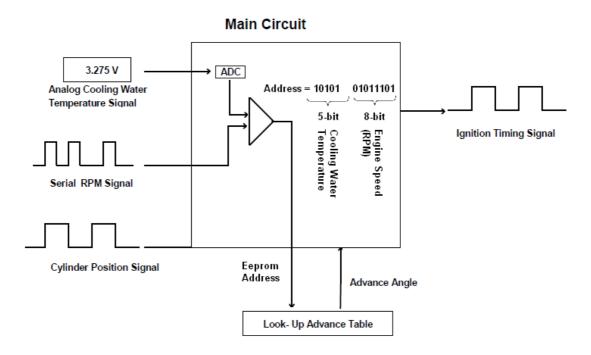


Figure 4.15: Operational View of the Main Circuit

(The values 3.275 V and 10101 01011101 are symbolic numbers). The required advance angle value for the engine speed and cooling water temperature in the address which the advance angle value will be read from, was loaded into that address before, this is the philosophy to load advance angle map into eeproms.

Selection of advance angle according to engine speed and cooling water temperature is told above, the advance angle value which is read from the eeprom is a time delay and this delay is added to cylinder position signal. The main control circuit program goes to wait for position signal of the first cylinder after it reads the advance angle value. When it detects the falling edge of the first cylinder position signal it waits for a moment, this moment is advance angle value which is read from eeprom memory, and then it sends ignition point (the falling edge of the ignition timing signal) to the first igniter circuit, and it repeats this process for eight times.

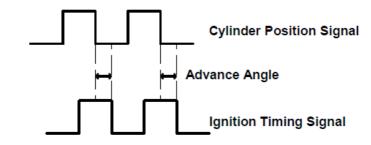


Figure 4.16: Ignition timing signals

The ignition timing signal is a square wave, when the main control circuit receives the cylinder position signal it makes its related pin high (ignition mode_0), after advance delay it makes the pin low and creates the spark with the igniter circuit. The point at which the pin is made high changed according to the engine speed, it is called dwell angle and it is going to be told in part 5.5.

For the time being, it is impossible to determine advance values, because advance angle values are determined after series of tests which is called calibration tests.

4.2.5 Receiving Ignition Timing Signal and Firing Spark Plugs

As stated in previous chapter, there are eight PIC16F628A based igniter circuits which are dedicated to receiving ignition timing signals and trigger induction coils. Ignition timing is determined by the main circuit according to advance angle, as seen in Figure 4.16, it is a square wave. In signals which are in square wave form, there are two reference points, rising edge and falling edge. Our igniter circuit detects its related input pin continuously to catch the rising edge of ignition timing signal, when it catches the rising edge it opens the way of current which flows through the primary winding of induction coil by driving mosfet via optocoupler. Then it starts to detect the related input pin continuously to catch the falling edge of ignition timing signal, when it detects the falling edge, it closes the way of the current suddenly to induct high voltage in the secondary winding of induction coil.

This high voltage jumps to ground via spark plug as a spark and ignition occurs. Figure 4.17 shows operational view of the igniter circuit.

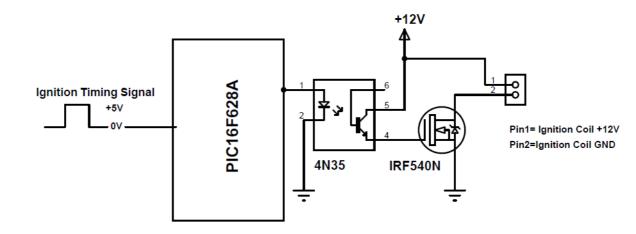


Figure 4.17: Operational view of the igniter circuit

CHAPTER 5

DESIGN CALCULATIONS

Control circuits which are used in our system are based on PIC microcontroller and the microcontroller units on the circuits are programmed in assembly language. Ignition is a fast process, so our ignition system should be fast enough to initiate ignition at the required time. In the circuits 4 MHz crystals are used as an oscillator; it means our circuits are able to make 1000000 operations per second; this operational speed is suitable for our application, but the control circuits convert analog speed signal and cooling water temperature to digital value, and read ignition advance angle value from an external eeprom these are time consuming operations, so the registers related to operational speed of these operations should be set according to time requirements.

5.1 A/D Conversion Calculations

5.1.1 Acquisition Time

Before the analog to digital conversion starts, the charge holding capacitor (C_{HOLD}) must be allowed to fully charge to input channel voltage level. Analog input model of PIC microcontroller unit is given in Figure 5.1; according to analog input model the source impedance (R_S), internal sampling switch impedance (R_{SS}) and interconnect resistance (R_{IC}) directly affect the time required to charge the capacitor (C_{HOLD}).

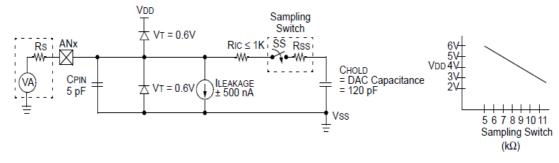


Figure 5.1: Analog input model

Another parameter affecting acquisition time is amplifier settling time, internal amplifier of the microcontroller unit is set before the conversion. Also working conditions especially temperature affects acquisition time of the microcontroller unit. The acquisition time of mcu can be stated as follows [1]:

 T_{ACQ} = Amplifier Settling Time + Hold Capacitor Charging Time + Temperature Coefficient (5.1)

$$\begin{split} &= T_{AMP} + T_C + T_{COFF} \\ &= 2 \ \mu s + T_C + \left[(\text{Temperature -25 °C})^* (0.05 \ \mu s/ \ ^{\circ}C) \right] \\ &T_C = C_{HOLD} \ ^* (R_{IC} + R_{SS} + R_S)^* \ln(1/2047) \\ &= -120 \ pF \ (1 \ k\Omega + 7 \ k\Omega + 10 \ k\Omega) \ \ln(0.0004885) \\ &= 16.47 \ \mu s \\ &T_{AMP} = 2 \ \mu s \\ &T_{ACQ} = 16.47 + 2 + (75-25)^* 0.05 \\ &= 20.97 \ \mu s \end{split}$$

The result of equation 4.1 gives the acquisition time of voltage, it may be assumed as a delay before the A/D conversion. The order of magnitude of acquisition time is microsecond; it is acceptable for our application.

5.1.2 Selecting the A/D Conversion Clock

The analog to digital conversion time per bit is defined as T_{AD} . The analog to digital conversion requires a minimum 12 T_{AD} per 10-bit conversion process. For correct A/D conversion operation, the A/D clock must be selected to ensure a minimum T_{AD} 1.6 µs [1]. The source of the analog to digital conversion clock is software selected and there are six options for T_{AD} :

- 2 T_{OSC}
- 4 T_{OSC}
- 8 T_{OSC}
- 16 T_{OSC}
- 32 T_{OSC}
- 64 T_{OSC}

Note: T_{OSC} is period of oscillator. The oscillator on the control circuits is 4 MHz crystal:

```
Frequency (f) = 1/ Period (T)

5.2

4 MHz = 4000 000 Hz

4000000 = 1/T_{OSC}

T_{OSC} = 0.25 \ \mu s

As stated before, T_{AD} should be selected as minimum 1.6 \mu s.

X^*T_{OSC} = 1.6 \ \mu s X*0.25 \mu s = 1.6 \ \mu s so X = 6.4 (minimum)

So it is selected as 8T_{OSC}. Conversion time can be calculated as 12^*T_{AD}

12^*1.6 = 19.2 \ \mu s required time for 10-bit conversion.
```

5.1.3 A/D Conversion Resolution

As it is stated before, PIC16F877A has 10-bits A/D conversion module it means it can sense 4.8876×10^{-3} volts.

Resolution = $(Vref^+ - Vref) / (2^{10}-1)$

5.3

= (5-0) / 1023=4.8876x10⁻³ volts

5.2 Serial Communication Rate

In our system synchronous serial communication method is used. Minimum operating time is selected for analog to digital conversion operation, but it is about 20 μ s. There is no specific limit for serial communication rate, but it can be select as

equal to the analog to digital conversion rate. The required time for serial communication will be selected as 16 μ s (for 8-bit). Operational speed of serial communication is defined with baud rate; it is numbers of bits transferred per second; and it is set by SPBRG register. For synchronous serial communication [1]:

Baud rate = $F_{OSC} / (4*(SPBRG+1))$

5.4

1/Baud rate = T (time required to send 1 bit data) (s)5.5

As mentioned above, the required time for serial communication may be selected as $16 \,\mu s$ So from the equation 5.5:

 $16x10^{-6} = 8*(1 / Baud rate)$ for 8-bit data Baud rate = 500 kHz From the equation 5.4: 500000 = 4000000 / (4*(SPBRG+1))

SPBRG = 1

5.3 Reading Ignition Advance From External Eeprom

The most time consuming operation is reading ignition advance angle value from an external eeprom. This operation is held by using I²C master mode operation. The master device generates all of the serial clock pulses and the start and stop conditions. The operation has two part as follows master transmitter mode and master receive mode. In master transmitter mode serial data is output through SDA pin (pin RC4) while SCL (pin RC3) outputs the serial clock. The first byte transmitted contains the slave address of the receiving device (7bit) and read/write (R/W) bit for this operation R/W bit will be logic 0; it means master device will write. After each byte is transmitted an acknowledge bit (ACK) is received. In master receive mode, the first byte transmitted contains the slave address of the slave address of the transmitting device (7 bits) and the R/W bit, for this operation the R/W bit will be logic high "1". Serial data is transmitted 8 bits at a time. After each byte is transmitted, an acknowledge bit (ACK) is received the assembly code to check ACK bit is command

lines between 884 and 895 in Appendix A. The assembly code of the operations to read data from external eeprom is between command lines 828 and 937 in Appendix A. The external eeprom memory which is used in our system has 64 Kbit memories; so it is addressed with 2 bytes; they are called high byte and low byte. The data transfer rate of this communication is set with SSPADD register as below [1]

 $Clock = F_{OSC} / (4*(SSPADD+1))$

5.6

The original communication speed was defined with a maximum 100 kbit per second (max frequency 100 KHz) so we will select clock as 100 KHz.

From the equation 5.6:

100000 = 4000000 / (4*(SSPADD+1))

SSPADD = 9

Equation 5.5 can be used to calculate required time to read or send 1-bit data as follows:

 $1/100000 = 10 \,\mu s$ required time to send 1-bit data.

The operational view of reading 8-bit data from external eeprom with 2 byte address is shown in Figure 5.2.

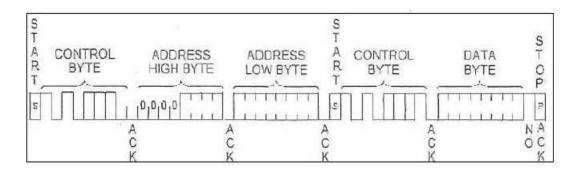


Figure 5.2: Operational view of reading 8-bits data in I²C master mode

The operations to read ignition advance angle value in our system will be as follows:

- Send 8-bit control byte
- Wait for ACK signal
- Send high byte of address which will be read
- Wait for ACK signal
- Send low byte of address which will be read

- Wait for ACK signal
- Send 8-bit control byte
- Wait for ACK signal
- Read 8-bit data

As stated above, to read 8-bit data the system send or receives 8 bit data for five times and wait for ACK signal for four times. So required time to read 8-bit data will be:

 $5*8*10 \mu s + 4$ wait for ACK signal

 $400 \ \mu s + 4$ wait for ACK signal

The operations and their time consumption were given above, but there are also mathematical calculations and delays during the operation. And the time consumed during those operations related to the engine speed so this time will be determined experimentally. The important point here is the time consumed during those operations shall not exceed time interval between two ignitions. This time interval can be calculated as follows:

Time interval between two ignitions = (1000*60)/(8*Engine Speed) 5.7

5.4 Calculating Advance Delay

In our system, advance angle values are kept in external eeprom. The control circuits read analog value and convert it into digital form. After the conversion, they scale it into 5-bits or 8-bits form to form external eeprom addresses. In our system, the cooling water temperature was taken as zero and advance angle addresses were calculated. So, engine speed is the only criterion to read advance angle. After conversion of engine speed into digital form, the related control circuit divides it to 4 to scale it into 8-bits form. It is calculated as in equation 5.8:

Eeprom address = Engine speed (volts) / $[4*4.8876x10^{-3} (volts)]$ 5.8

Advance angles are determined after calibration of the engine, so at this time we do not have data to write to the eeprom addresses. So, the advance angle values were selected the same with eeprom addresses because we are just testing ignition system for the time being. Advance delay which is read from external eeprom can be calculated as in equation 5.9.

5.9

5.5 Determination of Ignition Modes

As stated before, the ignition process starts with the flowing of the current through the primary coil of the ignition coil. When the current is broken, the spark is generated. But to have suitable spark quality, the ignition coils should be saturated, so there is a minimum duration which the current should keep flowing. This duration was observed around 5 ms for our ignition system. With the increasing engine speed, the starting point of the ignition process should be advanced; this is called as dwell angle. The main control circuit which manages the all operations is capable of arranging the dwell angle with its code. There are 4 main modes which are mode_0, mode_1, mode_2 and mode_3. Also, there are 3 transition modes between the main modes; they are premode_1, premode_2 and premode_3. The ignition modes are determined with the codes between 68 and 736 in Appendix A.

We have 2 points which we can use to arrange dwell angle they are cylinder position signals and ignition points. We can start the ignition process when the cylinder position signal is received (mode_0) which is valid for low engine speeds. We can start the ignition process at the ignition point or cylinder position signals of the previous cylinders. In mode_1, the ignition process is started at the ignition point of the previous cylinder, in mode_2 the process is started at the cylinder position signal of the previous cylinder and in mode_3 the process is started at the ignition process of two cylinders before. And the premodes are used for the transition between two ignition modes. The ignition mode intervals can be calculated as below.

Sweep Time (ms) = [Crank Angle (degree)] x 60000 / [360 x Engine Speed (rpm)] 5.10

5.10

The cylinder position signals give the position of the point which is around 22.5° before the cylinder, and the angle between the actual cylinder position and the ignition point of the previous cylinder can be assumed as 45° . The equation 5.10 can be used to determine the starting point of the ignition process. The most important parameter is that minimum sweep time between the starting point of the ignition process and the spark generation is 5 ms, and we can use the points at 22.5° , 45° , 67.5° , 90° etc.

Sweep Time (ms) = [Crank Angle (degree)] x 60000 / [360 x Engine Speed (rpm)] 5.10

We can arrange the equation 5.10 as follows.

Engine Speed (rpm) = [Crank Angle (degree)] x 60000 / [360 x Sweep Time (ms)]Let's calculate the maximum engine speed for 22.5° as a sample calculation: Engine Speed = $(22.5 \times 60000) / (360 \times 5)$ Engine Speed (max) = 750 rpm this is the upper limit of the mode_0 For the sweep time 5 ms and crank angles 22.5, 45, 67.5 and 90°, the engine speeds

calculated as follows.

Ignition Mode	Crank Angle	Max. Engine Speed (rpm)
Mode_0	22.5°	750
Mode_1	45°	1500
Mode_2	67.5°	2250
Mode_3	90°	3000

 Table 5.1 Maximum engine speeds of the ignition modes

To stay in the safe region, the engine speed limits for the ignition modes are selected as 650, 1350, 2050 and 3000. And the limits for the transition are selected as 700, 1400 and 2100. The usage of the speed limits is given in source code of the main control circuit with the lines 68 and 115 in Appendix A. And the decimal number which are used to determine the ignition mode (lines 74, 80, 86, 92, 98, 104 and 110) are the rounded digital values of the lower limits of the ignition modes, and they are calculated as follows.

Engine Speed (digital) = Engine Speed (rpm) x 4.8 / (3000 x Resolution) 5.11 As it is stated in previous chapters, the frequency to voltage converter circuit is designed to have 4.8 volts output for engine speed and "Resolution" is the resolution of the ADC module which is calculated with the equation 5.3

CHAPTER 6

SOURCE CODES OF THE CONTROL CIRCUITS AND IGNITER CIRCUITS

As it was given in chapter 3, there are two control circuits and eight igniter circuits in our experimental set-up; and those circuits are microcontroller based circuits. In this chapter, the codes which were written and loaded to microcontrollers on the circuits will be stated and explained. The source codes of microcontrollers were written in assembly language and complied with MPLAB IDE v7.00 by Microchip. The assembly language is more complex language than C or Basic based microcontroller programming languages.

6.1 Source Code of the Main Control Circuit

In this part of the chapter, the source code of the main control circuit which is given in Appendix A will be explained. The duty of the main control circuit is to manage the operations, receive the rpm value from the secondary circuit, read the cooling water temperature and scale it into 5-bit form, combine the rpm value with the cooling water temperature to form the address of the external eeprom, read the advance value from the external eeprom and arrange the ignition points. The main control circuit is PIC16F877A based and it is working with 4 MHz crystal. As stated before, PIC16F877A has 40 pins; and these pins have jobs more than one. For example, a pin can be configured as analog input, digital input or digital output. So, first thing which should be done during programming is to configure the pins of microcontroller. The main body of the source code is labeled as main, the command lines 10 and 11 calls the subroutines which configure the microcontroller to do the jobs which are stated above. The command line 10 calls the subroutine which initializes the I2C communication, serial communication, input-output pins and analog channels. The duty of the subroutine "initialize" is as follows. As it is given in chapter 4, the main control circuit uses its PORTD to receive cylinder position signals from the secondary control circuit and send ready signal to the secondary control circuit. The 0th pin of PORTD is used to receive cylinder position signals, so it should be configured as input; and the 1st pin of PORTD is used to send ready signal, so it should be configured as output. The command lines between 744 and 748 in initialize subroutine are used to configure PORTD. After sending ready signal, the main circuit starts to wait for serial rpm value with synchronize serial communication. In the experimental set-up, main control circuit works as slave and the secondary control circuit work as master. The serial communication settings are arranged with the command lines which are given below:

bsf TXSTA, SYNC banksel RCSTA bsf RCSTA, SPEN banksel TXSTA bcf TXSTA, CSRC bsf PIE1, RCIE banksel RCSTA bcf RCSTA, RX9 return

--- ---- ---- ----

;765 the SYNC bit of register TXSTA ; should be set to 1 ; to select synchronous serial ; communication ;766 go to bank0 ;767 opens the serial port ;768 go to bank1 ;769 selects the slave mode ;770 activates the data receive ; interrupt ;771 go to bank0 ;772 data format is 8-bit ;773 quit from the subroutine

There are some registers to configure serial communication mode and settings. One of them is TXSTA. This register is used to select synchronous or asynchronous and master or slave serial communication. The command line 765 is used to select synchronous serial communication and command line 769 is used to select slave mode serial communication. Another register is RCSTA, this is used to select 8-bit or 9-bit data transfer and open or close serial port. The command line 767 is used to open the serial port and the line 772 is used to select 8-bit data transfer. After receiving serial rpm data, the main control circuit reads analog cooling water temperature and converts it into digital form. So the analog to digital conversion parameters should be arranged. The command lines which are given below are used to configure ADC.

			ADCONO is a register which configures ADC the bits ADCONO,6 and ADCONO,7 are used to select ADC clock frequency and the bit ADCONO,0 is used to activate ADC module
		;	for clock=Fosc/8 ADCON0,6=1 ADCON0,7=0 to activate the module ADCON0,0 shall be 1 the sum of ADCON0,0 ADCON0,6 equals to d'65'=0x41
mo∨lw mo∨wf	0x41 ADCON0		50 W=0x41 51 ADCON0=0x41 it means clock frequency is Fosc/8 and ADC module is activated
	0x80 STATUS, R ADCON1	P0 ;	62 W=0x80 63 go to bank 1 64 ADCON1=0x80 the 7th bit of ADCON1 register
			shall be set to "1" to arrange ADRESH (high byte of ADC) and ADRESL (low byte of ADC) to get a 10-bit ADC result in form of 000000xx(ADRESH)xxxxxxxx(ADRESL) x=0 or 1 so ADCON1=d'128'=0x80

---- ---- ----

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The related registers to configure ADC settings are ADCON0 and ADCON1. The value 0x41 is appointed to ADCON0 to set the ADC clock frequency Fosc/8 [1] with command line 760 and 761. PIC16F877A has 10-bit ADC module, the format of the 10-bit data can be arranged by ADFM (bit-7) of ADCON1. In the source code, the ADCON1 is arranged to have 000000xx (high byte of 10-bit data) and xxxxxxx (low byte of 10-bit data) with the command lines 762 and 764.

The main control circuit reads advance angle value from an external eeprom with I2C protocol as it is given in part 5.3. From the result of equation 5.6 to have 100 kHz data transfer speed SSPADD register shall be 9. And to use I2C master mode and SDA and SCL pins for data transfer SSPCON register shall be equal to b'00101000'. All these requirements are arranged the codes in subroutine "I2C_init" which is the subroutine of "initialize" as below:

---- ---- ----

I2C_init

banksel	SSPSTAT	;828
clrf	SSPSTAT	;829

bsf	SSPSTAT, SMP	;830 SSPSTAT, SMP is used to select ; standard cycle frequency
mo∨lw	в'00001001'	<pre>;831 W=9 ; clock=Fosc/(4x(SSPADD+1)) Fosc=4MHz ; so for 100kHz clock SSPADD=9</pre>
	SSPADD SSPCON2 B'10011000'	,832 SSPADD=9 ;833 ;834 SDA and SCL are configured as input
movwf movlw bcf movwf clrf return	SSPCON	;835 ;836 ;837 ;838 master I2C mode is selected ;839 ;840

After initializing the ports and communication settings, the first duty of the main control circuit is send ready signal to the secondary control circuit by making high 1st pin of the PORTD with command line 12 in source codes, this is the starting point of the main loop which is called "loop". Then it calls the "snkSlaveRead"subroutine. This subroutine is used to read serial rpm data which is coming from secondary control circuit by master-slave serial communication. The command lines of the subroutine are:

---- ---- ----

snkSlaveRead

banksel RCSTA bsf RCSTA,	SPEN		opens the serial port again we should open the port again for every reading
banksel TXSTA bcf TXSTA,	CSRC	;816 ;817 ;	selects slave mode(after receiving data port configures itself to master mode)
banksel RCSTA bsf RCSTA,	CREN	;818 ;819 ;	starts to waiting for receiving data

btfss	PIR1, RCIF	;820 bit RCIF of PIR1 is set ; when the data received so ;
goto	\$-1	,821 wait for the end ; of data transfer
mo∨f	RCREG, W	;822 if data transfer is ; completed, W=RCREG ; RCREG is a register which ; stores the received data
bcf	PIR1, RCIF	; 823 clear the flag of received ; data for the next data transfer
btfsc	RCSTA, CREN	;824 if there is an error during ; the data transfer ; bit CREN of RCSTA is reset, ;so check whether there is an error ; or not if there is an erro set ; kontrol_register,0 (line 826)
return		;825

The command line 815 is used to open the serial communication port and command line 817 is used to configure slave communication mode. If there is an error during the serial communication, CREN bit of the RCSTA register will be zero so it should be set as high (1) before the communication, command line 819 is used for this purpose. The RCIF bit of the register PIR1 will be high (1) when the serial communication is completed. With the command line 820, the end of serial communication is waited. The line 822 gets the received data to temporary variable (W); and the command line 824 checks whether there is a communication error or not. If there is an error, the program sets the 0th bit of konrol_register (it is a register defined by the user). Then the user can check the kontrol_register and avoid receiving wrong data. With the "return" command program returns line 18 and appoint the value of "W" to tempH this is the first 8-bit of advance angle address.

The next step is to read cooling water temperature with analog to digital conversion module. For this purpose there are two variables defined ADC_Oku_kanalno (line 22) and ADC_Oku_sonucbyte (line 24). ADC_Oku_kanalno is the number of analog channel. As stated before, the PIC16F877A has 10-bit ADC module, so the result of the conversion is two 8-bit data. They are the ADRESL and ADRESH; the low 8-bit of the conversion is ADRESL and high 8-bit of the conversion is ADRESL. The source code was written to read ADRESL firstly and read ADRESH secondly. To read ADRESL, the value 0x00 is loaded to ADC_Oku_sonucbyte(line 24) and the

subroutine "ADC_Oku" is called. The subroutine "ADC_Oku" is between 783 and 801. The analog channel is chosen with the bit 5, 4 and 3 of the register ADCON0, so ADC_Oku_kanalno value should be required 3-bit format, this is done with the command lines 784,785 and 786. To initialize ADC module 0x41 values was loaded to ADCON0 with command line 761, so this value should be added to 3-bit channel number; this is done with command line 787.

---- ---- ----

bcf	STATUS, C		;783 STATUS,C is affected by command rl ; so it should be disabled ; before the operation	lf
rlf	ADC_Oku_kanalno,	F	;784 register ADCONO is used	
rlf	ADC_Oku_kanalno,	F	; to configure ADC module ;785 bit 3, bit 4 and bit 5 of : ADCONO is used to select	
rlf	ADC_Oku_kanalno,	W	786 ADC channel xx000xxx channel 1 xx001xxx channel 2 xx010xxx channel 3 xx111xxx channel 7 so the value ADC_Oku_kanalno should be shifted to the left for 3 times	

The analog channel is chosen with the bit 5, 4 and 3 of the register ADCON0, so ADC_Oku_kanalno value should be required 3-bit format, this is done with the command lines 784,785 and 786. To initialize ADC module 0x41 values was loaded to ADCON0 with command line 761, so this value should be added to 3-bit channel number; this is done with command line 787.

	iorlw	b'01000001'	<pre>;787 to open ADC module ADCON0,0 and for the clock frequency 0x41 should be added (lines 760 and 761)</pre>
	Banksel	ADCON0	; ;788 iorlw b'01000001'adds ; 0x41 to ADC_0ku_kanalno
	mo∨wf bsf	ADCONO ADCONO, 2	;789 ;790 starts the conversion
ADC_j1			
	btfsc	ADCONO, 2	;791 if ADCON0,2 is zero it means ; it is the end of conversion

	- movf btfss	- ADC_Oku_sonucbyte, F STATUS, Z	,793 ,794	waits for the conversion if ADC_Oku_sonucbyte is zero, it means read the low byte of conversion go to line 796
	goto	ADC_j2	;795 ;	if it is not zero go to ADC_j2 and read high byte
	bsf movf return	STATUS, RPO ADRESL, W	;797	go to bank1 w=ADRESL quit from the loop
ADC_j2				
	bcf mo∨f return	STATUS, RPO ADRESH, W	;800	go to bank0 W=ADRESH quit from the loop

The conversion starts with the command line 790, bsf ADCON0; 2. If the ADC_Oku_kanalno is 0x00, program goes to "ADC_j1" and takes the low 8-bit of the conversion and loads it into sicaklikL (command line 28); if the ADC_Oku_kanalno is 0x01, program goes to "ADC_j2" and takes the high 8-bit of the conversion and loads it into sicaklikH (command line 40). As stated in previous chapters, the cooling water temperature will be scaled into 5-bit format. The command lines between 43 and 58 which is subroutine "dongu2" scale it into 5-bit format.

dongu2

---- ---- ----

---- ---- ----

subwf	d'33' sicaklikL,1 stAtus,c		sicaklikL=sicaklikL-33 if the new value of sicaklik is negative
incf	\$+3 bolum,1 dongu2 bolum,1 STATUS,0	,46 ,47 ,48 ,49 ,50	<pre>(checks the overflow of 7th bit) "C" bit of STATUS is set to zero when the result of mathematical operation go to line 49 bolum=bolum+1 go to line 43 bolum=bolum+1 set "C" bit of STATUS to 1 for the next operation</pre>
mov]w subwf	d'1' sicaklikH,1	;51 ;52	sicaklikH=sicaklikH-1
goto goto decf goto	STATUS,C \$+2 \$+3 bolum,1 \$+2 dongu2	;54 ;55 ;56 ;57	if there is an overflow go to line 56 go to line 56 go to line 58 bolum=bolum-1 go to line 59 go to the starting point of the "dongu2"

Now the program is ready to form 13-bit address of the external eeprom and read advance value. In this study, the cooling water temperature was read for future works but was not used as an input in this study, so the high byte of the external eeprom is taken as zero with the line 62. The codes which are given below are used to form 13-bit eeprom address and call the subroutine which reads the advance value.

	mo∨f	tempH,0	;59 W=tempH, this line loads	W=tempH, this line loads the value of tempH to the
	movwf	sayacH	;60	sayacH=W it means sayacH=tempH
		I2C_Device I2C_AdrH		I2C_Device=0 I2C_AdrH=0 because we did not use the cooling water temperature for this study but it may be used in the future (it may be the output of any sensor with analog output)
	mo∨f mo∨wf	sayacH,0 I2C_AdrL		W=sayacH I2C_AdrL=sayacH
	call	I2C_ReadEE	;65 ;	calls the subroutine "I2C_ReadEE" which
			;	reads 8-bit data from the external eeprom
bcf	PO	RTD,1	,66	makes the 1st bit of PORTD logic low elapsed time between line 12 and line 66 gives the required time to read serial rpm data, read analog value and convert it into digital, scale 10-bit ADC result into 5-bit and read the advance value from the external eeprom

With the command lines 59 and 60, the serial rpm value which is in 8-bit format is loaded to "sayacH" then it is loaded to low value part of the eeprom address with the command lines 63 and 64. For the time being there is no cooling water so the high value part of the eeprom address is taken as zero with the command line 62. Now we are ready to read advance angle value with the command line 65, "call I2C_ReadEE".

---- ---- ----

As it is stated in part 5.3 with figure 5.2, first of all we should start the I2C serial communication this is done with subroutine "I2CStart" (command line 841). In this subroutine, the start bit (SEN) of the register SSPCON2 is enabled by the command

line 844). Then the program waits for the being disabled of SEN bit of the register SSPCON2 in subroutine "I2CStart_j1" to continue. Then it checks whether the initiated start condition was completed by the MSSP module, by checking SSPIF bit of the register PIR1 with command line 850. SSPIF bit will be high if the start condition is completed. If it is enabled, the program erase that flag with bcf PIR1,SSPIF command for the other operations. To learn the duties of the registers and their bits, it will be helpful to look at the datasheet of PIC16F877A. The codes required to start I2C communication are as below:

I2CStart				
banksel bcf	PIR1 PIR1, SSPIF	;841 ;842 PIR1,SSPIF is set at the end of ; the I2C communication ; so it should be cleared before ; the communication		
bsf bsf	STATUS, RPO SSPCON2, SEN	;843 ;844 bit SEN of SSPCON2 is used to ; start the I2C communication ; line 844 starts the communication		
I2CStart_j1				
btfsc goto	SSPCON2, SEN I2CStart_j1	;845 waits for the starting operation ;846 if it is not started yet ; go to "I2CStart_j1"		
banksel	PIR1	;847		
I2CStart_j2				
btfss	PIR1, SSPIF	;848 checks whether the data ; transfer is completed or not		
goto	I2CStart_j2	;849 waits for the data transfer		
bcf return	PIR1, SSPIF	;850 if data is transferred clear the bit		

----- ----- -----

Now we can send the control byte to the external epprom, the control byte is combination of hardware address of the eeprom (1010, MSB) and logic states of A0, A1 and A2 pins of the eeprom and R/W bit (LSB), R/W bit is used to select reading from eeprom or writing to the eeprom. R/W is 0 for wirting operation and 1 for reading operation. A0, A1 and A2 pins are used to address the eeproms and give us chance to use 8 eeproms at the same time (2^3=8, it means possibility of 8 different addresses). All the pins in our application are connected to the GND. So, the 4 less significant bits of the control byte is 0000. With the command lines 912, 913 and 914 the source code forms the control byte, by this method you can connect another eeprom to the circuit and use it without changing the source code. With the command line 915, the control byte is loaded to "I2CSend_data".

I2C_Read	dee		
	call rlf	I2CStart I2C_Device, W	<pre>;911 starts the communication ;912 data format of control byte ; is 1010(A2)(A1)(A0)(R/W) ; so to have this form we ; shall shift the I2C_Device ; to the left. Actually we can ; write the control byte directly ; because there is only one ; external eeprom. This code form is ; used for future works</pre>
	andlw iorlw movwf call	I2CSend_Data	,913 ,914 R/W is 0 ,915 I2CSend_Data=control byte ,916 calls the subroutine which sends , data to the external eeprom

Then the program goes to the subroutine "I2CSend", this is the subroutine which sends the data to the external eeprom with the code given below. There is an another register called as "SSPBUF", this is the buffer of the master synchronous serial port; so to send the data I2CSend_Data is loaded into that register with the command line 863.

```
I2CSend
banksel PIR1 ;861
bcf PIR1, SSPIF ;862 should be reset before
movf I2CSend_Data, W ;863 W=I2CSend_Data
movwf SSPBUF ;864 SSPBUF=I2CSend_Data
; SSPBUF is buffer register,
; it stores the received or sent data
return ;865 quit from the routine
```

The other subroutine in the routine "I2C_ReadEE" is "I2CAck", as it is seen in figure 5.2, after data transfer external eeprom send a received signal. (Ack means acknowledged). The most important line of that routine is "btfsc SSPCON2, ACKSTAT" because ACKSTAT bit of the SSPCON2 becomes low (0) when the data is received by the eeprom. The duty of I2CAck subroutine is to check whether the data sent to the eeprom is received or not.

After the control byte, the high byte part of the eeprom address is sent to eeprom, for each data transfer the I2CACK subroutine is called to check whether the data is sent or received. The codes below are used to send the high byte of the address and checkACK.

movf	I2C_AdrH, W	;918 W=high byte of eeprom address ; which the advance data will be read
	I2CSend_Data I2CSend	;919 I2CSend_Data=high byte of address ;920 calls the subroutine which sends ; data to the external eeprom
call	12CAck	; 921 after sending high byte of ; address we should check ACK

Then the low byte part of the eeprom address is sent to the eeprom and ACK is checked again.

---- ---- ----

---- ---- ----

---- ---- ----

mo∨wf	I2C_AdrL, W I2CSend_Data I2CSend	;922 W=low byte of eeprom address ;923 I2CSend_Data=low byte of address ;924 calls the subroutine which
call	12CACk	; sends data to the external eeprom ;925 after sending low byte of address ; we should check ACK

The next step needs to be paid attention, the address value is sent to the eeprom and the data at that address will be read, to read a value from the external eeprom, new control byte with R/W=1 should be sent, so the eeprom should be restart again. To restart the eeprom the subroutine "I2CReStart" will be called, to restart the eeprom RSEN bit of SSPCON2 register will be set with the command "bsf SSPCON2, RSEN"(command line 857). Then control byte should be sent to the eeprom, but R/W bit shall be 1, it means reading operation will be held. The codes which are used to restart are given below.

I2CReStart				
nop nop nop nop banksel bsf	SSPCON2 SSPCON2,	RSEN	;851 ;852 ;853 ;854 ;855 ;856 ;857	SSPCON2, RSEN is used to restart the I2C mode
I2CReStart_j1				
btfsc	SSPCON2,	RSEN	;858 ;	SSPCON2, RSEN is reset at the end of resatrt operation

goto	I2CReStart_j1	;859 this lines are used to wait	t
		; for the end of restart	
return		;860	

Finally the I2CRead subroutine will be executed. The value of the SSPBUF register is the value of the data which we want to read. "I2CRead" subroutine has also some registers and bits which are enabled or disabled after data transfer, these registers can be easily found in the datasheet of PIC16F877A [1].

```
I2CRead
        banksel SSPCON2
                                        ;866
                                        ;867 this line activates the
        bsf
               SSPCON2, RCEN
                                        ;
                                             receiving mode
I2CRead_j1
        btfsc SSPCON2, RCEN
                                        ;868 wait for the end of
                                        ; activation of receiving mode
        goto _ I2CRead_j1
                                        ;869
        banksel PIR1
                                        ;870
I2CRead_j2
                                       ; is data received?
;871 if no, wait for the data transfer
        btfss PIR1, SSPIF
        goto
               I2CRead_j2
        bcf
               PIR1, SSPIF
                                        ;872 after data transfer, reset
                                            the data transfer flag
       movf
                                        873 read the received data
               SSPBUF, W
                                        ;874 quit from the routine
        return
```

The last step of reading advance angle data from an external eeprom is calling I2CNak subroutine. This routine is used to check whether reading operation completed or not, there are some registers which set or reset at the end of reading operation these registers can be easily found in the datasheet of the PIC16F877A[1]. The codes which are given below are used to check "NO ACK".

```
I2CNak
       banksel SSPCON2
                                       :896
       bsf SSPCON2, ACKDT
                                        ;897 set bit ACKDT of SSPCON2
I2CNak_j1
        btfsc SSPCON2, ACKSTAT
                                       ;898 waits for the acknowledgement of
                                            data by the slave device
       goto
               I2CNak_j1
                                       ;899
               SSPCON2, ACKEN
                                       ;900 sets the receiving mode of
        bsf
                                            master device and
                                            sends ACKDT bit to slave device
                                        :901
       bcf
               STATUS, RPO
                                       ;902 reset the bit SSPIF of PIR1
        bcf
               PIR1, SSPIF
I2CNak_j2
                                          ;903
        banksel SSPCON2
                                          ;904 after sending of ACKDT,
, ACKEN is reset
        btfsc SSPCON2, ACKEN
                                          ;905 so these lines checks
                I2CNak_j2
        goto
                                              whether ACKDT is sent or not
                                          ;906
        banksel PIR1
I2CNak_j3
        btfss
                                          ;907 is the data transferred?
                PIR1, SSPIF
        goto
                I2CNak_j3
                                          :908 waits for the data transfer
        bcf
                PIR1, SSPIF
                                          ;909 reset PIR1, SSPIF for
                                               the next operations
                                          ,910 quit from the routine
        return
 -- ---- ----
```

When the advance angle value is read from the external eeprom, the main control circuit makes 1st bit of PORTD low by the command line 66. The read advance angle value is loaded to variable "avans" with command 67. Now the circuit is ready to receive cylinder position signals from the secondary control circuit and add advance value to the cylinder position and ignite the spark plugs. As stated in previous parts, to ignite the spark plugs we should saturate the ignition coils it means we let the current flow through the primary coil of ignition coils for a while, this duration is around 5 ms for our application. But, if the engine speed increases the time between two cylinder positions decreases, so we do not have required time to saturate the ignition coils and get poor spark quality. To avoid getting poor spark quality with the increasing engine speed, the code block which is between command lines 69 and 115 was written. With this code block, the start point of the current flow through the primary coil of ignition coils between 68 and 72,

the rpm value is loaded to a variable "mode_sayac" and according to this variable starting point of the current flow is determined.

For example, if the rpm value (mode_sayac) is between 1 and 54, it means the engine speed is between 0 and 650 rpm, the subroutine mode_0 (command lines between 116 and 196) is called, with this subroutine main circuit receives first cylinder position signal from the secondary control circuit with PORTD,0 and starts the current flow through the primary coil of first ignition coil and then breaks the current at the ignition point and spark occurs. And it repeats this sequence for the other seven ignition coils. Then it goes to the starting point of the main loop ("loop"). For this case, the engine speed is low and the time between two ignition points is much enough to saturate the ignition coils. The "loop 7" which is given below is used to check whether the engine speed is between 0 and 650 rpm

loop7

```
movlw d'1'
                                        ;110 W=1
subwf mode_sayac,W
                                          ;111 mode_sayac=mode_sayac-1
                                          ;112 whether the result of line 111 is
btfss STATUS,C
                                                negative or not
                                          ;113 if it is negative go to
; starting of the "loop"
;114 if it is not negative, calls
; the ignition mode "mode_0"
goto
         100p
call
         mode_0
         100p
                                          ;115 when the ignition sequence is
goto
                                                complete,
                                                go to the starting of the "loop"
```

---- ---- ----

For the case mode_1 (command lines between 279 and 368), there is not enough time between two ignition points, so the starting point of the current flow through the primary winding of ignition coils are advanced. The commands given below are from case mode_1, when the main control circuit ignites the 8th ignition coil; it starts to saturate the 1st coil according to these codes. But, there is an important point; while the first execution of mode_1 first ignition coil would not be started to saturate before, so the first park of the ignition coil 1 would have poor quality. To prevent this situation, the control code has "premode_x" routines. For example, the premode_1 subroutine is the same with the mode_0 routine except command line 277. With this command line it starts to saturate the 1st ignition coil at the end of the

ignition sequence and will be ready for the mode_1. There is a disadvantage of these premode_x routines, if the engine rotates with the speed within the premode_x routines for a long time the 1st ignition coil and igniter circuit starts to heat, so the speed limits of premode_x were kept tight. The codes given below are the part of premode_1. With the line 277, the 1st ignition coil is started to be saturated at the ignition point of the 8th ignition coil.

	PORTB,0	;272;273	
call bcf	delay_ms_data delay_ms PORTB,0	;274;275;276	ale des inisies suite is
bsf	portb , 7	;	the 1st igition coils is started to be saturated at this point for the the mode_1
return		;278	

----- ----- -----

---- ---- ----

The other modes and premodes have the same philosophy with mode_0, premode_1 and mode_1. With the increasing engine speed, they advances the starting point of the current flow through the primary windings of ignition coils, and eliminate the decreasing spark quality with the increasing engine speed. The mode of the ignition ignition is determined with the loops "loop2", "loop3", "loop4", "loop5", "loop6", "loop7" and lines between73-79.

After completing the ignition of all sparks, the program goes to the starting point of the "loop" (line 12) to repeat the steps which are told above.

6.2 Source Code of the Secondary Control Circuit

As stated before, the two control circuits communicate with each other by synchronous master-slave communication. Main control circuit works as slave circuit and secondary control circuit works as master circuit in our application. The source code of the main control circuit is given in Appendix A and explained in previous part. In this part, the source code of the secondary control circuit which is given in appendix B will be explained.

The main duty of the secondary control circuit is to read engine speed and send it to the main control circuit, and detect cylinder positions and send them to the main control circuit. As it is in the previous source code, the code starts with an initialization subroutine. In that subroutine, Input/output pins of the PORTD and PORTB is configured. With the command line 83, all the pins of PORTB configured as output, because the secondary control circuit shows number of pulses in binary form with the leds connected to PORTB, also 7th pin of PORTB is used to send cylinder position signals to the main control circuit. 0th, 1st and 2nd pins of PORTD shall be configured as input because 0th pin detects the ready signal of the main control circuit, 1st pin detects output of the reference point sensor and 2nd pin detects output of cylinder position sensor. Those pins are configured as input with the command lines 86 and 87. The codes given below are used to configure the ports.

initial				
		STATUS,RPO	;81	go to bank1
		TRISC	;82	all pins of PORTC are output
	clrf	TRISB	;83	all pins of PORTB are output
	movlw	D'255'		W=255
	mo∨wf	TRISA	;85	TRISA=255 it means all pins of PORTA are
			;	input
	movlw			W=7
	mo∨wf	TRISD	;87	TRISD=7 it means 0th, 1st and 2nd pins of
			;	PORTD
			;	are input, the other pins are output
	bcf	STATUS, RPO	:88	go to bankO
		PORTB	:89	initial value of PORTB is zero
	clrf		:90	initial value of rpmL is zero
	clrf	rpmH	:91	initial value of rpmH is zero
	clrf	sayac2	;92	initial value of sayac2 is zero
	clrf	sayac3	93	initial value of sayac3 is zero
		-	-	•

____ ____

---- ---- ----

The command lines between 95 and 98 are used to configure ADC module, this part is the same with the part which is given in part 6.1. The secondary circuit is master circuit, so serial communication rate will be set by the secondary control circuit. From the result of equation 5.4 SPBRG = 1 for 500 kHz communication rate. The command lines between 100 and 105 are written to set the baud rate to 500 kHz.

```
;100 W=0x01
movlw 0x01
                                      ;101
                                      ;102 go to bank0
banksel TXREG
clrf
                                      ;103 TXREG=0
       TXREG
banksel SPBRG
                                      ;104 go to bank1
                                           the register SPBRG is used to select
                                           serial communication baudrate
                                           the formula to calculate the baudrate
is baudrate=Fosc/(4x(SPBRG+1))
we have selected the baudrate as 500000,
                                           so 500000=4000000/(4x(SPBRG+1))
                                           SPBRG=1
movwf SPBRG
                                      ;105 SPBRG=1
```

The other settings of the serial communication are configured with the lines given below.

	-		
banksel bsf	TXSTA TXSTA, SYNC	;106 ;107 the SYNC bit of register ; TXSTA should be set to 1 ; to select synchronous serial ; communication	
bsf	TXSTA, CSRC	;108 selects the master mode	
bsf	PIE1, TXIE	;109 data sending interrupt is activat	ed
bcf	txsta, tx9	;110 8-bit data format is selected	
bsf banksel bcf bsf	TXSTA, TXEN RCSTA RCSTA, SREN RCSTA, SPEN	;111 data sending is activated ;112 ;113 no data receiving ;114 opens the serial port	
return		;115	
	-		

Also, bsf TXSTA, CSRC (command line 108) is different from the main control circuit, this code is used to enable CSRC bit to set master mode.

Now the code has completed configuration and initialization parts, and it is ready for the operation. Main loop of the source code is called as "tekrar", first of all it detects the ready signal of the main control circuit with the command line 2, when it receives ready signal it reads the engine speed with the command lines between 4 and 20. Then it scale the 2 two 8-bit data into 8-bit and send it to the main control circuit

with the subroutine "dongu2", and sends it to the main control circuit with the subroutine "snkMasterWrite".

---- ---- ---snkMasterWrite banksel TXREG ;152 go to bank0 movwf TXREG ;153 with line 39, value of "bolum" was loaded to W TXREG=bolum (the data which will be sent is loaded to TXREG) :154 go to bank O banksel PIR1 the bit TXIF of PIR1 is set when data transfer is completed btfss PIR1, TXIF ;155 checks whether the transfer is completed or not \$-1 ;156 if not, wait for the data transfer goto ;157 if data is transferred, reset bcf PIR1, TXIF the PIR1, TXIF for the next communication return

---- ---- ----

---- ---- ----

After sending rpm data to the main control circuit, it starts to detect the output of reference point sensor with the command line 42, at the falling edge of the pulse it sends first cylinder position signal to the main control circuit with PORTB,7. The PORTB,7 stays at logic high state for 20 us, then it goes to logic low again.

Banks	el portb	;41	go to bankO
goto	PORTD,1 \$-1 PORTD,1	;42 ;43 ;44	checks the first cylinder position waits for the cylinder position signal checks the falling edge of the
goto bsf	\$-1 portb,7	;45 ;46 ;	first cylinder position signal waits for the falling edge if the falling edge is detected, send first cylinder position signal to the main control circuit
call bcf	delay_20us PORTB,7	;47	to the main control circuit 20 us delay makes low the PORTB,7

Then the program goes to another loop which is called as "dongu3", in this loop it counts the ten pulses to detect the positions of the other cylinders as follows. It counts 10 pulses because the gear wheel in our experimental set-up has 80 teeth, so 10 teeth mean the new cylinder position. Then it makes 7th pin of PORTB high for 20

us to send new position signal to the main control circuit. The program repeats this routine for 7 times and completes its duty. Then it goes to the main loop "tekrar".

---- ---- ---dongu3 bcf STATUS,Z ;49 clears the STATUS,Z ;50 no operation nop ;51 no operation nop ;52 is there a pulse? ;53 if no go to line 52 btfss PORTD,2 goto \$-1 ;54 if yes wait for the falling edge btfsc PORTD,2 goto \$-1 ;55 ;56 banksel PORTB incf sayac2,F movf_sayac2,0 ;57 sayac2=sayac2+1; ;58 W=sayac2 ;59 PORTB=sayac2, this is used to see movwf PORTB the pulses with the leds of PORTB ;60 W=10 mov]w d'10' ;61 W=sayac2-10 subwf sayac2,W ;62 if sayac2=10 go to line 64 btfss STATUS,Z the gear wheel which is used to measure the crank shaft angle (detecting the cylinder positions) has 80 teeth, so 10 teeth (pulses) means 45 degree, new cylinder position goto dongu3 ;63 sayac2 is not equal to 10, go to the starting point of the dongu3 ;64 clears PORTB clrf PORTB ;65 sends the cylinder position signal ; to the main control circuit ;66 20 us delay bsf PORTB,7 call delay_20us PORTB,7 bcf ;67 makes PORTB,7 low ;68 sayac2=0, for the next cylinder ; position detection clrf sayac2 ;69 go to bankO banksel PORTB ;70 sayac3=sayac3+1 sayac3 is incf sayac3,F ; the number of detected ; cylinders (except first cylinder) ;71 W=7 movlw d'7' subwf sayac3,W ;72 W=sayac3-7 ;73 if sayac3=7 (if all cylinde are btfss STATUS,Z detected which means one full revolution) go to line 75 goto dongu3 ;74 if not go to the starting point of the dongu3 ;75 go to bank0 banksel PORTB bsf PORTB,7 ;76 send cylinder position signal to the main control circuit ;77 20 us delav call delay_20us ;78 makes PORTB,7 low bcf PORTB,7 clrf sayac3 ;79 sayac3=0 goto tekrar ;80

---- ---- -----

6.3 Source Code of the Igniter Circuits

As it is stated before, igniter circuits are simple microcontroller based circuits, they waits for the ignition timing signal from the main control circuit, when they detect the rising edge of the ignition timing signal they start to let the current flow through the primary winding of ignition coils, then they start to detect the falling edge of the ignition timing signal. When they detects the falling edge of the ignition timing signal they break the current which flows through the ignition coil and initiate the spark generation. They have simple source code as below. As it can be understood, it is using the pin 5 of PORTB as input and pin 0 as output; the command lines 1, 2 and 3 are used to configure pin 5 of PORTB as input and the other pins of PORTB as output. The analog pins of the circuit are also configured as digital with the command lines 7 and 8, these pins may be used as input. The subroutine "RB5_TEST" is dedicated to detect the rising edge of the ignition timing signal which is connected to the pin 5 of PORTB, when it detects the rising edge; it makes the pin 0 of PORTB high with the command line 11 and goes to subroutine "RB5_TEST_low", this routine is dedicated to detect falling edge of the ignition timing signal. When it detects the falling edge it makes pin 0 of PORTB low and goes to "RB5_TEST".

----- ----- -----

	movlw BANKSEL movwf MOVLW MOVWF BANKSEL MOVLW MOVWF	b'00100000' TRISB TRISB H'FF' TRISA PORTB h'07' CMCON	;1 ;2 ;3 ;4 ;6 ;7
RB5_TES	т		
	BTFSS GOTO BSF	PORTB,5 RB5_TEST PORTB,0	;9 ;10 ;11
RB5_TES	T_low		
END	BTFSC GOTO BCF GOTO	PORTB,5 RB5_TEST_low PORTB,0 RB5_TEST	;12 ;13 ;14 :15 ;16

CHAPTER 7

EXPERIMENTAL RESULTS

In this study, a microcontroller based ignition system was designed and constructed for a special type of engine which is a new design. There are some design criteria which shall be achieved. In this chapter, those design criteria and how they were achieved will be stated. The design criteria can be stated as follows: Data transfer speed of the control circuits, correct advance angle, noise free ignition signals and spark quality. The data shown on figures 7.2, 7,3, 7.4 and 7.5 are collected with the DS1000 series Rigol digital oscilloscope.

7.1 Data Transfer Speed

The maximum speed of engine for which our ignition system is designed, is 3000 rpm. So, our system shall be fast enough to follow engine at 3000 rpm. Figure 7.1 shows ignition points of the engine and angle between two ignitions.

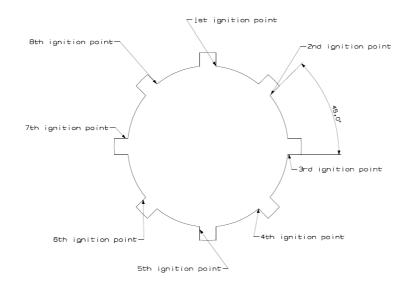


Figure 7.1: Ignition points of the engine

In our system, advance angle determination takes place between 8th ignition and 1st ignition as seen in Figure 7.1. There is 45° between two ignition points; during the determination two analog to digital conversions, mathematical operations and advance angle reading from external eeprom take place. These operations shall be completed before the 1st ignition point. From the equation 5.7 in chapter 5, the maximum time interval in which our system shall complete all operations to determine advance angle value, can be found. According to the equation: Maximum Time interval = (1000*60) / (8*3000)

= 2.5 ms

Our main control circuit makes one of its pins high to tell it is ready for data transfer and makes low when it completes all operations to find advance angle value. The time which the pin stays at logic high gives the time consumed for all operations. Figure 7.2 shows consumed time during those operations. It is around 1.5 milliseconds; it is acceptable because it means our system can work at 5000 rpm.

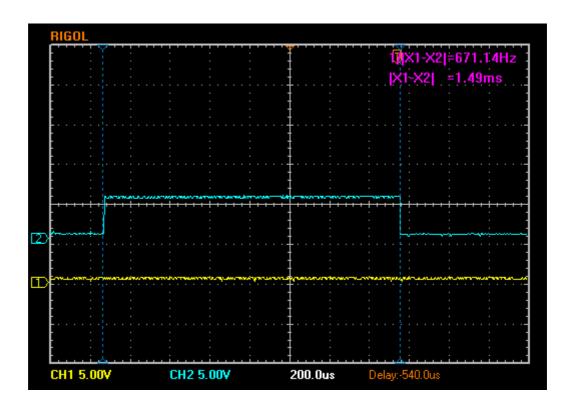


Figure 7.2: Time consumed during advance angle value determination

7.2 Advance Angle

Another requirement which shall be met is correct advance angle. Our system was tested for different engine speeds. Firstly, it is tested for engine speed which outputs 1 volt. The result of the test is given in Figure 7.3. The value X1-X2 in the figure gives the advance delay.

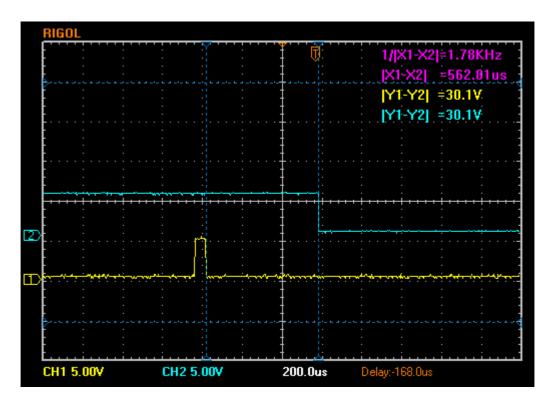


Figure 7.3: Advance delay for 1 Volt

According to equation 5.9 in chapter 5, the calculated advance delay will be as follow:

Advance delay = $[1 / (4*4.8876 \times 10^{-3})]*11 \,\mu s$

When we compared with the experimental result, it seems pretty good. But it is difficult to get exact value on the graph because the positions of the cursors adjusted manually. Secondly, it is tested for 2 volts; the related result is given in figure 7.4. According to equation 5.9 the advance delay would be as follow:

Advance delay = $[2 / (4*4.8876 \times 10^{-3})]*11 \,\mu s$

 $= 1125.3 \,\mu s$

The experimental result is 1.09 ms, but calculated one is around 1.13millisecond.

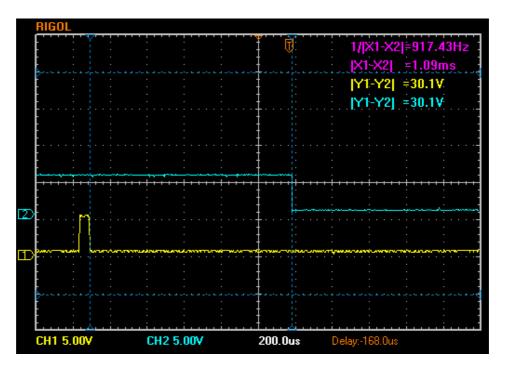


Figure 7.4: Advance delay for 2 Volts

Finally, the system is tested for 3 volts; the experimental result is given in Figure 7.5

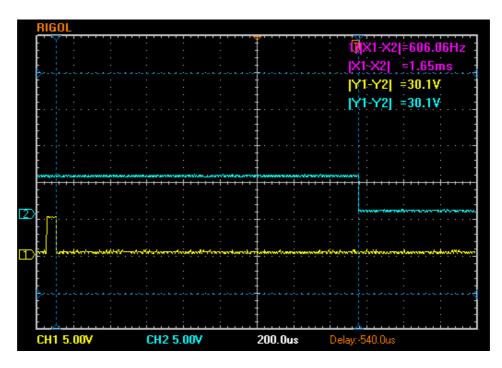


Figure 7.5: Advance delay for 3 Volts

The calculated advance delay is: Advance delay = $[3 / (4*4.8876 \times 10^{-3})]*11 \ \mu s$ = 1687.95 \ \mu s

The experimental results and calculated results were given above, there are small negligible differences. The reasons of these small differences can be stated as follows: With the 8-bit microcontrollers, floating point calculations cannot be done; this is one of the reasons. To adjust the positions of cursors on the graph to get exact numbers is so difficult. Engine speed outputs were measured 1, 2, and 3 volts but the voltmeter which was used to measure these values has a measuring tolerance. While calculating advance delays with equations 5.3 and 5.9 we used Vref⁺ as 5 volts, but the voltage regulators which are assembled on our control circuits, have ± 4 % output voltage tolerances; this may be stated as another reason. As stated above, there are small negligible differences between calculated and experimental results; the Table 7.1 gives tabulated results and the percentage of differences.

Table 7.1: Tabulated results and errors	Table 7.1:	Tabulated	results	and errors
--	-------------------	-----------	---------	------------

Test	Calculated	Experimental	Error (%)
Speed(volts)	Result(µs)	Result(µs)	
1	562.65	562.81	0.03
2	1125.3	1090	3.1
3	1687.95	1650	2.2

7.3 Noise Free Ignition Signals

Control software was developed in Delphi 4.0; it is working with a data acquisition card. The digital inputs of the card are connected to ignition signal pins. With this control software we are able to scan ignition signals for a while and see whether there is a discontinuity or not. To check conditions of ignition signals such a scanning operation is held around maximum operating speed and figure 7.6 shows result of scanning. As seen in the figure, the result is acceptable there is no

discontinuity in ignition signals and their positions according to each other are as expected.

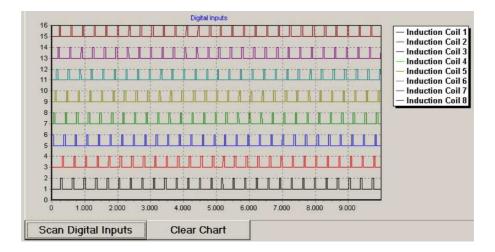


Figure 7.6: Ignition signals

7.4 Spark Quality

For the time being, there is no criterion for spark quality, so the spark quality was checked visually. Figure 7.7 shows a photo during spark generation, the spark seems reasonable.



Figure 7.7: Spark generated by our igniter circuit

CHAPTER 8

DISCUSSION AND CONCLUSION

In this study, electronic ignition system was designed and constructed for a special type of engine which was designed by Prof. A. Demir BAYKA. The engine has different working principle than the engines which are assembled on the cars in the market. There are many parts which were done during the study. First of all, two PIC16F877A based circuits were designed and related ports and pins were determined. Then, communication procedures between those two circuits were developed and working conditions were simulated with a signal generator and a power supply. With that simulation, bugs of the microcontroller codes were eliminated and the code was optimized. Then, the related hardware such as sensors, induction coils, spark plugs and igniter circuit were assembled and two PIC16F877A based circuits were faced, advantages and disadvantages of the system and further recommendations related to the system will be stated.

The designed and constructed system is able to measure engine working conditions such as engine speed and the cooling water temperature, and it is able to adopt itself to those working conditions. It can detect cylinder position signals and determine the correct ignition points according to changing engine conditions. There are 8 igniter circuits and they are able to be triggered by the main control circuits with logic level signals. There are 2 control circuits and they are able to read 5 analog sensor outputs.

As it is stated in part 7.1, the necessary operations to find advance delay take place between ignition points 8 and 1; the angle between those two ignition points is 45°. For 3000 rpm, the engine travels 45° in 2.5 ms, so our control circuits shall complete all necessary communications and calculations in a time interval less than 2.5 ms. Figure 7.2 shows measured time interval in which all necessary operations take place to find advance delay. The result is around 1.5 ms; it is so good result because it means our system can work at around 5000 rpm. Also, this rpm value can be increased by optimizing communication and calculation rates, and changing 4MHz crystal with a high speed crystal.

The experimental results of advance delay were given in part 7.2; they are actually pretty good results, because the system can change the advance delay according to engine speed. There are also small difference between calculated results and experimental results; the reasons of those differences were given in chapter 5. Those differences are because of output tolerances of voltage regulators, measuring tolerances of voltmeter, lack of ability for floating point calculation and resolution of result graphs. The source code of control circuits were tested to check whether it is working correctly or not. For this purpose, the same advance value was written to all eeprom addresses and it was read and displayed in light emitting diodes which are connected to PORTB of main control circuits. The main control circuit was able to read and display the written value to eeprom addresses perfectly. So, the problems related to source codes which determine advance delay were not stated as a reason of differences between experimental and calculated results. In part 7.3, the ignition signals which are generated by the control circuits were given. As seen in Figure 7.6, there is no discontinuity in the signals. It means, the control circuit receives ignition timing signals and sends ignition signals correctly. In the next part, a figure shows generated spark was given. As seen in the figure, it is good enough to be seen in the day light. Actually, the spark quality is better in cylinder during combustion when it is compared with a generated spark in the atmosphere, because ionization in combustion chamber is higher because of higher temperature and pressure. It means the generated spark which is shown in Figure 7.7, is good enough and will be better in combustion chamber.

This is an experimental study, and when you working on an experimental study you face with a lot of difficulties. The most difficult thing faced during this study was magnetic field. In chapter 3, EMC is told; electromagnetic compatibility refers to the ability of equipment or a system to perform satisfactorily in its electromagnetic environment without introducing intolerable interference into anything in that environment. The ignition cable or induction coil manufacturers take into account electromagnetic compatibility, but the microcontrollers and frequency to voltage converters which were used on the circuits are very sensitive to electromagnetic

field. The biggest source of electromagnetic interference is AC motor which was used to simulate engine speed in our experimental set-up. To overcome this difficulty, decoupling capacitors were used on frequency to voltage converter circuits to eliminate noise caused by AC motor. Also, the motor was put into metal cage which is called Faraday cage to block static or non-static electric fields. Another difficulty with which was faced was high voltage. To generate spark, the voltage is increased up to 20-30 kV; it is so high voltage because of this reason it can jump to anywhere by following the shortest way. The experimental set-up had been placed on a wooden table with metal chassis and all igniter circuits and control circuits were on the same table. The high voltage jumped to igniter circuits because the bottom surfaces of igniter circuits were not isolated and wooden was not a good isolating material. After that experience, all circuits were isolated with a good resistant material. The PIC microcontrollers which were used on the system have both digital and analog input pins. The analog pins are affected by electromagnetic field, so these pins should not be used as input pin. As it is stated above, the difficulties which were faced during the study may be stated as disadvantages of our system because the circuits which were used are not professionally soldered and isolated circuits. So, they are affected by electromagnetic field and high voltage easily. In modern automotive applications, ECU (Engine control unit) is used to control the processes during engine running to ensure the optimum running conditions. These units are microcontroller based circuits, too. However, they are designed to work in tough conditions, so they are not affected by electromagnetic field, vibration, temperature, etc. A commercial engine control unit might be modified to use in our application, but it would be very difficult to use because manufacturers make them too complicated to protect them against being copied. Advance angle map will be generated according to our special engine if we had used a commercial ECU, we would not have chance to change advance map of the ECU according to our special engine. To design and construct a PIC16F877A based circuit, and use it as control circuit is the easiest way because PIC16F877A is most popular microcontroller unit and you can find thousands of source codes on the internet. Also, PIC16F877A microcontroller is so cheap, easy to use and easily found in the market; these may be stated as advantage of our system.

As it is told in previous chapters, there are two PIC16F877A based circuits and they communicate via Master–Slave serial communication, this communication type is enough for this application, but if there were another circuit and if you needed to communicate with that circuits; traditional serial communication would not be enough. A modern car has around 70 control circuits, some of these circuits are independent systems, but most of them communicate with each others, so a special communication standard called as CAN is developed for automotive industry in 1980's. This is a multi-master broadcast serial bus standard for connecting control circuits; and all circuits is able to send and receive messages. There are a few PIC microcontrollers which have CAN interface, but PIC16F877A does not have such an interface. This is another disadvantage of our system. The igniter circuits open and close primary voltage of induction coils with mosfets, IRF540N; these mosfets are driven by optocouplers, 4N35. The turn on and turn off times of 4N35 are around 10µs, actually turn off time is more important for us because ignition takes place by closing of mosfet. The turn off time of 4N35 may be accepted, but there are some optocouplers which have better closing times such as 6N139. Its turn off time is around 1µs. The optocouplers on the igniter circuits are used to drive mosfets, because IRF540N is not driven by logic signal, but there are some logic mosfets in the market such as IRL540 or IRLZ44, these mosfets can be driven by microcontrollers without a optocoupler. These options may be used in the future works of our ignition system

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APPENDIX A: SOURCE CODE OF THE MAIN CONTROL CIRCUIT

• * * * * * ,	************************
;	Source Code of Main Control Circuit
• * * * * *	***************************************
	list p=16f877A
	<pre>#include <p16f877a.inc></p16f877a.inc></pre>
	config H'3F31'

delay_ms_data	equ 0x20	;variable for delay
		;subroutine
sicaklikH	equ 0x22	;higher value byte cooling
		;water
		;temperature
tempH	equ 0x23	;serial rpm data
bolum	equ 0x24	;5-bit form of
		;SicaklikL+sicaklikн
sayacH	equ 0x25	;temporary variableto arange
		;ignition mode
kontrol_register	equ 0x26	;variable to detect
		;comunication error
sicaklikL	equ 0x27	;lower value byte of cooling
		;water
		;temperature

avans ADC_Oku_kanalno	equ 0x28 equ 0x70	;advance angle value ;Analog channel number
ADC_Oku_sonucbyte	equ 0x71	;ADRESL-ADRESH selection ;variable
mode_sayac	equ 0x72	;variable to arrange ;ignition mode
deneme	equ 0x73	;temporary variable for port
I2CSend_Data I2C_Device	equ 0x74 equ 0x75	;configuration ;Data sent with I2C ;hardware address of ;external eeprom
I2C_AdrH	equ 0x76	;higher value byte of ;external ;eeprom address
I2C_AdrL	equ 0x77	;lower value byte of ;external ;eeprom address
I2C_Data	equ 0x78	;advance angle value read ;from the eeprom

ORG	0x000
clrf	PCLATH
goto	main
ÕRG 4	

; interrupt subroutine is fired when the ; TimerO is up

interrupt		
btfss	INTCON, 5	;1 checks whether the Timer0
		; interrupt ; is activated or not?
goto btfss	int_j1 INTCON, 2	;2 if not? goto int_j1 ;3 checks whether the Timer0
goto	int_j1	; interrupt is fired or not ;4 bit 2 of INTCON register ; is set when ; the timer fires if not? ; go to int_j1
movlw	D'6'	;5 initial value of TimerO ; for 2 ms timer period
mo∨wf bcf bsf	TMRO INTCON, 2 kontrol_register,1	;6 ;7 clear the flag of Timer0 ;8 kontrol_register is ; defined to check ; whether 2ms period was ; exceeded or not ; this register may be used
		; durig the ; serial communication ; between two ; control circuits.

int_j1 retfie

;9 exit from the subroutine

r	nain	call	initialize		;10	calls the subroutine "initialize"
		call	ilk_islemler		,11 ,	calls the subroutine "ilk_islemler"
-	lоор	bsf POR	TD,1		;12	makes the 1st pin of PORTD high, this is ready signal sent to
		;bsf	INTCON, D'5'		; ;13	the secondary circuit activates the TimerO
		;bsf	INTCON, D'7'		; ;14	overflow interrup activates all interrupts
		nop nop call	snkSlaveRead		;16	no operation no operation calls the subroutine "snkSlaveRead", this subroutine reads synchronous serial data from the secondary circuit and loads it to "W"
		movwf nop nop	tempH		; ,19	loads the serial data read by "snkSlaveRead" to the variable "tempH" no operation no operation
		movlw	0x00			analog channel 0 is
		movwf	ADC_Oku_kanalno		; ;22	selected
		mo∨lw	0x00		;23	the value 0x00 is loaded to
		movwf	ADC_Oku_sonucbyt	2	,24	"ADC_Oku_kanalno" read the low byte (ADRESL) of analog digital conversion PIC16F877A has 10-bit ADC module so the result of ADC is 2 bytes (they are called high byte and low byte) PIC16F877A is a 8-bit microcontroller and has 8-bit registers so we should call "ADC_Oku" twice to read 10-bit data
		call	ADC_Oku		;25	calls the subroutine "ADC_Oku", this subroutine reads the analog value and converts it into digital
	;	Banksel movwf	PORTB PORTB			go to bank0 may be used to see the result of ADC with the leds of PORTB
				120		

	movwf	sicaklik∟	;28 ;	loads the value read by "ADC_Oku" to the "sicaklikL"
	nop nop nop nop		;30 ;31	no operation no operation no operation no operation
	movlw movwf	0x00 ADC_0ku_kana1no	;33 ;34 ;	analog channel 0 is selected
	movlw movwf	0x01 ADC_Oku_sonucbyte	;35 ;36 ;	value 0x01 is loaded to "ADC_Oku_sonucbyte" it means "read the high byte of ADC
	call	ADC_Oku	;37 ;	calls the subroutine "ADC_Oku"
;	Bankse movwf	l portb portb	; 39	go to bank0 may be used to see the result of ADC with the leds of PORTB
	movwf	sicaklikн	,40	loads the value read by "ADC_Oku" to the "sicaklikH"
	movlw movwf		;41 ;42 ;	initial value of "bolum" is zero
; value	into 5	ine is used to scale th -bit. This is 16-bit di result)/33	e 10-b [.] vision	it digital operation
dongu2				
	movlw subwf btfss	d'33' sicaklikL,1 STATUS,C		sicaklikL=sicaklikL-33 if the new value of sicaklik is negative (checks the overflow of 7th bit) "C" bit of STATUS is set to zero when the result of
	goto incf goto incf bsf	<pre>\$+3 bolum,1 dongu2 bolum,1 STATUS,0</pre>	;47 ;48 ;49	mathematical operation go to line 49 bolum=bolum+1 go to line 43 bolum=bolum+1 set "C" bit of STATUS to 1 for the next operation
	movlw subwf	d'1' sicaklikH,1	;51 ;52	sicaklikH=sicaklikH-1
	btfss	STATUS,C	;53	if there is an overflow
	goto goto decf goto	\$+2 \$+3 bolum,1 \$+2	;56	go to line 56 go to line 56 go to line 58 bolum=bolum-1 go to line 59
		130		

	goto	dongu2	;58 ;	go to the starting point of the "dongu2"	
	movf movwf	tempH,O sayacH	;	W=tempH, this line loads the value of tempH to sayacH=W it means sayacH=tempH	
	clrf clrf	I2C_Device I2C_AdrH	;61 ;62	I2C_Device=0 I2C_AdrH=0 because we did not use the cooling water temperature for this study but it may be used in the future (it may be the output of any sensor with analog output)	
	mo∨f mo∨wf	sayacH,0 I2C_AdrL		W=sayacH I2C_AdrL=sayacH	
	call	I2C_ReadEE	;65 ;	calls the subroutine "I2C_ReadEE" which reads 8-bit data from the external eeprom	
	bcf	PORTD,1	;66 ; ; ;	makes the 1st bit of PORTD logic low elapsed time between line 12 and line 66 gives the required time to read serial rpm data, read analog value and convert it into digital, scale 10-bit ADC result into 5-bit and read the advance value from the external eeprom	
	movwf	avans	;67	loads the value which is read by subroutine "I2C_ReadEE" into "avans"	
	clrf	mode_sayac	;68	initial value of mode_Sayac is zero	
	mo∨f mo∨wf	sayacH,О mode_sayac	,69 ,70	W=sayacH mode_Sayac=sayacH	
	nop nop			no operation no operation	
5	block checks mode_Sayac is greater than				

; this block checks mode_Sayac is greater than ; 175 or not.This means whether the engine speed ; is between 2100 and 3000 rpm or not ; if the result of (mode_Sayac-175) ; is negative STATUS,C will be 0

bcf	STATUS,C	, , , ,	makes STATUS,C zero to guarantee it is not "1" because we are checking it is 1 or not with line 76
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;74 W=175 movlw d'175' ;75 mode_Sayac= subwf mode_sayac,W mode_Savac-175 ;76 whether the result btfss STATUS, C ; of line ; 75 is negative or not ;77 if it is negative go ; to "loop2" goto loop2 ,78 if it is not negative, call mode_3 calls the ignition mode "mode_3" ;79 when the ignition 100p goto sequence is complete, go to the starting of the "loop" "loop2" checks mode_Sayac is greater than 170 or not. This means whether the engine speed is between 2050 and 2100 rpm or not if the result of (mode_Sayac-170) is negative STATUS, C will be 0 loop2 movlw d'170' ;80 W=170 subwf mode_sayac,W ;81 mode_sayac= mode_sayac-170 ;82 whether the result btfss STATUS,C of line 81 is negative or not ;83 if it is negative go to ; "loop3" 100p3 goto ;84 if it is not negative, call premode_3 calls the ignition mode "premode_3" 85 when the ignition loop goto sequence is complete, go to the starting of "loop" "loop3" checks mode_Sayac is greater than ; 117 or not. This means whether the engine speed ; is between 1400 and 2050 rpm or not ; if the result of (mode_Sayac-117) ; is negative STATUS,C will be 0 100p3 d'117' ;86 W=117 movlw ;87 mode_sayac= subwf mode_sayac,W mode_sayac-117 btfss STATUS,C ;88 whether the result of line 87 is negative or not ;89 if it is negative go ; to "loop4" ;90 if_it is not negative, loop4 goto call mode_2 calls the ; ignition mode "mode_2"

goto 100p ;91 when the ignition sequence is complete, go to the starting of the "loop" ; "loop4" checks mode_Sayac is greater than 113 or not. This means whether the engine speed is between 1350 and 1400 rpm or not if the result of (mode_Sayac-113) is negative STATUS, C will be 0 100p4 ;92 W=113 movlw d'113' ;93 mode_sayac= subwf mode_sayac,W mode_sayac-113 btfss STATUS,C ;94 whether the result of line 93 is negative or not ;95 if it is negative go ; to "loop5" ;96 if it is not negative, ; calls the loop5 goto call premode_2 ignition mode "premode_2" 97 when the ignition goto loop sequence is complete, go to the starting of the "loop' "loop5" checks mode_Sayac is greater than 58 or not. This means whether the engine speed is between 700 and 1350 rpm or not if the result of (mode_Sayac-58) is negative STATUS, C will be 0 100p5 ;98 W=58 ;99 mode_sayac= d'58' movlw mode_sayac,W subwf mode_sayac-58 ;100 whether the result ; of line 99 ; is negative or not btfss STATUS,C ;101 if it is negative go ; to "loop6" ;102 if it is not negative, goto 100p6 call mode_1 calls the ignition mode "mode_1" 103 when the ignition goto loop sequence is complete, go to the starting of the "loop" "loop6" checks mode_Sayac is greater than 54 or not. This means whether the engine speed ; is between 650 and 700 rpm or not ; if the result of (mode_Sayac-54) ; is negative STATUS,C will be 0

100p6

	movlw subwf	d'54' mode_sayac,W	;105	W=54 mode_sayac= mode_sayac-54
	btfss	STATUS,C	;106 ; ;	whether the result of line 105 is negative or not
	goto	loop7	;107	if it is negative go
	call	premode_1	,108	to "loop7" if it is not negative, calls the ignition mode
	goto	Тоор	,109	"premode_1" when the ignition sequence is complete, go to the starting of the "loop"
loop7" checks mode_Sayac is greater than				

; "loop7" checks mode_Sayac is greater than ; 1 or not. This means whether the engine speed ; is between 0 and 650 or not ; if the result of (mode_Sayac-1) ; is negative STATUS,C will be 0

loop7

movlw subwf	d'1' mode_sayac,W	;110 ;111	W=1 mode_sayac=mode_sayac-1
btfss	STATUS,C	;112 ;	whether the result of line 111 is negative or not
goto	Тоор	;113	if it is negative go to
call	mode_0	; ;114 ;	starting of the "loop" if it is not negative, calls the ignition mode "mode_0"
goto	Тоор	;	when the ignition sequence is complete, go to the starting of the "loop"

;ignition mode "mode_0 is the ignition mode for the ;lowest engine speed ;engine speed low enough to saturate the ignition ;coil after cylinder position signal comes ;cylinder position signal does not give the actual position ;of the cylinder, it gives the 22.5 degree before the cylinder ;it is the middle of two cylinders

btfss	portd,0	,	did the secondary circuit send the 1st cylinder position? if yes go to the line 118
		;	line 118

goto	\$-1	;117	'if not go to line 116 and wait
btfsc goto	PORTD,0 \$-1	;	for the signal for the signal ignition process will starting with the falling edge of the cylinder position signal so wait for the falling edge. if PORTD,0 is low, go to line 120, if not wait for the falling edge go to line 118
bankse	avans,0 1 PORTB PORTB,7	;121	W=avans go to bank0 makes the 7th bit of PORTB high, this is ignition signal and 1st igniter circuit lets the current flow through the primary winding of the 1st ignition coil
mo∨wf	delay_ms_data	;123	delay_ms_data= avans,this is the duration which PORTB,7 stays at logic high state
call	delay_ms	,124	calls "delay_ms"
bcf	PORTB,7	,125	subroutine, makes PORTB,7 logic low, this is the end of ignition signal igniter circuit breaks the current which is flowing through the primary coil of the first ignition coil and spark occurs
btfss	portd,0	;126	did the secondary circuit send the 2nd cylinder position? if yes, go
goto	\$-1	,127	to the line 128 if not go to line 126 and
btfsc	portd,0	128	wait for the signal ignition process will starting with the falling edge of the cylinder position signal so wait for the falling edge. if PORTD,0 is low, go to line 130,
goto	\$-1	,	f not wait for the falling edge
		135	

movf avans,0 banksel PORTB bsf PORTB,6	go to line 128 130 W=avans 131 go to bankO 132 makes the 6th bit of PORTB high, this is ignition signal and 2nd igniter circuit lets the current flow through the primary winding of the 2nd ignition coil
movwf delay_ms_data	;133 delay_ms_data=avans, ; this is the duration ; which PORTB,6 stays at
call delay_ms bcf PORTB,6	; logic high state ;134 calls the subroutine ; "delay_ms" ;135 makes PORTB,6 ; logic low, ; this is the end of ; ignition signal
	; igniter circuit ; breaks the ; current which is ; flowing through ; the primary coil ; of the 2nd ; ignition coil and ; spark occurs
btfss PORTD,0	;136 did the secondary ; circuit send the 3rd ; cylinder position? ; if yes,
goto \$-1	; go to the line 138 ;137 if not go to line 136 ; and
btfsc PORTD,0	wait for the signal 138 ignition process will starting with the falling edge of the cylinder position signal so wait for the falling edge. if PORTD,0 is low, go to line 140,
goto \$-1	139 if not wait for the falling
movf avans,0 banksel PORTB bsf PORTB,5	; edge go to line 138 ;140 W=avans ;141 go to bank0 ;142 makes the 5th bit ; of PORTB ; high, this is ; ignition signal ; and 3rd ; igniter circuit ; lets the current ; flow through the ; primary winding ; of the 3rd
13	; ignition coil 36

movwf call bcf	-		;144	delay_ms_data=avans calls the subroutine "delay_ms" makes PORTB,5 logic low, this is the end of ignition signal igniter circuit breaks the current which is flowing through the primary coil of the 3rd ignition coil and spark occurs
btfss	portd,0		;146	did the secondary circuit send the 4th cylinder position? if yes,
goto	\$-1		, 147	go to the line 148 if not go to line 146 and wait
btfsc	portd,0		,148 ,,	for the signal ignition process will starting with the falling edge of the cylinder position signal so wait for the falling edge. if PORTD,0 is low, go
goto	\$-1		,149	to line 150, if not wait for the falling
	avans,0 1 PORTB PORTB,4		;151	edge go to line 148 W=avans go to bank0 makes the 4th bit of PORTB high, this is ignition signal and 4th igniter circuit lets the current flow through the primary winding of the 4th ignition coil
movwf call	delay_ms_data delay_ms		,153 ,154	delay_ms_data=avans calls the subroutine "delay_ms"
bcf	PORTB,4		,155	makes PORTB,4 logic low this is the end of ignition signal igniter circuit breaks the current which is flowing through the primary coil of the 4th ignition coil and spark occurs
btfss	portd,0	137	;156 ;	did the secondary circuit send the 5th cylinder position?

goto			;	if yes, go to the line 158 if not go to line 156 and wait for the signal
bt†sc	portd,0		;158	ignition process will starting with the
			;	falling
			;	edge of the cylinder position signal
			,	so wait for the falling edge.
			;	if PORTD.0 is low.
goto	\$-1		;	go to line 160, if not wait for the
9	• -		;	falling
movf	avans,0		;160	edge go to line 158 W=avans
bankse bsf PO	1 PORTB		;161	go to bankO makes the 3rd bit of
051 PU	, , , , , , , , , , , , , , , , , , , ,		;	PORTB high, this is
			;	ignition signal and 5th igniter circuit
			;	lets the current flow
			,	through the primary winding of the 5th
mov/wf	delay_ms_data		;	ignition coil delay_ms_data=avans
call	delay_ms		;164	calls the subroutine
bcf	PORTB,3		; ;165	"delay_ms" makes PORTB,3
			;	makes PORTB,3 logic low, this is the end of
			;	ignition signal
			,	igniter circuit breaks the current which is
			,	flowing through the primary coil
			;	of the 5th
			;	ignition coil and spark occurs
btfss	portd,0		:166	did the secondary
	, .		;	circuit
			,	send the 6th cylinder position? if
goto	\$-1		;	yes, go to the line 168 if not go to line
goco	÷ -		;;	166 and
btfsc	portd,0		; 168	wait for the signal ignition process will
			,	starting with the falling edge of the
			,	cylinder position signal
			;	so wait for the
			; ; if	falling edge. PORTD,0 is low,
aoto	\$-1		; 169	go to line 170, if not wait for
goto	Ψ⊥		;	the falling
movf	avans,0			edge go to line 168 W=avans
bankse bsf PO	1 PORTB		;171	go to bank0 makes the 2nd bit of
531 FU	, , , , , , , , , , , , , , , , , , ,		; 1/2	PORTB high, this is
			,	ignition signal and 6th igniter circuit
			,	lets the current flow through the primary
		138	,	the primary

movwf call bcf	delay_ms_data delay_ms PORTB,2		;174	winding of the 6th ignition coil delay_ms_data=avans calls the subroutine "delay_ms" makes PORTB,2 logic low, this is the end of ignition signal igniter circuit breaks the current which is flowing through the primary coil of the 6th ignition coil and spark occurs
btfss	portd,0		,	did the secondary circuit send the 7th cylinder position? if yes,
goto	\$-1		; ,177	go to the line 178 if not go to line 176
btfsc	portd,0		;	and wait for the signal ignition process will starting with the falling edge of the cylinder position signal so wait for the falling edge. if PORTD,0 is low,
goto	\$-1		, 179	go to line 180, if not wait for the falling
bankse bsf	avans,0 1 PORTB PORTB,1		,181 ,182	edge go to line 178 W=avans go to bank0 makes the 1st bit of PORTB high, this is ignition signal and 7th igniter circuit lets the current flow through the primary winding of the 7th ignition coil
movwf	· · ··)_ · _·			delay_ms_data=avans
call bcf	delay_ms PORTB,1		;	calls the subroutine "delay_ms" makes PORTB,1 logic low, this is the end of ignition signal igniter circuit breaks the current which is flowing through the primary coil of the 7th ignition coil and spark occurs
btfss	portd,0	139	;186 ;	did the secondary circuit send the 8th cylinder

			;		position? if yes, go to
-	goto otfsc	\$-1 portd,0	;	187	the line 188 if not go to line 186 and wait for the signal ignition process will starting with the
			9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9 9		falling edge of the cylinder position signal so wait for the falling edge. if PORTD,0 is low, go to line 190,
g	joto	\$-1	;1	189	if not wait for the falling edge go to line 188
b	oankse1	avans,0 PORTB PORTB,0	;1	190 191 192	W=avans go to bank0 makes the Oth bit of PORTB high, this is ignition signal and 8th igniter circuit lets the current flow through the primary winding of the 8th
m		delay_ms_data delay_ms	;1 ;1	193	ignition coil delay_ms_data=avans calls the subroutine
b	ocf	portb,0	, 1 ,		"delay_ms" makes PORTB,0 logic low, this is the end of ignition signal igniter circuit breaks
r	return		; ; ; 1		the current which is flowing through the primary coil of the 8th ignition coil and spark occurs quit from the loop,
;mode_0 a ;preparat ;for engi ;there is	and mod tion fo ne spe s only	tion mode is a tra le_1. The aim of th or the mode_1 eds between 650 ar one difference bet that is line 277	nis mode i nd 700 rpm	is n	between
premode_1	L				
b	otfss	portd,0	;1		did the secondary circuit send the 1st cylinder position? if yes, go to the line 199
g	joto	\$-1	;1	198	if not go to line 197 and wait for the signal
b	otfsc	portd,0	;1		ignition process will starting with the falling edge of the cylinder position signal so wait for the falling edge.

bankse	\$-1 avans,0 1 PORTB PORTB,7		<pre>if PORTD,0 is low, go to line 201, 200 if not wait for the falling edge go to line 199 201 W=avans 202 go to bank0 203 makes the 7th bit of PORTB high, this is ignition signal and 1st igniter circuit makes the 7th bit of PORTB high, this is ignition signal and</pre>
movwf call bcf	-		<pre>ist igniter circuit 204 delay_ms_data=avans 205 calls the subroutine "delay_ms" 206 makes PORTB,7 logic low, this is the end of ignition signal igniter circuit breaks the current which is flowing through the primary coil of the 1st ignition coil and spark occurs</pre>
btfss goto	PORTD,0 \$-1		;207 The lines between ; 207 and 216 ;208 are the same operations
btfsc goto movf bankse bsf PO movwf call	PORTD,0 \$-1 avans,0 1 PORTB RTB,6 delay_ms_data		; for 2nd ignition coil ;209 ;210 ;211 ;212 ;213 ;214 ;215 ;216
btfss goto	PORTD,0 \$-1		;217 The lines between ; 217 and 226 ;218 are the same operations
btfsc goto movf bankse bsf PO	PORTD,0 \$-1 avans,0 1 PORTB RTB,5 delay_ms_data		for 3rd ignition coil 219 220 221 222 223 224 225 226
btfss goto btfsc goto movf	PORTD,0 \$-1 PORTD,0 \$-1 avans,0	141	;227 The lines between ; 227 and 236 ;228 are the same operations ; for 4th ignition coil ;229 ;230 ;231

	bsf movwf	l PORTB PORTB,4 delay_ms_data delay_ms PORTB,4		;232 ;233 ;234 ;235 ;236
		PORTD,0		;237 The lines between ; 237 and 246
	goto	\$-1		;238 are the same operations ; for 5th ignition coil
	goto movf bankse bsf movwf	avans,0 1 PORTB PORTB,3 delay_ms_data delay_ms		239 ;240 ;241 ;242 ;243 ;244 ;245 ;246
	btfss	portd,0		;247 The lines between ; 247 and 256
	goto	\$-1		;248 are the same operations
	goto movf bankse bsf movwf	avans,0 PORTB PORTB,2 delay_ms_data delay_ms		; for 6th ignition coil ;249 ;250 ;251 ;252 ;253 ;254 ;255 ;256
	btfss	portd,0		;257 The lines between ; 257 and 256
	goto	\$-1		; 258 are the same operations ; for 7th ignition coil
	goto movf			;259 ;260 ;261 ;262 ;263 ;264 ;265 ;266
	btfss	portd,0		;267 The lines between
	goto	\$-1		; 267 and 278 ;268 are the same operations
	btfsc goto movf bankse bsf movwf call bcf bsf	PORTD,0 \$-1 avans,0 PORTB PORTB,0 delay_ms_data delay_ms PORTB,0 PORTB,7		for 8th ignition coil 269 270 271 272 273 274 275 276 277 the 1st igition coils is started to be
				; saturated at this ; point for the the
mode_1	return		142	;278

;this mode is for higher speeds than mode_0 ;this is the ignition mode for engine speeds ;between 700 and 1350 rpm. For these engine speeds ;there is not enough time to saturate the ignition coils ;between two cylinder position signals. So the ignition coils ;should be started to be satureted before the cylinder position ;signal

btfss	portd,0			;279	did the secondary
				;	circuit
				;	send the 1st
				;	cylinder position?
				;	if yes,
					go to the line 281
goto	\$-1			:280	if not go to line
5				;	279 and
					wait for the signal
btfsc	portd,0			281	ignition process will
					starting with the
					falling
				;	edge of the cylinder
				;	position signal
				;	so wait for the
				;	falling edge.
				;	if PORTD,0 is low, go to line 283,
				;	go to line 283,
goto	\$-1			;282	if not wait for
				;	the falling
_	_			;	edge go to line 281
movf	avans,0			;283	W=avans
	PORTB_			;284	go to bank <u>0</u>
bst	PORTB,7			;285	makes the 7th bit
				;	of PORTB high,
				;	to guarantee
				,	the start of
				,	saturation of 1st
max	dalay ma data			;	igniter circuit
call	delay_ms_data			,200	delay_ms_data=avans
Call	delay_ms			,207	calls the subroutine "delay_ms"
bcf	PORTB,7			, 288	makes PORTB,7 logic
DCT	FURID,7			,200	low, this
					is the end of
					ignition signal
					igniter circuit
				;	breaks the
				:	current which is
				÷	flowing through
				;	the primary coil of
				;	the 1st
				;	ignition coil and
				;	spark occurs
bsf	PORTB,6			;289	makes PORTB,6
				;	logic high,this
				;	is the starting
				;	point_of ignition
				;	signal
				;	for 2nd ignition coil
h+fcc				. 200	The lines between
btfss	portd,0			,290	The lines between 290 and 300
goto	\$-1			,291	are the same operations
9000	Ψ -	1	43	,291	
			↔ 1		

goto movf bankse bsf movwf call	PORTB.6		for 2nd and 3rd 292 ignition coils 293 294 295 296 297 298 299 300
goto btfsc goto movf bankse bsf movwf call	PORTD,0 \$-1 PORTD,0 \$-1 avans,0 PORTB PORTB,5 delay_ms_data delay_ms PORTB,5 PORTB,4		301 The lines between 301 and 312 302 are the same operations for 3rd and 4th 303 ignition coils 304 305 306 307 308 309 310 312
btfss goto	PORTD,0 \$-1		;313 The lines between ; 313 and 323 ;314 are the same operations
goto movf bankse bsf PO movwf	avans,0 l PORTB RTB,4 delay_ms_data delay_ms PORTB,4		; for 4th and 5th ;315 ignition coils ;316 ;317 ;318 ;319 ;320 ;321 ;322 ;323
btfss goto	PORTD,0 \$-1		;324 The lines between ; 324 and 334 ;325 are the same operations
goto movf bankse bsf movwf call			; for 5th and 6th ;326 ignition coils ;327 ;328 ;329 ;330 ;331 ;332 ;333 ;334
btfss	portd,0		;335 The lines between ; 335 and 345
goto	\$-1 DODTD 0		336 are the same operations for 6th and 7th
goto movf bankse	1 PORTÉ PORTB,2	144	;337 ignition coils ;338 ;339 ;340 ;341 ;342

	call bcf bsf		;343 ;344 ;345	
	btfss	portd,0	;346	The lines between
	goto	\$-1	,347	346 and 356 are the same operations for 7th and 8th
	goto movf bankse bsf	avans,0 PORTB PORTB,1 delay_ms_data delay_ms PORTB,1	348 349 350 351 352 353 354 355 356	ignition coils
	btfss	portd,0	;357	The lines between
	goto	\$-1	,358	346 and 356 are the same operations for 8th and 1st
	goto movf bankse bsf movwf call bcf	PORTD,0 \$-1 avans,0 PORTB PORTB,0 delay_ms_data delay_ms PORTB,0 PORTB,7	;360 ;361 ;362 ;363 ;364 ;365 ;366 ;367	quit from the loop
;mode_1 ;In ign ;will bo ;The air ;prepara ;for end	and mod ition mode advand n of the ation for gine spe ly diffe	ition mode is a transien de_2. ode_2 the starting point ced more is mode is or the mode_2 eeds between 1350 and 140 erence between mode_1 and	of the	e saturation
			a pi ciii	Juc_2 13
premode <u></u>				Juc_2 13
premode <u></u>	_2 btfss goto btfsc goto movf	PORTD,0 \$-1 PORTD,0 \$-1	;369 ;370 ;371 ;372 ;373 ;374	The first ignition coil was started to be saturated (line 367) with this line we`ve guaranteed the its starting of being saturated

goto btfsc goto movf banksel bsf call bcf btfss goto btfsc goto btfsc goto movf banksel bsf call bcf	PORTB,6 delay_ms_data delay_ms PORTB,6 PORTB,5 PORTD,0 \$-1 PORTD,0 \$-1 avans,0 PORTB PORTB,5 delay_ms_data delay_ms PORTB,4 PORTD,0 \$-1 PORTD,0 \$-1 PORTB,4 delay_ms_data delay_ms PORTB,4 delay_ms_data delay_ms PORTB,4 delay_ms PORTB,4 delay_ms PORTB,4 delay_ms PORTB,3 delay_ms_data delay_ms PORTB,3 delay_ms_data delay_ms PORTB,3 delay_ms_data delay_ms PORTB,3 delay_ms_data delay_ms PORTB,2 PORTB,2 delay_ms_data delay_ms PORTB,2		38456789012345678901234567890112345678901123445678901233456789012345678901233456789012345678901123455678901123456789011234567890112345678901123456789011234567890112345678901123456789011234567890112345678901123456789011234567890112345678901123456789011234567890112345678901123455678901123456789011234556789001123455678900112345567890011234556789000000000000000000000000000000000000
bsf btfss goto btfsc goto	PORTD,0 \$-1 PORTD,0 \$-1 \$-1		;445 ;446 ;447 ;448 ;449
movf	avans,0	146	;450

	bankse	1 PORTB	;45	51
	bsf	portb,0	;45	
	bsf	PORTB,7	;45	53
	mo∨wf	delay_ms_data	ı ;45	54
	call	delay_ms	;45	
	bcf	portb,0	;45	
;	bsf	PORTB,6	;45	
	return		;45	58
: this	is iani	tion mode for	engine speeds	

; this is ignition mode for engine speeds ; between 1400 and 2050 rpm ; In this mode, the starting point of the ignition coils ; is at the cylindir position signal of the previous cylindir

btfss	portd,0		;459 ;	did the secondary circuit send the 1st cylinder position? if yes, go to the line 461
goto	\$-1		; ;460	if not go to line 461 and wait for the signal
btfsc	portd,0		,461 ,	and wait for the signal ignition process will starting with the falling edge of the cylinder position signal so wait for the falling edge. if PORTD,0 is low, go to line 463,
goto	\$-1		,462	if not wait for the falling edge go to line 461
bankse	avans,0 PORTB PORTB,7		:464	W=avans go to bank0 makes the 7th bit of PORTB high,to guarantee
			;	the start of saturation
			,	of 1st igniter circuit (it was set high with line 453)
bsf	PORTB,6		;466 ;	starts to saturate the 2nd ignition coil for the next spark generation
movwf call	delay_ms_data delay_ms		,467 ,468	delay_ms_data=avans waits for a while, duration
bcf	PORTB,7		,469 ,	is advance value makes PORTB,7 logic low, this is the end of ignition signal igniter circuit breaks the current which is flowing through
		147	,	the primary coil of the 1st

		; ignition coil and ; spark occurs
btfss	portd,0	;470 The lines between : 470 and 480
goto	\$-1	;471 are the same operations ; for 2nd and 3rd
goto mo∨f	PORTD,0 \$-1 avans,0] PORTB	;472 ignition coils ;473 ;474 ;475
bsf bsf movwf call bcf	delay_ms_data delay_ms	;476 ;477 ;478 ;479 ;480
btfss	portd,0	;481 The lines between ; 481 and 491
goto	\$-1	; 481 and 491 ;482 are the same operations ; for 3rd and 4th
goto movf bankse bsf	avans,0 1 PORTB PORTB,5 PORTB,4 delay_ms_data delay_ms	; 107 370 and 407 ;483 ignition coils ;484 ;485 ;486 ;487 ;488 ;489 ;490 ;491
btfss	portd,0	;492 The lines between ; 492 and 502
goto	\$-1	; 493 are the same operations ; for 4th and 5th
goto mo∨f bankse	PORTD,0 \$-1 avans,0 PORTB PORTB,4 PORTB,3 delay_ms_data delay_ms PORTB,4	;494 ignition coils ;495 ;496 ;497 ;498 ;499 ;500 ;501 ;502
btfss	PORTD,0	;503 The lines between
goto	\$-1	; 503 and 513 ;504 are the same operations ; for 5th and 6th
btfsc goto movf	PORTD,0 \$-1	;505 ignition coils ;506 ;507

	btfss	portd,0	;514	The lines between
	goto	\$-1	; ;515	514 and 524 are the same operations
	goto movf banksel bsf bsf movwf	PORTB PORTB,2 PORTB,1 delay_ms_data delay_ms	; 516 ;517 ;518 ;519 ;520 ;521 ;522 ;523 ;524	for 6th and 7th ignition coils
	btfss	portd,0	;525	The lines between
	goto	\$-1	; ;526	525 and 535 are the same operations
	goto movf banksel bsf bsf movwf	avans,0 PORTB PORTB,1 PORTB,0	;527 ;528 ;529 ;530 ;531 ;532 ;533 ;533 ;534 ;535	for 7th and 8th ignition coils
	btfss	portd,0	;536	The lines between 536 and 546
	goto	\$-1	,537	are the same operations for 8th and 1st
	btfsc goto	PORTD,0 \$-1	;538 ;539	ignition coils
	movf bankse]	avans,0	;540 ;541	
	bsf bsf		;542;543	
	movwf call	delay_ms_data delay_ms РОКТВ,0	;544 ;545 ;546	
	return		;547	
:premode	3 iani	tion mode is a transient	mode	between
;mode_2 ;In igni ;will be ;The aim ;prepara	and mod tion mod advance of this tion fo		of the	
;the onl ;lines 6	y diffe	erence between mode_2 and	premo	ode_3 is
	-			

premode_	_3

goto	PORTD,0 \$-1 PORTD,0	;548 ;549 ;550
goto movf	\$-1 avans,0	 , ,551 ,552

banksel bsf	PORTB PORTB,7	• [•] •]	55 55	3	
movwf call bcf	delay_ms_data delay_ms PORTB,7	.,.,	55 55 55	5 6 7	
btfss goto btfsc goto movf banksel	PORTD,0 \$-1 PORTD,0 \$-1 avans,0 PORTB		55 56 56 56	8 9 0 1 2 3	
bsf bsf movwf call bcf	PORTB,6 PORTB,5 delay_ms_data delay_ms PORTB,6	. , . , . , . , . ,	56 56 56	5 6 7	
btfss goto btfsc goto movf banksel bsf movwf call bcf	PORTD,0 \$-1 PORTD,0 \$-1 avans,0 PORTB PORTB,5 PORTB,5 PORTB,4 delay_ms_data delay_ms PORTB,5	• 7 • 7 • 7 • 7 • 7 • 7 • 7 • 7 • 7 • 7	57 57 57	2 '3 '4	
btfss goto btfsc goto movf banksel bsf movwf call bcf	PORTD,0 \$-1 PORTD,0 \$-1 avans,0 PORTB PORTB,4 PORTB,3 delay_ms_data delay_ms PORTB,4	. , . , . , . , . , . , . , . , . , . ,		12345678	
btfss goto btfsc goto movf banksel bsf movwf call bcf	PORTD,0 \$-1 PORTD,0 \$-1 avans,0 PORTB,3 PORTB,2 delay_ms_data delay_ms PORTB,3			12 13 14 15 16 17	

btfss goto btfsc goto movf bankse bsf movwf call bcf	PORTD,0 \$-1 PORTD,0 \$-1 avans,0 I PORTB PORTB,2 PORTB,1 delay_ms_data delay_ms PORTB,2	;602 ;603 ;604 ;605 ;606 ;607 ;608 ;609 ;610 ;611 ;612
btfss goto btfsc goto movf bankse bsf movwf call bcf bsf	PORTD,0 \$-1 PORTD,0 \$-1 avans,0 PORTB,1 PORTB,1 PORTB,0 delay_ms_data delay_ms PORTB,1 PORTB,7	;613 ;614 ;615 ;616 ;617 ;618 ;619 ;620 ;621 ;622 ;623 ;624
btfss goto btfsc goto movf bankse bsf	PORTD,0 \$-1 PORTD,0 \$-1 avans,0 PORTB PORTB,0	;625 ;626 ;627 ;628 ;629 ;630 ;631
movwf call bcf bsf return	delay_ms_data delay_ms РОКТВ,0 РОКТВ,6	;632 ;633 ;634 ;635 ;636

; this is the ignition mode for max engine speed ; in this ignition mode, the ignition coils will be started to ; saturated at the ignition point of cylinder which ;is 90 degree before

btfss	portd,0			cylinder position
	¢ 1		;	signal?
goto btfcc	»-⊥ PORTD,0		;639	if not go to line 638 if yes, wait for
DUISC	PORID,0		,040	the falling edge
goto	\$-1		, 641	wait fot the
9020	* -		; • · -	falling edge
mo∨f	avans,0			W=avans
bankse	1 portb			go to bank0
bsf	PORTB,7		;644	makes high PORTB,7,
			;	to guarantee the
			;	starting of being
			,	saturated of
mount	dalay ma data		;	ignition coil 1
movwf call	delay_ms_data delay_ms		;645	delay_ms_data=avans
bcf	PORTB,7			The 1st ignition coil
bel				was started to
		4 - 4	,	

bsf	PORTB,5	; be saturated with ine 624 this is the ignition point of first ignition coil 648 3rd ignition coil ; is started ; to be saturated
btfss	portd,0	;649 The lines between :
goto	\$-1	; for 2nd and 4th
goto movf bankse bsf movwf call	l PORTB PORTB,6 delay_ms_data	;651 ignition coils ;652 ;653 ;654 ;655 ;656 ;657 ;658 ;659
btfss	portd,0	;670 The lines between : 670 and 680
goto	\$-1	; 670 and 680 ;671 are the same operations ; for 3rd and 5th
goto movf bankse bsf	l PORTB PORTB,5 delay_ms_data delay_ms	;672 ignition coils ;673 ;674 ;675 ;676 ;677 ;678 ;679 ;680
btfss	portd,0	;681 The lines between
goto	\$-1	; 681 and 691 ;682 are the same operations ; for 4th and 6th
btfsc goto movf bankse bsf movwf call bcf bsf	PORTD,0 \$-1 avans,0 PORTB,4 delay_ms_data delay_ms PORTB,4 PORTB,2	;683 ignition coils ;684 ;685 ;686 ;687 ;688 ;689 ;690 ;691
btfss	portd,0	;692 The lines between ; 692 and 702
goto	\$-1	; for 5th and 7th
btfsc goto movf bankse bsf movwf call bcf bsf	PORTD,0 \$-1 avans,0 PORTB,3 delay_ms_data delay_ms PORTB,3 PORTB,1	;694 ignition coils ;695 ;696 ;697 ;698 ;699 ;700 ;701 ;701

		PORTD,0 \$-1		,	The lines between 703 and 713 are the same operations
ב ס מ ל מ מ מ מ מ מ מ מ מ מ מ מ מ מ מ מ מ	otfsc goto novf oanksel osf novwf call	PORTD,0 \$-1 avans,0		;	for 6th and 8th ignition coils
b	otfss	portd,0		;714	The lines between 714 and 724
ç	goto	\$-1		,715	are the same operations for 7th and 1st
ַם ה ל ה ה ל ה ל ה ה ל ה ל ה ל ה ל ה ל ה	goto novf banksel osf novwf call ocf	avans.0		716 717 718 719 720 721 722 722 723 724	ignition coils
b	otfss	portd,0		;725	The lines between 725 and 736
Ç	goto	\$-1		,726	are the same operations for 8th and 2st
ַרַ ה ב ה ב ה ב ב ב ב ב ב ב ב ב ב ב ב ב ב	goto novf Danksel Dsf novwf	PORTD,0 \$-1 avans,0 PORTB PORTB,0 delay_ms_data delay_ms PORTB,0 PORTB,6		;728 ;729 ;730 ;731 ;732 ;733 ;734 ;735	quit from the loop
;this sub ;	oroutin	e initializes	the ADC, I	2C and	d PORT configurations
initializ	ze				
c	all	I2C_init		;737 ;	calls the subroutine "I2C_init" to initialize the I2C communication
		6111111111		.720	w_b'11111111

	b'11111111' STATUS,RPO	,739	w=b'11111111' go to bank1 to reach to the TRIS register
mo∨wf	TRISC	;740	TRISC=b'11111111' (all pins of PORTC
movwf	TRISA	; ;741	(all pins of PORTC are input) TRISA=b'111111111'

bankse movlw movwf movf bsf	TRISB PORTB d'1' deneme deneme,0 STATUS,RP0 TRISD		<pre>(all pins of PORTA are input) 742 clear TRISB, it means all pins of PORTB are output 743 go to bank0 744 745 746 W=1 747 go to bank1 to 748 TRISD=1, it means PORTD,0 is input and the others</pre>
	PORTB PORTB		; are output ;749 go to bank0 ;750 initial value of
clrf	PORTD		; PORTB is zero ;751 initial value of
clrf clrf clrf clrf clrf clrf clrf	sicaklik⊥ sicaklikH		; PORTD is zero ;752 tempH=0 ;753 sayacH=0 ;754 mode_sayac=0 ;755 sicaklikL=0 ;756 sicaklikH=0 ;757 I2C_Data=0 ;758 initial value ; of low byte ; of eeprom address
clrf	I2C_AdrH		; is zero ;759 initial value of ; high byte ; of eeprom address ; is zero
			; ADCONO is a register ; which configures ADC ; the bits ADCONO,6 ; and ADCONO,7 are ; used to select ADC ; clock frequency ; and the bit ADCONO,0 ; is used to ; activate ADC module ; ; for clock=Fosc/8 ; ADCONO,6=1 ADCONO,7=0 ; to activate the module ; ADCONO,0 shall be 1 ; the sum of ADCONO,0 ; ADCONO,6 ; equals to d'65'=0x41
movlw movwf	0x41 ADCON0		;760 w=0x41 ;761 ADCON0=0x41 ; it means clock ; frequency is Fosc/8 ; and ADC ; module is activated
movlw bsf movwf	0x80 STATUS, RPO ADCON1		;762 W=0x80 ;763 go to bank 1 ;764 ADCON1=0x80 ; the 7th bit of ; ADCON1 register ; shall be set ; to "1" to arrange ; ADRESH ; (high byte of ADC)
		154	

bsf	TXSTA, SYNC	and ADRESL (low byte of ADC) to get a 10-bit ADC result in form of 000000xx(ADRESH) xxxxxxx(ADRESL) x=0 or 1 so ADCON1=d'128'=0x80 765 the SYNC bit of register TXSTA should be set to 1 to select synchronous serial communication
	RCSTA RCSTA, SPEN	;766 go to bank0 ;767 opens the serial
	TXSTA TXSTA, CSRC	; port ;768 go to bank1 ;769 selects the
	PIE1, RCIE	; slave mode ;770 activates the
	el RCSTA RCSTA, RX9	; data receive ; interrupt ;771 go to bank0 ;772 data format is 8-bit ;773 quit from the ; subroutine
;this subrouti ; ;	ne initializes th	e TimerO
ilk_islemler		;OPTION_REG register ;is uset to ;configure TimerO module ;0xD2 is selected ;to have timerO ;ratio 1/8 and ;clock source is internal ;command cycle
movlw	0xD2	;774 W=0xD2
bankse	1 OPTION_REG	;775 go to bank1
movwf	OPTION_REG	;776 OPTION_REG=0xD2
bcf movlw	STATUS, RPO D'6'	;777 go to bank0 ;778 initial value ; of TMR0=6 ; to have 2 ms ; timer period
movwf	TMR0	;779 8us(256-TMR0)=2000 us
;bsf ;bsf	INTCON, D'5' INTCON, D'7'	;780 enables Timer0 ; interrupt ;781 activates all enabled 155

; interrupts

;782

return

```
ADC_Oku
```

	bcf	STATUS,C	:783	STATUS,C is affected by
		5171105,0	;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;;	command rlf so it should be disabled before the operation
	rlf	ADC_Oku_kanalno, F	;784	register ADCONO is used
			;	to configure ADC module
	rlf	ADC_Oku_kanalno, F	;785 ;	bit 3, bit 4 and bit 5 of ADCONO is used to
	rlf	ADC_Oku_kanalno, W	786	select ADC channel xx000xxx channel 1 xx001xxx channel 2 xx010xxx channel 3
			, , , , , , , , , , ,	xx111xxx channel 7 so the value ADC_Oku_kanalno should be shifted to the left for 3 times
	iorlw	b'01000001'	;787	to open ADC module ADCON0,0 and for the clock frequency 0x41 should be added (lines 760 and 761)
	Banksel	ADCON0	,788	iorlw b'01000001'adds 0x41 to ADC_0ku_kanalno
ADC_j1	movwf bsf	ADCONO ADCONO, 2	;789 ;790	starts the conversion
-	btfsc	ADCON0, 2	,791	if ADCON0,2 is zero it means it is the end of conversion
	goto	ADC_j1	;792	if it is not completed,
	movf	ADC_Oku_sonucbyte, I	= 793	waits for the conversion
	btfss	STATUS, Z		if ADC_Oku_sonucbyte is
			;	zero, it means read the
		156	;;;	low byte of conversion go to line 796

	goto	ADC_j2	;795 ;	if it is not zero go to ADC_j2 and read high byte
	bsf movf return	STATUS, ADRESL,	;797	go to bank1 w=ADRESL quit from the loop
ADC_j2				
	bcf movf return	STATUS, ADRESH,	;800	go to bank0 W=ADRESH quit from the loop

;this routine is used to have a delay during the program ;the delay duration is value of delay_ms_data

, delay_ms

delay_j0

movlw movwf	D'1' delay_ms_data+1	;802 ;803
nop		;804
nop		;805

delay_j1

nop decfsz goto	delay_ms_data+1, F delay_j1	;806 ;807 ;808
nop decfsz	delay_ms_data, F	;809 ;810
goto nop return	delay_j0	;811 ;812 ;813

;this routine is used to read serial rpm data ;from the secondary circuit

snkSlaveRead

banksel bsf		SPEN	;814 ;815 ;	opens the serial port again we should open the port
			;	again for every reading
banksel bcf		CSRC	;	selects slave mode(after receiving data port configures itself to master mode)
banksel bsf		CREN	;818 ;819 ;	starts to waiting for receiving data
btfss	PIR1, F	RCIF	;820	bit RCIF of PIR1 is set
			;	when the data

			, , ,	received so
	goto	\$-1		wait for the end of data transfer
	movf	RCREG, W	,822	if data transfer is completed, W=RCREG RCREG is a register which stores the received data
	bcf	PIR1, RCIF	,823 ,	clear the flag of received data for the next data transfer
	btfsc	RCSTA, CREN	,824	if there is an error during the data transfer bit CREN of RCSTA is reset, so check whether there is an error or not if there is an erro set kontrol_register,0 (line 826)
	return		;825	
	bsf return	kontrol_register,0	;826 ;827	
I2C_ini	t			
	banksel clrf bsf	SSPSTAT SSPSTAT SSPSTAT, SMP	;828 ;829 ;830 ;	SSPSTAT, SMP is used to select standard cycle frequency
	movlw	в'00001001'	,831 ,	W=9 clock=Fosc/ (4x(SSPADD+1)) Fosc=4MHz so for 100kHz clock SSPADD=9
	movwf		,832	SSPADD=9
	movlw	SSPCON2 B'10011000'	;833 ;834 ;	SDA and SCL are configured as input
	movwf movlw	TRISC B'00101000'	;835 ;836	
	bcf movwf	STATUS, RPO SSPCON	;837 ;838	master I2C mode is selected
	clrf return	PORTC	, ;839 ;840	
; this	subrouti	ne sends start bit to th	ne ext	ernal eeprom

I2CStart

banksel bcf	 SSPIF		;841 ;842 PIR1,SSPIF is set a	t

				3 3 3 3 3	the end of the I2C communication so it should be cleared before the communication
	bsf bsf	STATUS, RPO SSPCON2, SEN		;843 ;844 ;	bit SEN of SSPCON2 is used to start the I2C communication line 844 starts the communication
12CStar [.]	t_j1				
	btfsc	SSPCON2, SEN		;845	waits for the
	goto	I2CStart_j1		,846	<pre>starting operation if it is not started yet go to "I2CStart_j1"</pre>
	banksel	PIR1		; ;847	go to l2CStart_j1
12CStar	t_j2				
	btfss	PIR1, SSPIF		;848	checks whether the data
	goto	I2CStart_j2		; ; ;849	transfer is completed or not waits for the
	-	-		;	data transfer
	bcf	PIR1, SSPIF		;850 ;	if data is transferred clear the bit
	return				
I2CReSt	art				
		SSPCON2 SSPCON2, RSEN		;851 ;852 ;853 ;854 ;855 ;856 ;857 ;	SSPCON2, RSEN is used to restart the I2C mode
I2CReSt	art_j1				
	btfsc	SSPCON2, RSEN		;858	SSPCON2, RSEN is reset at the end of restart
	goto	I2CReStart_j1		,859	operation this lines are used to wait
	return			; ;860	for the end of restart
12CSend	banksel bcf	PIR1 PIR1, SSPIF		;861 ;862	should be reset before the data transfer
	mo∨f mo∨wf	I2CSend_Data, W SSPBUF			W=I2CSend_Data SSPBUF=I2CSend_Data SSPBUF is buffer register, it stores the received
			159		

	return			; ;865	or sent data quit from the routine
12CRead		SSPCON2 SSPCON2, RCEN		;866 ;867 ;	this line activates the receiving mode
I2CRead_	_j1				
	btfsc	SSPCON2, RCEN		;868 ;	wait for the end of activation of receiving mode
	goto banksel	I2CRead_j1 PIR1		,869 ,870	
I2CRead_	_j2				
	btfss goto	PIR1, SSPIF I2CRead_j2		; ,871	is data received? if no, wait for the data transfer
	bcf	PIR1, SSPIF		;872	after data transfer, reset the data transfer flag
	mo∨f	SSPBUF, W		;873	read the received data
	return			;874	quit from the routine
12CStop		SSPCON2 SSPCON2, PEN		;875 ;876	when the bit PEN of SSPCON2 is set it sends stop bit
I2CStop_	_j1			,	
	btfsc	SSPCON2, PEN		;877	waits for the end of sending stop bit
	goto banksel	I2CStop_j1 PIR1		, 878 879	
I2CStop_	_j2				
	btfss	PIR1, SSPIF			checks whether the stop-bit transfer is completed
	goto	I2CStop_j2		;881 ;	if not go to the "I2CStop_j2"
	bcf	PIR1, SSPIF		;882	if yes, clear the "PIR1, SSPIF"
	return			;883	11(1, 33)11
12CACk	banksel bcf	SSPCON2 SSPCON2, ACKDT		;884 ;885 ;	bit ACKDT of SSPCON2 is set when the data is acknowledged (master receiving mode) so before the data transfer it should be reset
	bsf	SSPCON2, ACKSTAT	160	,886 ,	bit ACKSTAT of SSPCON2 is reset when the data is acknowledged by

			, , ,	the slave so it should be set before the communication		
I2CAck_	j1		;887			
	btfsc	SSPCON2, ACKSTAT	,888 ,889 ,	waits until the received data is acknowledged by the slave device		
	goto banksel	I2CACK_j1 PIR1	;890 ;891			
I2CACK_	_j2					
	btfss	PIR1, SSPIF	;892 ;	checks whether data_sending is		
	goto bcf return	I2CACK_j2 PIR1, SSPIF	; ,893 ;894 ;895	completed or not		
I2CNak		SSPCON2 SSPCON2, ACKDT	;896 ;897	set bit ACKDT of SSPCON2		
12CNak_	_j1		;			
	btfsc	SSPCON2, ACKSTAT	;898 ;	waits for the acknowledgement of data by the slave device		
	goto bsf	I2CNak_j1 SSPCON2, ACKEN	;899 ;900	sets the receiving mode of master device and sends ACKDT bit to		
	bcf bcf	STATUS, RPO PIR1, SSPIF	,901 ,902	slave device reset the bit SSPIF of PIR1		
I2CNak_	_j2					
		SSPCON2 SSPCON2, ACKEN	;903 ;904	after sending of ACKDT,		
	goto	I2CNak_j2	,905	ACKEN is reset so these lines checks whether ACKDT is		
	banksel	PIR1	;906	sent or not		
12CNak_	_j3					
	btfss	PIR1, SSPIF		is the data		
	goto	I2CNak_j3	,908	transferred? waits for the data transfer		
	bcf	PIR1, SSPIF	;909	reset PIR1, SSPIF for		
	return		, 910	the next operations quit from the routine		
; this subroutine is used to read advance data						

; this subroutine is used to read advance data ; from the external eeprom

; to read data from the external eeprom ; first of all we send control byte ; control byte is the combination of hardware address ; logic states of AO, A1 and A2 pins (which are used to address ; the external device) and R/W bit ; 1010(A2)(A1)(AO)(R/W) is the for of ; control byte ; A2, A1 and AO are connected to GND in our application ; so for reading operations, the control byte is 10100001 ; for writing operations, the control byte is 10100000 ; after sending control byte, we should check ACK (acknowledged) ; then we willsend high address byte and check ACK ; after checking the ACK, we will send low address byte and ; check ACK. Now we are ready to read the data of sent address ; for reading operation we should restart the device, ;send reading control byte ; and check the ACK. After ACK is received, advance data will received ; the operations will end with No ACK and we ;will stop the communication

I2C_ReadEE

call rlf	I2CStart I2C_Device, W	;911 starts the ; communication ;912 data format of ; control byte ; is 1010 ; (A2)(A1)(A0)(R/W) ; so to have this form we
		<pre>shall shift the I2C_Device to the left. Actually we can write the control byte directly because there is only one external eeprom. This code form is used for future works</pre>
andlw iorlw	0xFE 0xA0	;913 ;914 R/w is O
movwf	I2CSend_Data	;915 I2CSend_Data=control
call	12CSend	; byte ;916 calls the subroutine ; which sends ; data to the
call	I2CAck	; external eeprom ;917 after sending control ; byte we ; should check ACK
movf	I2C_AdrH, W	; Should check Ack ;918 W=high byte of eeprom ; address ; which the advance ; data will be read
movwf	I2CSend_Data	;919 I2CSend_Data=high
call	I2CSend	; byte of address ;920 calls the subroutine ; which sends ; data to the external
call	I2CACk	; eeprom ;921 after sending ; high byte of ; address we should
	1.00	

	movf movwf call call call	I2C_AdrL, W I2CSend_Data I2CSend I2CAck I2CReStart		923 924 925	check ACK W=low byte of eeprom address I2CSend_Data=low byte of address calls the subroutine which sends data to the external eeprom after sending low byte of address we should check ACK for reading operation we
				,	should restart the device
	rlf	I2C_Device,	W	;927 ;	formation of control byte for reading operation
	andlw iorlw	0xFE 0xA1		;928 ;929	R/W is 1
	mo∨wf	I2CSend_Data		;930 ;	I2CSend_Data=control byte
	call call	I2CSend I2CAck			sends the control byte checks whether the control byte acknowledged or not
	call	I2CRead		, 933 ,	reads the advance data from the eeprom
	movwf call	I2C_Data I2CNak			I2C_Data=advance value checks the No ACK
	call	I2CStop			stops the I2C communication
	return			;937	
• * * * * * * * * '	END ********	* * * * * * * * * * * * * * * * * * *	* * * * * * * * *	;938	* * * * * * * * * * * * * * * * * * * *

APPENDIX B: SOURCE CODE OF THE SECOND CONTROL CIRCUIT

• * * * * * * * * * * * * * * * * * * *	******	***********
; Source Code of	Secondary	/ Control Circuit
;***************	*****	***************************************
list p=16f877A		
#include <p16f8< td=""><td>377A.inc></td><td></td></p16f8<>	377A.inc>	
config H'3F31	L'	;PWRT on, diðerleri kapalý,
		;Osilatör XT ve 4 Mhz.
;		
; Deðiþken tanýmlama		
;		
delay_ms_data	equ 0x20	;delay routine variable
rpmL	equ 0x25	;low byte of rpm value
rpmH	equ 0x23	;high byte of rpm value
bolum	equ 0x24	;8-bit form of rpmL+rpmH
ADC_Oku_kanalno	equ 0x70	;ADC channel number
ADC_Oku_sonucbyte varibale	equ 0x71	;ADRESL or ADRESH selection
sayac2	equ 0x72	;counter for gear wheel pulses
sayac3	equ 0x73	;counter for cylinder number

ORG 0x000

goto main

main tekrar	call	initial		;1
	btfss F	PORTD,0		;2 is the main ; contror circuit
	goto \$-	-1		; ready for data transfer? ;3 wait for the ready ; signal of
	movlw movwf	0x00 ADC_0ku_kanalno		; the main control circuit ;4 W=0x00 ;5 ADC_0ku_kanalno=0x00 ; analog ; channel 0 is selected
	mo∨lw mo∨wf	0x00 ADC_Oku_sonucbyt	e	;6 W=0x00 ;7 ADC_Oku_sonucbyte=0x00 ; read the low byte of ADC
	call	ADC_Oku		;8 calls the subroutine ; "ADC_Oku"
	Banksel movwf nop nop nop movlw	PORTB rpmL 0x00		;9 go to bank0 ;10 rpmL=low byte of ADC ;11 no operation ;12 no operation ;13 no operation ;14
	movwf	ADC_Oku_kanalno		;15 analog channel 0 selected
	movlw movwf	0x01 ADC_0ku_sonucbyt	e	;16 ;17 reads the high
	call	ADC_Oku		; byte of ADC ;18 calls the subroutine ; "ADC_Oku" to read high ; byte of rpm
	Banksel movwf			;19 go to bank0 ;20 rpmH= high byte of ADC
	movlw movlw movwf	rpmH d'O' bolum		;20 rpm= frigh byte of Abc ;21 w=0 ;22 bolum=0, initial value ; of bolum is zero
dongu2				
	movlw d	1'4'		;23 the operations which are ; done with lines
	subwf r	pmL ,1		; between 23-38 ;24 are the mathematical ; operations (16-bit
	btfss S	STATUS,C		; division) ;25 which is done to scale ; 10-bit ; ADC result to 8-bit
	movlw d subwf r btfss s goto \$ goto \$ decf b goto \$ goto d movf b	longu2 polum,1 STATUS,0 I'1' SPMH,1 STATUS,C S+2 S+3 polum,1 S+2		ADC result to 8-bit 26 27 28 29 30 31 32 33 34 35 36 37 38 39 W=bolum, bolum is the 8-bit form of rpm value 40 calls the subroutine which sends
			165	,

	Bankse	PORTB	; ; ;41	the rpm data to the main control circuit go to bankO
	btfss	PORTD,1	;42	checks the first
	goto	\$-1	; ;43	cylinder position waits for the cylinder
	btfsc	PORTD,1	; ;44	position signal checks the falling
			,	edge of the first cylinder
	goto	\$-1	; ;45	position signal waits for the
	bsf	PORTB,7	; ;46	falling edge if the falling edge
			,	is detected, send first cylinder position signal to the main control circuit
	call bcf	delay_20us PORTB,7	, ;47 ;48	20 us delay makes low the PORTB,7
; remair : positi	loop is ning 7 ion sid	s detects the position o cylinders and sends cyl nals to the circuit	f	- ,
dongu3				
	bcf nop	STATUS,Z	;49	clears the STATUS,Z no operation
	nop	PORTD,2	;51	no operation is there a pulse?
	goto		;53	if no go to line 52 if yes wait for the
	goto		; 55	falling edge
	bankse incf	el PORTB sayac2,F	;56	sayac2=sayac2+1;
	mo∨f mo∨wf	sayac2,0 PORTB	;58	W=sayac2 PORTB=sayac2, this
			;	is used to see the pulses with the
	movlw	d'10'	; ; 60	leds of PORTB W=10
	subwf	sayac2,W STATUS,Z	;61 ;62	W=sayac2-10 if sayac2=10 go to
			,	line 64 the gear wheel
			;	which is used to measure the crank
			;	shaft angle (detecting the
			;	cylinder positions) has 80 teeth, so 10
			,	teeth (pulses) means 45 degree, new
			,	cylinder position
	goto	dongu3	;63 ;	sayac2 is not equal to 10, go to
	7 6		,	the starting point of the dongu3
	clrf bsf	PORTB PORTB,7	;64 ;65	clears PORTB sends the cylinder
			,	position signal to the main
		166		

	bcf clrf bankse incf movlw subwf	delay_20us PORTB,7 sayac2 el PORTB sayac3,F d'7' sayac3,W STATUS,Z	;67 ;68 ;69 ;70 ;71 ;71	control circuit 20 us delay makes PORTB,7 low sayac2=0, for the next cylinder position detection go to bank0 sayac3=sayac3+1 sayac3 is the number of detected cylinders (except first cylinder) W=7 W=sayac3-7 if sayac3=7 (if all cylinde are
	goto	dongu3	; ;74	detected which means one full revolution) go to line 75 if not go to the starting
		el portв portв,7	,75 ,76	point of the dongu3 go to bank0 send cylinder position signal to the main control circuit
	call bcf clrf goto	delay_20us PORTB,7 sayac3 tekrar	;78	20 us delay makes PORTB,7 low sayac3=0
initial	clrf clrf movlw movwf movlw	TRISD	;82 ;83 ;84 ;85 ;86 ;87 ;88	go to bank1 all pins of PORTC are output all pins of PORTB are output W=255 TRISA=255 it means all pins of PORTA are input W=7 TRISD=7 it means Oth, 1st and 2nd pins of PORTD are input, the other pins are output go to bank0 initial value of PORTB is zero
	clrf clrf clrf clrf		,91 ,92	porte is zero initial value of rpmL is zero initial value of rpmH is zero initial value of sayac2 is zero initial value of sayac3 is zero

; ADCONO is a register

movlw 0x41	<pre>which configures ADC the bits ADCON0,6 and ADCON0,7 are used to select ADC clock frequency and the bit ADCON0,0 is used to activate ADC module for clock=Fosc/8 ADCON0,6=1 ADCON0,7=0 to activate the module ADCON0,0 shall be 1 the sum of ADCON0,0 ADCON0,6 equals to d'65'=0x41 ;95 W=0x41</pre>
movwf ADCON0	96 ADCON0=0x41 ADCON0=0x41 it means clock frequency is Fosc/8 and ADC
	<pre>the 7th bit of ADCON1 register shall be set to "1" to arrange ADRESH(high byte of ADC) and ADRESL (low byte of ADC) to get a 10-bit ADC result in form of 000000xx(ADRESH) xxxxxxx(ADRESL) x=0 or 1 so ADCON1=d'128'=0x80</pre>
movlw 0x80 bsf STATUS, RP0 movwf ADCON1	;97 W=0x80 ;98 go to bank1 ;99 ADCON1=0x80
movlw 0x01	;100 W=0x01 ;101 ;
banksel TXREG clrf TXREG	;102 go to bank0 ;103 TXREG=0
banksel SPBRG	;104 go to bank1
	<pre>the register SPBRG is used to select serial communication baudrate the formula to calculate the baudrate Fosc/(4x(SPBRG+1)) we have selected the baudrate as 500000, so 500000= 4000000/(4x(SPBRG+1)) SPBRG=1</pre>
movwf SPBRG banksel TXSTA	;105 SPBRG=1 ;106 168

	bsf	TXSTA, SYNC		;107	the SYNC bit of register
				;	TXSTA should be set to 1
				,	to select synchronous serial communication
	bsf	TXSTA, CSRC		;108	selects the master mode
	bsf	PIE1, TXIE		;109 ;	data sending interrupt is activated
	bcf	txsta, tx9		;110 ;	8-bit data format is selected
	bsf	TXSTA, TXEN		;111	data sending is activated
	banksel bcf bsf	RCSTA RCSTA, SREN RCSTA, SPEN		;112 ;113 ;114	no data receiving opens the serial port
	return			;115	
delay_20	Dus nop nop nop nop nop nop nop nop nop nop			;116 ;117 ;118 ;119 ;120 ;121 ;122 ;123 ;124 ;125 ;126 ;127 ;128 ;129 ;130 ;131 ;132 ;133 ;134 ;135 ;136	
;delay s	subrouti	ne			
delay_ms delay_j(
	movlw movwf	D'1' delay_ms_data+1		;137 ;138	
dolov i	nop nop			;139 ;140	
delay_j1	nop nop nop decfsz goto nop decfsz goto nop return	delay_ms_data+1, delay_j1 delay_ms_data, F delay_j0	F 169	;141 ;142 ;143 ;144 ;145 ;146 ;147 ;148 ;149 ;150 ;151	

; this subroutine is used to send data with ; synchronous serial communication

snkMasterWrite

banksel	TXREG	;152	go to bank0
mo∨wf banksel		, , , , ,	with line 39, value of "bolum" was loaded to W TXREG=bolum (the data which will be sent is loaded to TXREG) go to bank 0
		, , ,	the bit TXIF of PIR1 is set when data transfer is completed
btfss	PIR1, TXIF		checks whether the transfer is completed or not
goto	\$-1	;156	if not, wait for the data transfer
bcf	PIR1, TXIF	;157	if data is transferred, reset the PIR1, TXIF for the next communication
return		,	communication

return

; this routine is used to ; read analog value and convert it into digital ; with "ADC_Oku_kanalno" any channel can be selected ; with "ADC_Oku_sonucbyte" high or low byte of ADC is selected

ADC_Oku

bcf ST4	ATUS,C	;158	STATUS,C is affected by command rlf so it should be disabled before the operation
rlf	ADC_Oku_kanalno, F	;159 ;	register ADCONO is used to configure ADC module
rlf	ADC_Oku_kanalno, F	160	bit 3, bit 4 and bit 5 of ADCONO is used to select
rlf	ADC_Oku_kanalno, W	,161	ADC channel xx000xxx channel 1 xx001xxx channel 2 xx010xxx channel 3 xx111xxx channel 7 so the value ADC_Oku_kanalno should be shifted to the left for 3 times to get right form
	4 -		

	iorlw	b'010000	001'	;162	to open ADC module ADCON0,0 and for the clock frequency 0x41 should be added (lines 95 and 96)
		ADCONO ADCONO ADCONO,	2	;163 ;164 ;165	ADCON0=0x41 starts the conversion
ADC_j1	btfsc	ADCON0,	2	;166 ;	if ADCON0,2 is zero it means it is the end of conversion
	goto	ADC_j1		,167	if it is not completed, waits for the conversion
	movf btfss	ADC_Oku_ STATUS,	_sonucbyte, F Z	,168 ,169	if ADC_Oku_sonucbyte is zero, it means read the low byte of conversion go to line 171
	goto	ADC_j2		;170	if it is not zero go to ADC_j2 and read high byte
	bsf movf	STATUS, ADRESL,		;171 ;172	go to bank1 W=ADRESL low byte of ADC is loaded to W
ADC_j2	return			;173	
,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,,	bcf movf	STATUS, ADRESH,		;174 ;175	go to bank0 W=ADRESH high byte of ADC is loaded to W
	return			;176	
• * * * * * * * * 1	END *******	******	*****	;177	****

APPENDIX C: SOURCE CODE OF THE IGNITER CIRCUIT

_BODEN_OFF & _LVP_OFF & _DATA_CP_OFF & _CP_OFF

ORG	h'00'	
movlw	b'00100000'	;1
BANKSEL	TRISB	;2
movwf	TRISB	;3
MOVLW	H'FF'	;4
MOVWF	TRISA	;5
BANKSEL	PORTB	;6
MOVLW	h'07'	;7
MOVWF	CMCON	;8
RB5_TEST		

BTFSS	PORTB,5	;9
GOTO	RB5_TEST	;10
BSF	portb,0	;11

RB5_TEST_low

BTFSC	PORTB,5	;12
GOTO	RB5_TEST_low	;13
BCF	portb,0	;14
GOTO	RB5_TEST	;15

END

;16

APPENDIX D: TECHNICAL DRAWINGS

