

**AN APPROACH ON DILUTION AND ORE RECOVERY/ LOSS  
CALCULATIONS IN MINERAL RESERVE ESTIMATIONS  
AT THE CAYELI MINE, TURKEY**

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Approval of the Graduate School of Natural and Applied Sciences

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## ABSTRACT

### AN APPROACH ON DILUTION AND ORE RECOVERY/ LOSS CALCULATIONS IN MINERAL RESERVE ESTIMATIONS AT THE CAYELI MINE, TURKEY

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Dilution and ore recovery/loss have an important role in calculation of mineral reserves. Each percent increase in dilution and decrease in recovery negatively affects economic value of the reserve. These parameters are mainly controlled by the quality of the mine design and stoping practice.

This study provides an approach developed for dilution and recovery/ore loss calculations. The contribution of mine design software (MineSight) and the recent survey technique called Cavity Monitoring System (CMS) were presented in this study. The purpose was to compare the new approach with the old system where the calculations had been done according to some assumptions and to optimize mineral reserve estimation process.

Results indicate that the new approach used in reserve estimation process gives ~1.6% closer tonnages to the actual numbers and the grades are both ~1.6% closer to the actual values numbers when compared with the old system.

*Keywords:* Dilution, Recovery, Mineral Reserve, Mine Design

## ÖZ

### ÇAYELİ MADENİ, TÜRKİYE'DEKİ CEVHER REZERVİ TAHMİNLERİNDE PASA KARIŞIMI VE CEVHER KAZANIMI/KAYBI HESAPLAMALARI ÜZERİNE BİR YAKLAŞIM

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Pasa karışımı ve cevher kazanımı / kaybı, mineral rezervleri hesaplamalarında önemli bir rol oynar. Her bir yüzdellik pasa karışımındaki artış ve cevher kazanımındaki azalış, rezervin ekonomik değerini olumsuz yönde etkiler. Bu parametreler, temel olarak maden tasarımına ve cevher üretim uygulamasına bağlı olarak değişir.

Bu çalışmada, pasa karışımı ve cevher kazanımı / kaybı hesaplamaları için geliştirilen bir yaklaşım verilmiştir. Paket programda (MineSight) yapılan maden tasarımı sistemlerinin ve yeni geliştirilmiş Boşluk Geometrisi Ölçüm Tekniğinin (CMS) katkıları bu çalışmada anlatılmıştır. Amaç, yeni yaklaşımı eski sistemle (varsayımlarla yapılan hesaplama) mukayese etmek ve mineral rezervi tahminlerini en uygun şekilde hesaplamaktır.

Sonuçlar, rezerv hesaplamalarında kullanılan yeni yaklaşımın, eski sistemle karşılaştırıldığında, gerçekleşen rakamlara tonaj bazında ~1.6% ve tenör bazında da yine ~1.6% (bakır ve çinko için) daha yakın değerler verdiğini göstermektedir.

*Anahtar Kelimeler:* Pasa Karışımı, Cevher Kazanımı, Reserv, Maden Dizayni

## **To My Parents**

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## LIST OF SYMBOLS

CBI	:	Cayeli Bakir Isletmeleri A.S., a Turkish company owned by Inmet Mining Corporation (100%)
CIM	:	Canadian Institute of Mining, Metallurgy and Petroleum
NI 43-101	:	The standards of Canadian National Instrument
CMS	:	Cavity Monitoring System for scanning solutions of dangerous and inaccessible cavities
CO	:	Clastic ore type, massive sulphides containing >10% sphalerite fragments which commonly show internal intergrowths of chalcopyrite
YO	:	Yellow ore type, copper-rich, and zinc poor sulphides
BO	:	Black ore type, zinc-rich massive sulphides with >4.5% Zn and Cu/Z ratio <1
NSR	:	Net Smelter Return cut-off, \$46 per tonne for the mineable reserve in Cayeli deposit
FWR	:	Foot Wall Ramp drift developed in Rhyolite zone at foot wall side for connecting sub-levels cutting the ore
MTA	:	Turkish Mineral Research and Exploration Institute

## **CHAPTER 1**

### **INTRODUCTION**

#### **1.1 General Remarks**

Cayeli Bakir Isletmeleri (CBI) is a Copper and Zinc mine which operates in Northeastern Turkey in the province of Rize. The Cayeli Deposit is located in 8 km south of the Black Sea coast. It is owned and operated by CBI, a Canadian company consisting of Inmet Mining Corporation (100%) of Toronto.

CBI prepares annual reserve report by the end of the previous year at the first quarter of the current year. The reports are prepared with factors for mining dilution and recovery. In addition, the sampling methods, assaying procedures, compositing methods, data handling, cutoff grade and Net Smelter Return (NSR) applications and grade calculations were reviewed.

Technical report on Mineral Resource and Mineral Reserve Estimates at CBI has been prepared as per CIM (Canadian Institute of Mining, Metallurgy and Petroleum) recommendations and as per Inmet standards. The CIM Definition Standards on Mineral Resources and Reserves establish definitions and guidelines for the reporting of exploration information, mineral resources and mineral reserves in Canada. The Mineral Resource and Mineral Reserve definitions were incorporated, by reference, in National Instrument 43-101 – Standards of Disclosure for Mineral projects (NI 43-101) (Appendix A) (Postle, Haystead, Clow, Hora, Vallee, and Jensen, 2000), which became effective February 1, 2001.

The deposit at CBI is characterized as a volcanogenic massive sulphide that exhibits similarities to the Kuroko deposits of Japan (Ohmoto and Skinner, 1983). It is currently in operation, producing 0.8M tonnes of ore from underground mining activities. The flotation concentrator plant on site produces copper and zinc concentrates which are sold to numerous customers throughout the world. The mining method is transverse/longitudinal sublevel retreat with paste and waste filling. Drift and fill method with 5 m horizontal slicing is also used for remnant areas. CBI, a wholly owned subsidiary of Inmet, has the surface rights to operate on the immediate mine property.

#### **1.2 Mineral Resource and Mineral Reserve Estimates**

The Mineral Resource and Mineral Reserve estimates by December 31, 2005 for the Cayeli Mine, according to NI43-101 standards, are summarized in the Table 1.1 and Table 1.2 (Anonymous, 2005a).

**Table 1.1: Mineral Resource in 2005 at a cut-off grade of \$35 NSR/tonne of ore**

Category	Mtonnes	Cu %	Zn %	Ag g/t	Au g/t	Pb %	\$ NSR/t
Measured	1.91	3.08	3.09	22	0.50	0.18	57
Indicated	2.65	3.05	2.55	20	0.44	0.15	54
<b>Meas. + Ind.</b>	<b>4.56</b>	<b>3.06</b>	<b>2.78</b>	<b>21</b>	<b>0.46</b>	<b>0.16</b>	<b>55</b>

Inferred	Mtonnes	Cu %	Zn %	Ag g/t	Au g/t	Pb %	\$ NSR/t
Cayeli	0.62	3.38	2.85	18	0.26	0.12	58
Russian Adit *	0.45	3.29	11.08	N/A	N/A	N/A	N/A
<b>Total Inferred</b>	<b>1.07</b>	<b>3.34</b>	<b>6.29</b>	<b>N/A</b>	<b>N/A</b>	<b>N/A</b>	<b>N/A</b>

(\*) Russian Adit inferred resources, Au and Ag have never been assayed.

**Table 1.2: Mineral Reserve in 2005 at a cut-off grade of \$46 NSR/tonne of ore**

Category	Mtonnes	Cu %	Zn %	Ag g/t	Au g/t	Pb %	\$ NSR/t
Proven	4.70	3.77	5.85	44	0.59	0.30	73
Probable	6.90	3.57	5.88	52	0.53	0.36	69
<b>Total</b>	<b>11.60</b>	<b>3.65</b>	<b>5.87</b>	<b>49</b>	<b>0.56</b>	<b>0.34</b>	<b>70</b>

### 1.3 Terms of Reference

The list of terms used in this report is as follows:

- Spec Ore : Reference to regular sulphide type mill feed as opposed to Clastic ore feed.
- Stockwork : Zone stratigraphically below the massive sulphide portion of the deposit in which predominantly copper mineralization occurs as a series of veins.
- Main Ore Zone : Portion of the deposit above the Scissor Fault.
- Deep Ore Zone : Portion of the deposit below the Scissor Fault.
- Scissor Fault : A prominent fault with strike sub-parallel to the deposit but dipping 50° to the ESE separates the upper “Main” zone of the deposit from the lower “Deep Ore” zone.
- CuEq : Copper Equivalent cut-off which is the minimum criteria used to differentiate between economically viable and non-economically viable materials.
- Dilution : The contamination of ore by non-ore material during the mining process.

Recovery : The allowance for the physical risks that occur in a stope during extraction phase of the production cycle.

#### **1.4 Objective of the Thesis**

The objective of this study is to find out the contribution of mine design systems in 3-D software and to optimize the calculation of dilution and recovery factors used in mineral reserve calculations. Since the calculations are based on the actual stope CMS surveys under 3-D software (MineSight) support, the results gathered for dilution and recovery serve us better estimations in mineral reserve and long term planning studies. This study gives an approach for calculation of dilution/recovery factors for mineral reserve estimations.

#### **1.5 Procedure**

Dilution and recovery factors used in mineral reserve estimations were based on some assumptions in old system and there was no correct measurement of the factors. A new approach developed in the new system that all open stope (mined- out) outlines has been surveyed by Cavity Monitoring System (CMS) and dilution and recovery calculations derived from the measurements. In the new system, correct volume of the mined out stopes, ore loss and diluted waste amounts are calculated by using 3-D software (MineSight) and CMS data.

## CHAPTER 2

### PROPERTY INFORMATION

#### 2.1 Property Location

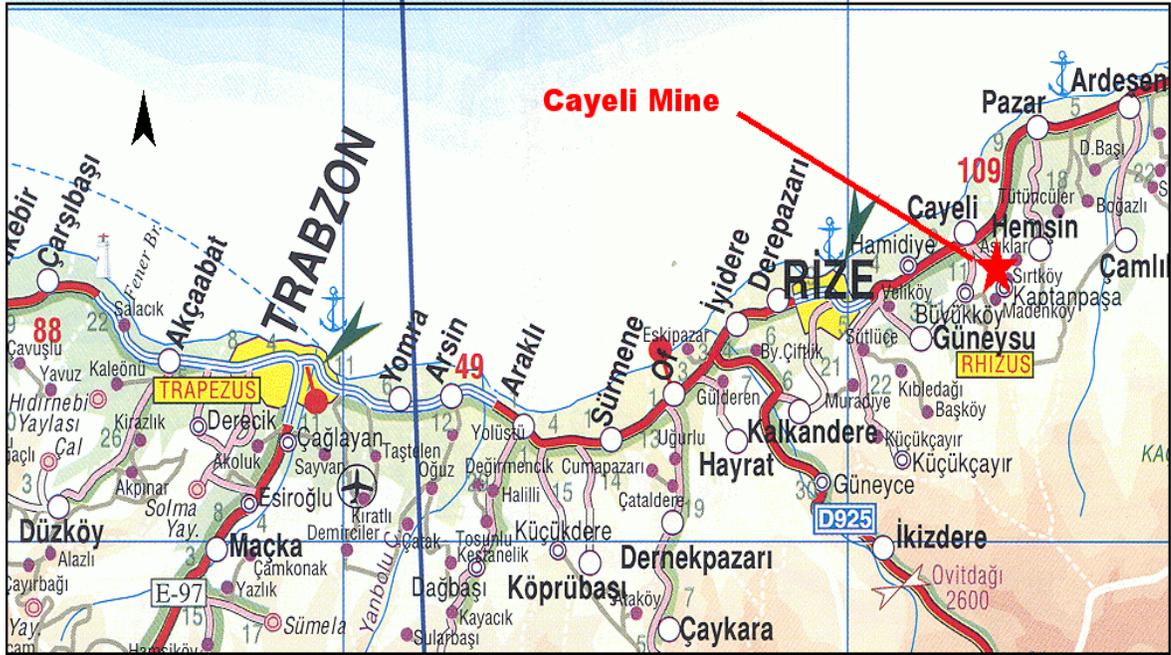
The Cayeli mine is located 8km south of the town of Cayeli, a fishing and tea-farming village with population of 56,000 located on the south coast of the Black Sea (Figure 2.1 and Figure 2.2).

Cayeli is a modern underground operation mining massive sulphide from which it produces copper and zinc concentrates. The deposit is operated through Cayeli Bakir Isletmeleri A.S., a company consisting of Inmet Mining Corporation (100%).

Small scale mining activity in the area dates back to the Roman times. Modern evaluation of the economic potential of the deposit took place through the late 1970's and 1980's. Full-scale production began in 1994, with a present extraction rate of 0.9 million tonnes of ore per year. The operation employs approximately 480 people who primarily live in the local communities of Cayeli and Rize.



Figure 2.1: Cayeli, Turkey Location Map



**Figure 2.2: Cayeli, Mine Location Map**

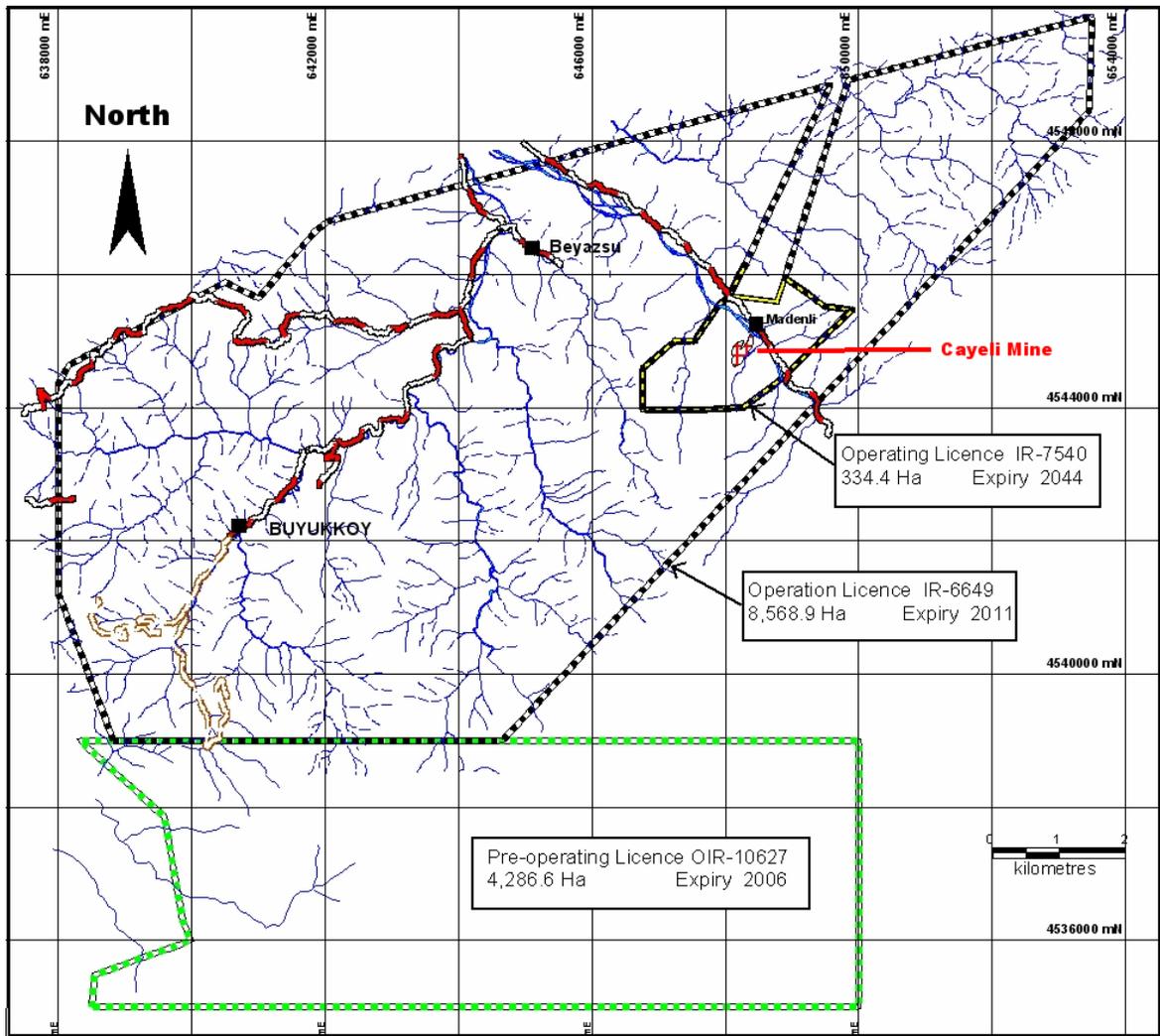
The mine and surrounding property consists of three separate leases as listed in Table 2.1 and shown in Figure 2.3. The total area of the property is approximately 13,000 hectares.

**Table 2.1: List of Properties**

License #	Registration #	Size (hectares)	Exp. Date	Status
IR 7540	4.70	3.77	5.85	44
IR 6649	6.90	3.57	5.88	52
OIR 10627	6.90	3.57	5.88	52

## 2.2 Property Accessibility

The mine is located in the foothills of the Kackar Mountains which extend along the eastern portion of the southern Black Sea coast. The Kackar Mountains are popular summer trekking and climbing destination and Mount Kackar, at 3932m, is the fifth highest peak in Turkey (Figure 2.4).



**Figure 2.3: Property Boundary Map**

Access to the mine, from Cayeli, is via paved road for a distance of 8km towards the small village of Madenli. The Karadeniz Highway provides transportation in an east-west direction along Black Sea coast from Samsun to the Georgian border located approximately 100km east of Cayeli. Rize with a population of approximately 365,000 is the port city located 20km west from Cayeli. An international airport exists in the city of Trabzon (population 975,000), located approximately 100 west of Cayeli. The access route can be classified into the four segments described in Table 2.2.



**Figure 2.4: Kackar Mountains**

**Table 2.2: Road Segment Distance**

From	To	Distance	Road Type
Trabzon	Rize	75km	Paved
Rize	Cayeli	20km	Paved
Cayeli	Madenli	8km	Paved

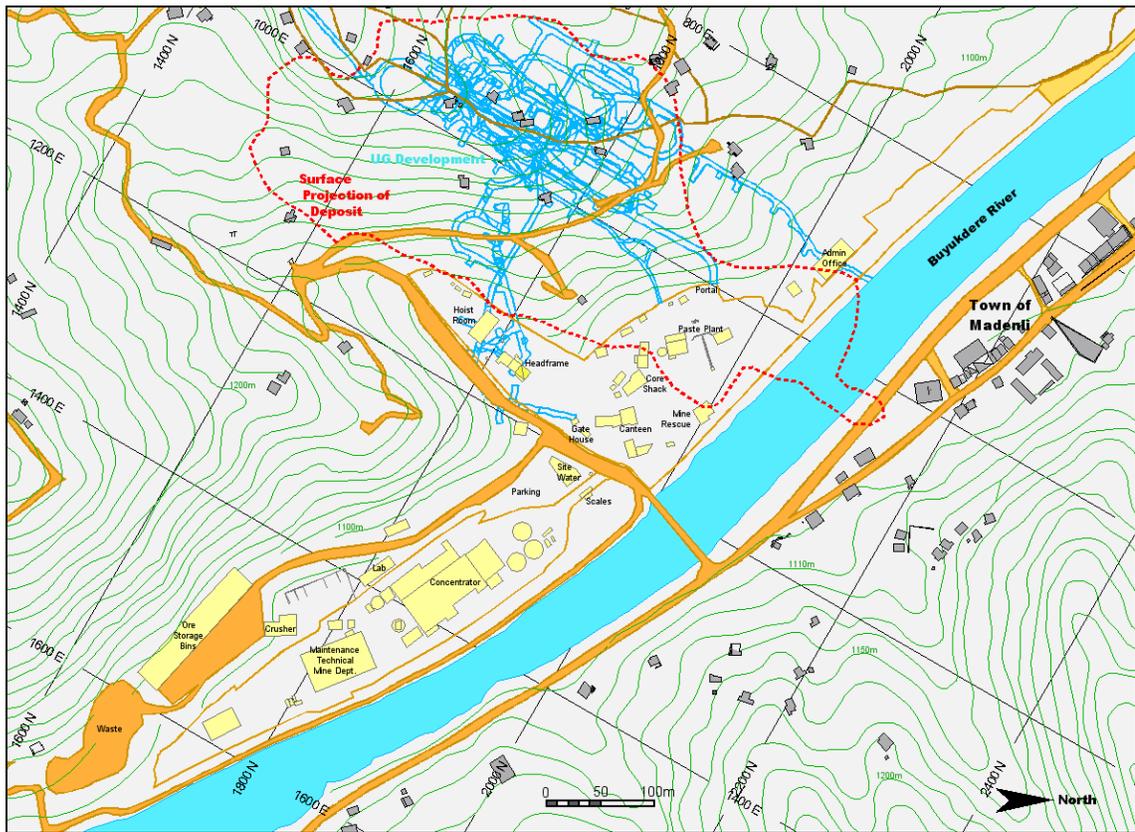
### **2.3 Infrastructure and Labor**

CBI has the surface rights to operate on the immediate mine property (IR-7540, Figure 2.5).

Electric power is provided via a single 31.5 kV, 30 MVA rated overhead power line running from the Turkish national grid system (TEK), substation at the town of Madenli. The substation at Madenli is equipped with one 25 MVA transformer, and one 10 MVA transformer as a back up reserve. Electric energy is delivered to the mine by

6.3 kV lines through the shaft and service ramp to the mine 300 or 500 kVA substations located on different levels and sublevels.

Fresh water is supplied to the mine from 7 wells on the bank of the Büyükdere River. The wells have a supply capacity of 450 m<sup>3</sup>/h. Potable water is supplied from Madenli municipality. Storage facilities for process water and potable water have a capacity of 1000 m<sup>3</sup> and 60 m<sup>3</sup>, respectively. The total water requirement of the mine and the mill is estimated at over 350 m<sup>3</sup>/h.



**Figure 2.5: Site Map**

The majority of the tailings produced are utilized as Paste Backfill in the mining sequence which is pumped underground and any excess is discharged via a 7.5km long HDPE overland pipeline to an undersea disposal site which is located 3km off shore at a depth of 275m in the Black Sea.

The mine locally employs approximately 480 people in its operations, the large majority of whom were hired locally (Table 2.3). Other skilled and professional workers have migrated from other parts of the country. Only 1.5% of the workforce is expatriates. 24 hours work achieved at mill, workshops, paste plant and underground operation as 3 shifts per day (7.5 hrs per shift). Administrative and support staff work a nine-hour day, five days a week.

**Table 2.3: Labor**

<b>Category</b>	<b>Number</b>
Executive	2
Human Resources	3
Ankara Office	10
Finance	32
Security	15
Mill	51
Mine	200
Maintenance	90
Technical	52
Safety, Health and Environment	7
Administration	18
<b>TOTAL</b>	<b>480</b>

## **2.4 History**

Mining activities along the Black Sea coast and at Cayeli date back at least a thousand years. At the turn of this century minor exploration by the Russians was reported and, between 1930 and 1955, various shafts and adits were driven and some minor production took place.

The work which led to the present mine was started in 1967 by the Turkish Mineral Research and Exploration Institute (MTA). MTA carried out a geophysical survey and drilling programme, and drove an adit into massive sulphide ore located just south of the current deposit.

In 1981, CBI was formed as a company with Etibank (now Eti Holding A.S.), Phelps Dodge and Gama Endustri AŞ as shareholders to develop the ore body. Phelps Dodge sold its 45% share to Metall Mining (now Inmet Mining) in 1988. Further underground work and metallurgical testing was done in the period 1988 to 1991. After positive results, a production decision was made and site construction started in 1992.

Basic mine infrastructure commenced in 1993 and in August 1994, the first concentrate was produced. The total capital cost of the operation was approximately \$200M.

In 2002, Inmet's share in ÇBİ increased to 55% after acquisition of Gama's 6% share. Acquisition of Cerattepe and Rize Property from Teck Cominco was done in 2003.

In 2004, Inmet purchased Eti Holding A.S.'s 45%, and owned (100%) of the total share.

In 2005, the project of deepening shaft to 540m elevation was commenced by Kopex, Polish company. This project will be completed by the end of the 1st quarter in 2007. In Table 2.4, the highlights of the activities are summarized (Yumlu, 2001).

The historical reserve and production figures are listed for comparison purposes in Table 2.5. The classification parameters for Proven + Probable reserves (as listed in this table) are considered to be consistent with National Instrument 43-101 (see Appendix A for the Definitions and Guidelines of CIM Standards on Mineral Resources and Reserves) (Postle, Haystead, Clow, Hora, Vallee, and Jensen, 2000).

Since the beginning of the operation, the production cut-off grade has varied between 3% and 5% CuEq. The current reserve statement is at a cut-off limit of 2.5% CuEq and appropriate adjustments have been made to account for reserves sterilized by mining at a higher cut-off limit.

**Table 2.4: Highlights of the Activities**

Year	Activity
1967	First geological survey and drilling program by MTA
1981	CBI was formed as joint venture between Etibank (now Eti Holding A.S.), Phelps Dodge and Gama Endustri A.S.
1983-1987	A small exploration ramp (10 m <sup>2</sup> ) was driven down to 1000 Level
1988	Phelps Dodge sold its share to Metall Mining (now Inmet)
1988-1991	U/G work and metallurgical testing was done
1992	Site construction started
1993	Basic mine infrastructure commenced
1994	First concentrate was produced in August
1995	Engineering and design for shaft started
1998	Shaft commissioned in July
1999	Paste backfill plant commissioned
2000	Achieved 4 million tonnes production since start up
2002	Inmet's share in CBI increased to 55% after acquisition of Gama's 6% share
2003	Achieved 6 million tonnes of mined production since start up and mining rate increased from 1350 tpd in 1995 to 3450 tpd. Acquisition of Cerattepe and Rize Property from Teck Cominco
2004	Inmet purchased Eti Holding A.S.'s 45%, and owned 100% of the total share
2005	Deepening of shaft down to 840m elevation commenced by Kopex. Achieved 8 million tonnes of mined production

The mining rate has increased from 1350 tonnes per day in 1995 to almost 3600 tonnes per day in 2005 through a series of capital and operating improvements. Metallurgical recoveries and concentrate quality have also improved since start-up.

**Table 2.5: Historical Reserves and Production**

	2005*	2004	2003	2002	2001	2000	1999	1998	1997	1996	1995	1994	1993
<b>Proven + Probable Reserves</b>													
Tonnes(million)	11.6	14.3	15.9	16.0	16.9	14.6	11.8	11.0	11.4	10.7	11.3	12.7	10.6
Cu %	3.7	3.4	3.6	3.6	3.8	4.1	4.2	4.8	4.3	4.4	4.5	4.4	4.7
Zn %	5.9	5.3	5.6	5.7	5.8	6.1	5.6	5.5	5.2	5.1	6.3	6.2	7.3
<b>Additional Resources</b>													
Tonnes(million)	4.6	3.7	3.2	3.3	2.9	1.3	4.3	5.9	6.5	6.5	6.5	4.1	N/A
Cu %	3.1	4.4	3.8	5.8	4.9	4.9	3.9	3.5	4.0	3.6	3.6	4.1	N/A
Zn %	2.8	4.8	5.9	8.7	6.9	8.6	8.0	8.3	8.0	7.8	7.8	8.4	N/A
<b>Production</b>													
Cut-off(EqCu%)	3.4	3.4	3.4	3.4	3.4	5.0	5.0	5.0	5.0	3.0	3.0	3.0	
Tonnes(million)	0.83	0.76	0.93	0.90	0.82	0.86	0.90	0.71	0.76	0.66	0.49	0.14**	
Cu %	3.8	3.9	4.2	4.2	4.6	4.9	5.1	4.6	4.7	3.6	3.3	4.4	
Zn %	6.7	5.8	5.1	5.1	4.5	4.5	5.3	6.6	7.0	8.5	7.2	8.1	

Notes : (\*) Reserves and resources are reported at a \$US 46 NSR/tonne cut-off for 2005 and at a 2.5% EqCu for the previous years.  
(\*\*) Includes 67,000 tonnes used to commission the mill extracted during 1993.

## CHAPTER 3

### GEOLOGICAL SETTING

#### 3.1 Regional Geology

The Eastern Black Sea volcanic province (Pontid Belt) is composed of three major geologic units: (i) a Precambrian - Palaeozoic crystalline basement complex, (ii) a Jurassic - Pliocene volcanic-sedimentary series and (iii) a granitic-granodioritic complex of Cretaceous - Oligocene age that has intruded the crystalline basement and part of the volcanic - sedimentary series (Anonymous, 1994). The Pontid volcanic belt is thought to be part of a large island arc system that developed during the late Jurassic – Eocene (Figure 3.1).

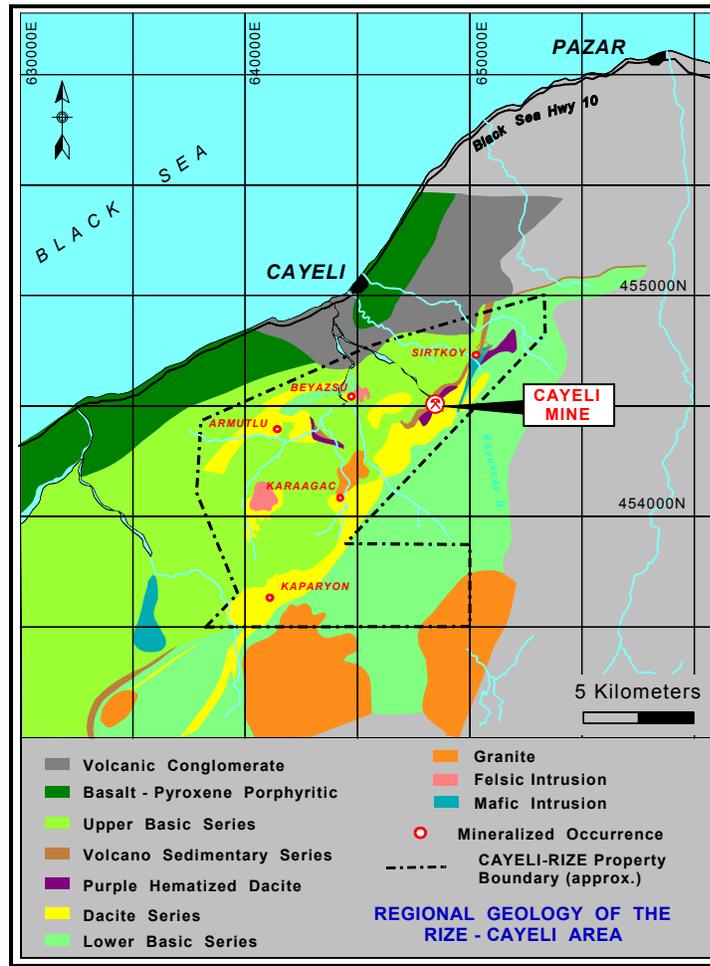


Figure 3.1: Regional Geology Map

It is generally accepted that two complete basalt-andesite-dacite-rhyodacite volcanic cycles evolved during the formation of the Pontid Volcanic Island Arc. The Cayeli massive sulphide orebody occurs on the contact between the Lower Dacitic and Upper Basic Series.

### **3.2 Deposit Geology**

The Cayeli orebody, with a strong similarity to Kuroko-type volcanogenic mineralization (Ohmoto and Skinner, 1983), occurs on the contact between Cretaceous-aged rocks of the Upper Basic Series (hangingwall pyroclastites and flows) and the Lower Dacitic Series (footwall rhyolite). The hangingwall rock sequence is a series of intercalated acid to intermediate pyroclastic and basaltic layers with some minor carbonate beds. The footwall rock sequence consists of rhyolite and felsic pyroclastic rocks. Hydrothermal alteration related to the formation of the deposit is restricted to the footwall stratigraphy in the form of clay (argillite) and chlorite. The footwall also hosts an extensive stockwork zone consisting of sulphide veins (chalcopyrite and pyrite) and varying degrees of silicification (Figure 3.2).

Mineralization of the Cayeli orebody is known over a strike length of 920m. The measured resource has a strike length of about 600m, a vertical depth of over 600m and varies in thickness from a few metres to 80m, with a mean of approximately 20m. The average dip is 65° to the NNW in the upper part of the deposit and shallows to about 50° at depth.

A prominent fault with strike sub-parallel to the deposit but dipping 50° to the ESE separates the upper “Main” zone of the deposit from the lower “Deep Ore” zone. This structure is referred to as the “Scissor” Fault due to its variable displacement, with essentially none in the southern parts of the deposit, increasing to some 80 metres of reverse displacement at the northern limits of ore. There is evidence that this is a synvolcanic structure that acted as an escarpment during the formation of the deposit and remained mildly active for a period after the development of the orebody (Figure 3.3 and Figure 3.4).

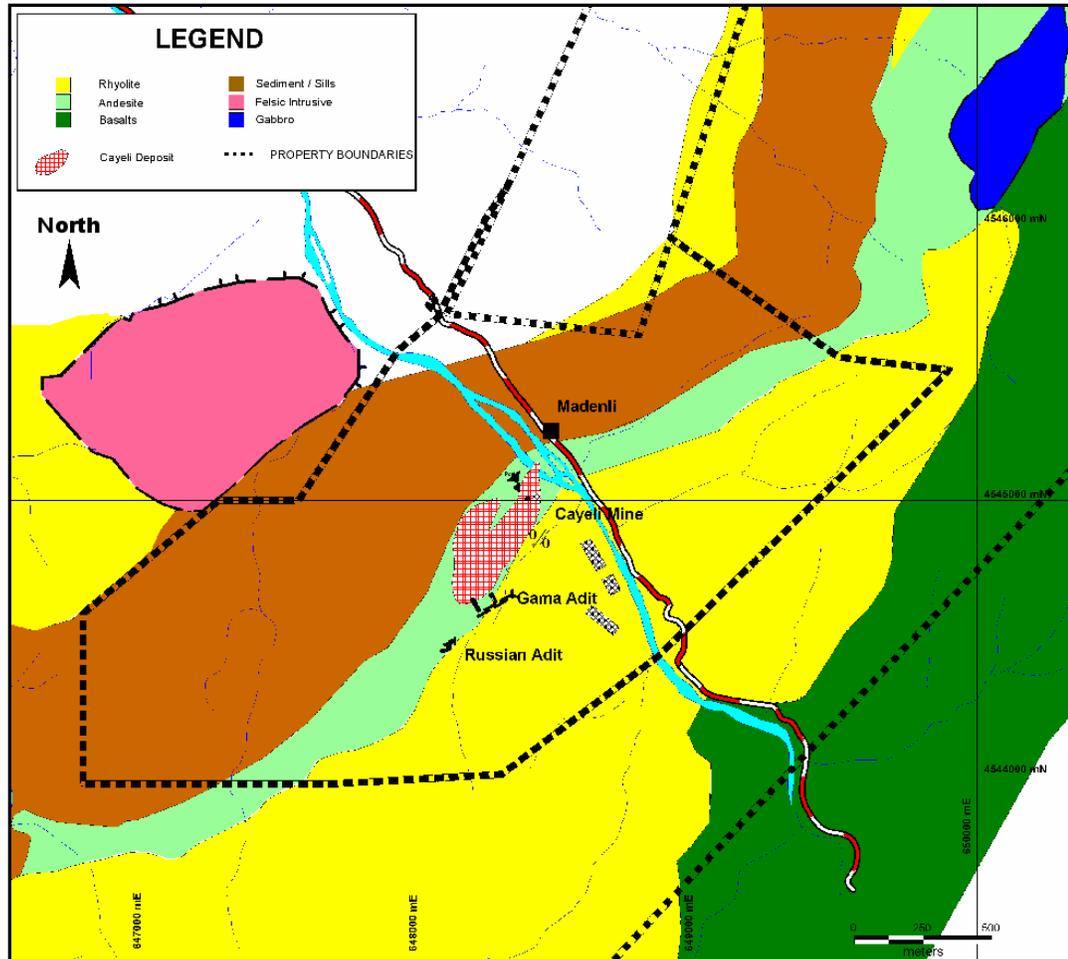


Figure 3.2: Deposit Geology Map

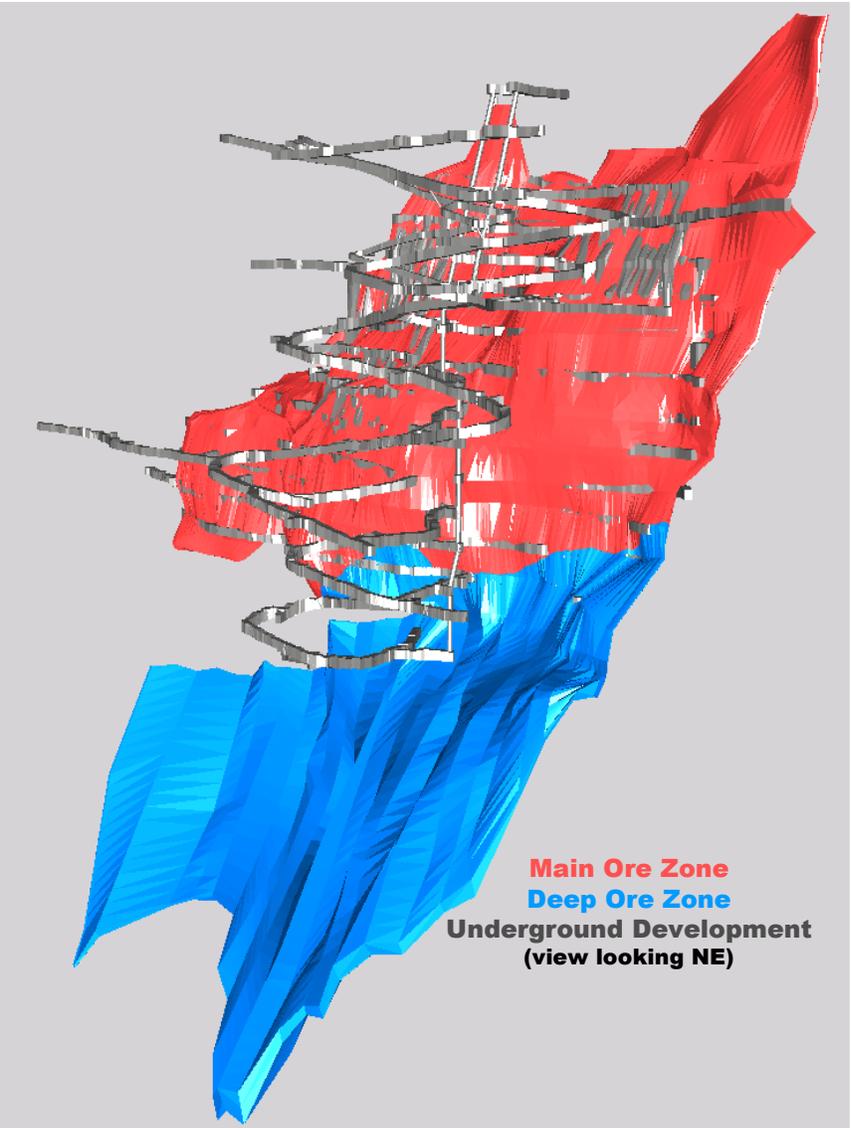


Figure 3.3: 3D Main and Deep Ore Zones

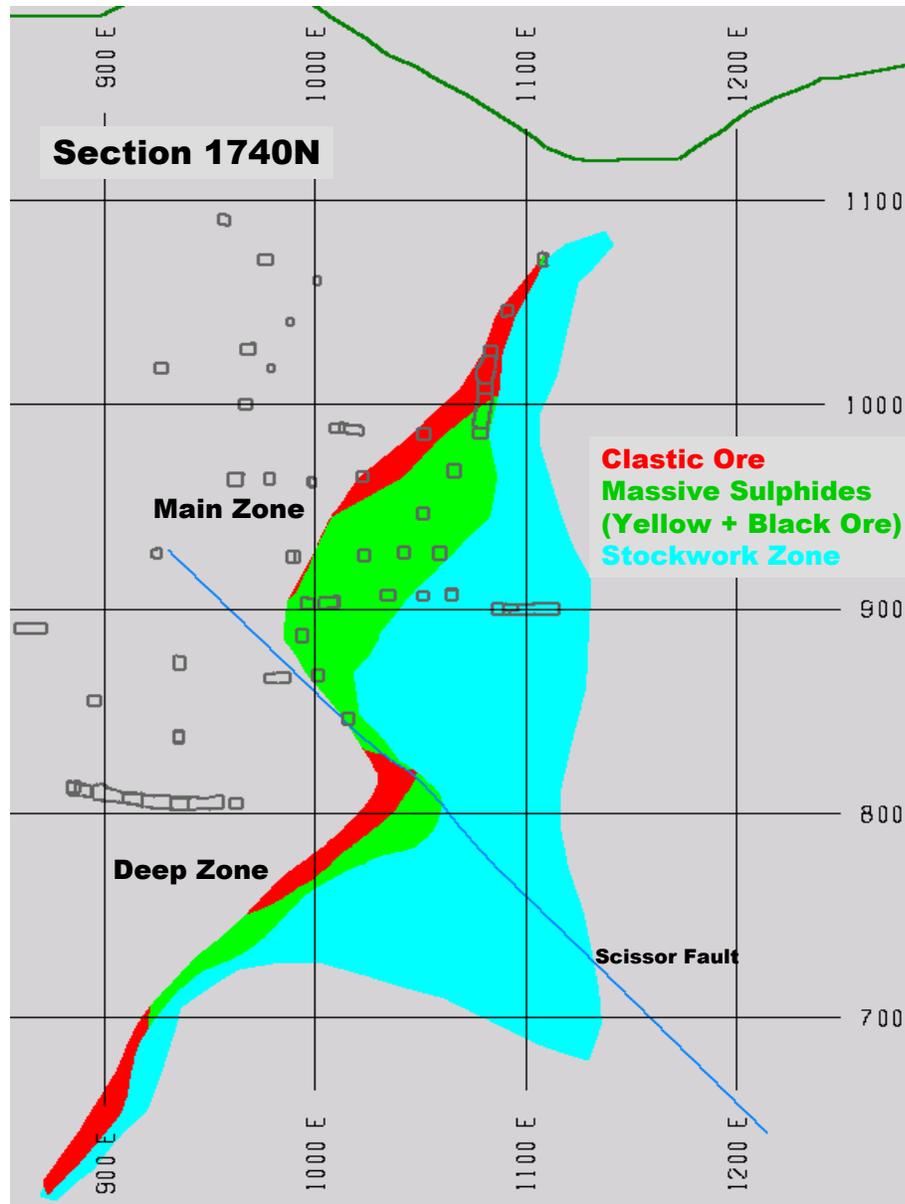


Figure 3.4: Geology Cross-Section (looking north)

### 3.3 Mineralization

The sulphide composition and grade distribution can be highly variable throughout the deposit indicating an active depositional environment with multiple sources (vent points) for hydrothermal activity. Massive sulphides, with little to no original primary textures, form the majority of the ore in the deposit. This is comprised of varying amounts of pyrite, chalcopyrite and sphalerite with minor dolomite and

barite. The stratigraphic top of the deposit (the hangingwall side) often shows fragmental textures indicating sloughing of the primary sulphides, an ore type that is referred to as “Clastic” (Figure 3.5). Below the massive sulphides there are varying widths of stringer mineralization which can often exceed the cut-off grade due to chalcopyrite veining. Referred to as “Stockwork” ore (Figure 3.5), the upper portion commonly shows pyrite + clay with veins of chalcopyrite which grades into more typical veins of chalcopyrite and pyrite in siliceous rhyolite.

Based on the requirements of the concentrator, mining activities work towards the segregation of three ore types. Clastic ore is material which, based on visual estimates, contains >10% sphalerite fragments in the massive sulphides. These fragments are generally fine grained and have intergrowths of chalcopyrite in the sphalerite which can affect the copper recoveries. The relative amount of Clastic ore is higher in the Deep ore at 40% compared to 11% in the Main ore zone, for an overall average of 19%.

The other two ore types, called Black and Yellow (Figure 3.5), are based on the contained zinc grade and are mined separately in order to allow for optimal grade blending from the stockpile bins on surface. Black ore comprises 33% of the remaining resource and is defined as material with >4.5%Zn and a Cu/Zn ratio of <1. 48% of the deposit is Yellow ore which is comprised of approximately one half massive sulphides and one half stockwork material (stockwork mineralization generally contains very little sphalerite).

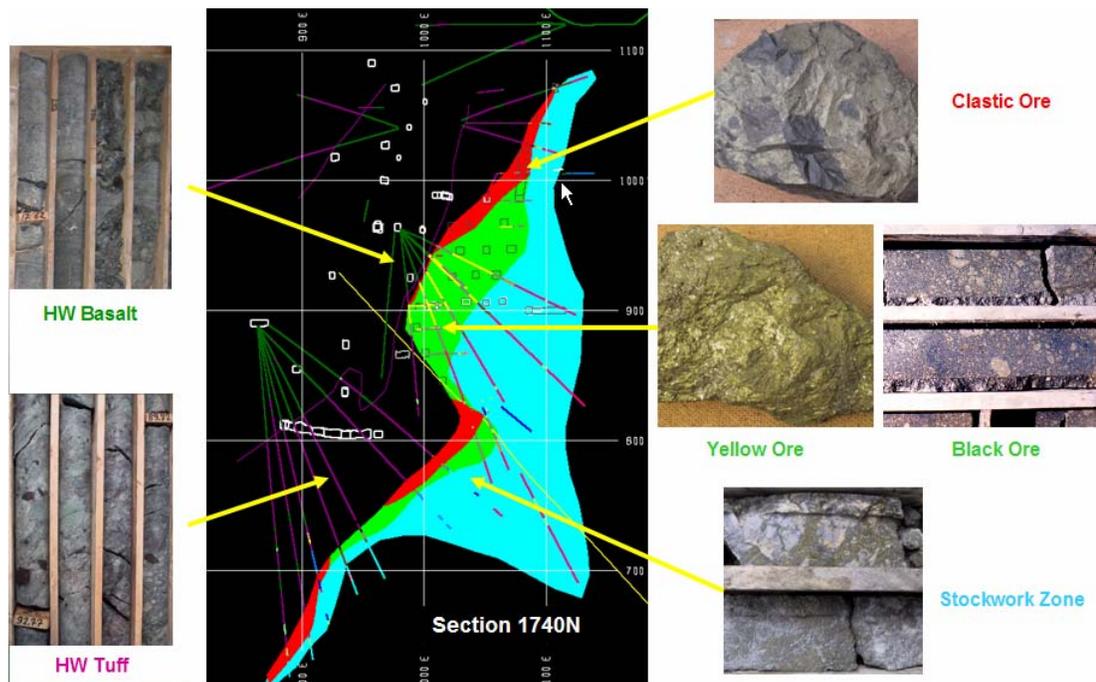


Figure 3.5: Mine Geology - Ore types

## CHAPTER 4

### MINING OPERATIONS AT CAYELI MINE

#### 4.1 Mine Development

The main levels are developed from the service ramp along the strike of the orebody at 45m to 100m vertical intervals. The sea level is called as 1000L in order to prevent possible conflicts due to +/- sign in front of level name. From top of the mine (1060 Level) down to the 800 Level, levels are located on the hangingwall side, and from 800 level down to the bottom of the mine (535 Level), they are located on the footwall side of the orebody (Figure 4.1). The main levels divide the orebody into mining blocks. There are seven main mining blocks which are as follows:

- Block 1 : 1060L-980L
- Block 2 : 960L-900L
- Block 3 : 880L-820L
- Block 4 : 800L-775L
- Block 5 : 760L-685L
- Block 6 : 670L-580L
- Block 7 : 565L-535L

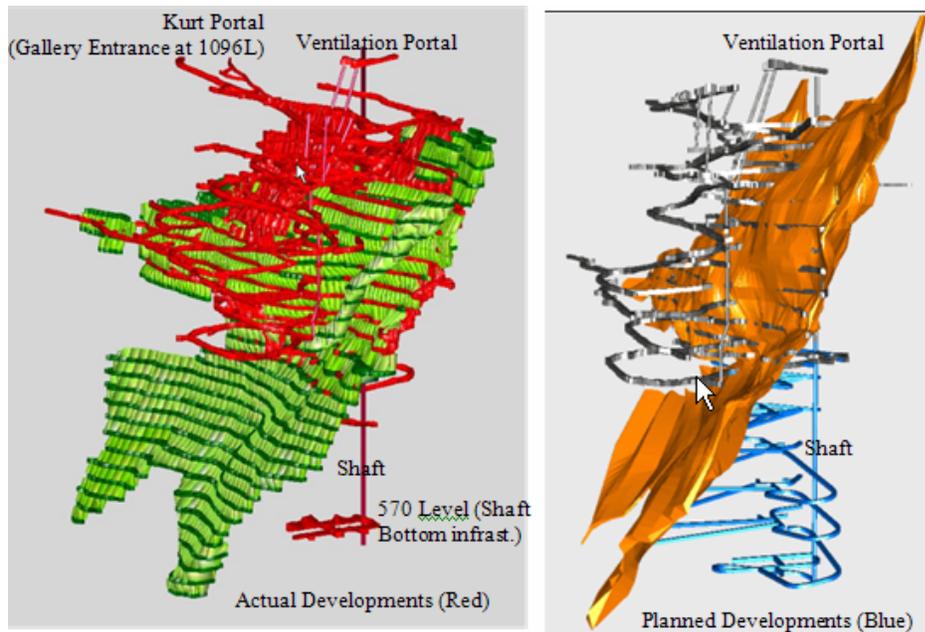


Figure 4.1: Actual and Planned Mine Development

Sublevels are developed inside the orebody along the contact with the hangingwall or in the centre of the orebody in the upper parts of the mine. In the lower parts of the mine, sublevels are developed along the gradational contact with the footwall. The sublevels are part of the stopes. Stopes are grouped as primary, secondary and tertiary. The ore within sublevel drift configurations is recovered after the primary and secondary stopes in a block are mined out and backfilled. Extraction of the ore from the sublevels drifts is called the tertiary stoping and is done in a retreat scenario.

The sublevel vertical distance is dictated by the stope height. In the upper parts of the mine (above 800 Level), it is 20m, allowing development of a 15m high by 7m wide stope bench for production drilling. In the lower part of the mine (below 800 Level), the sublevels will be developed 15m apart, allowing development of a 10m high by 10m wide bench for production drilling.

## 4.2 Mining Method

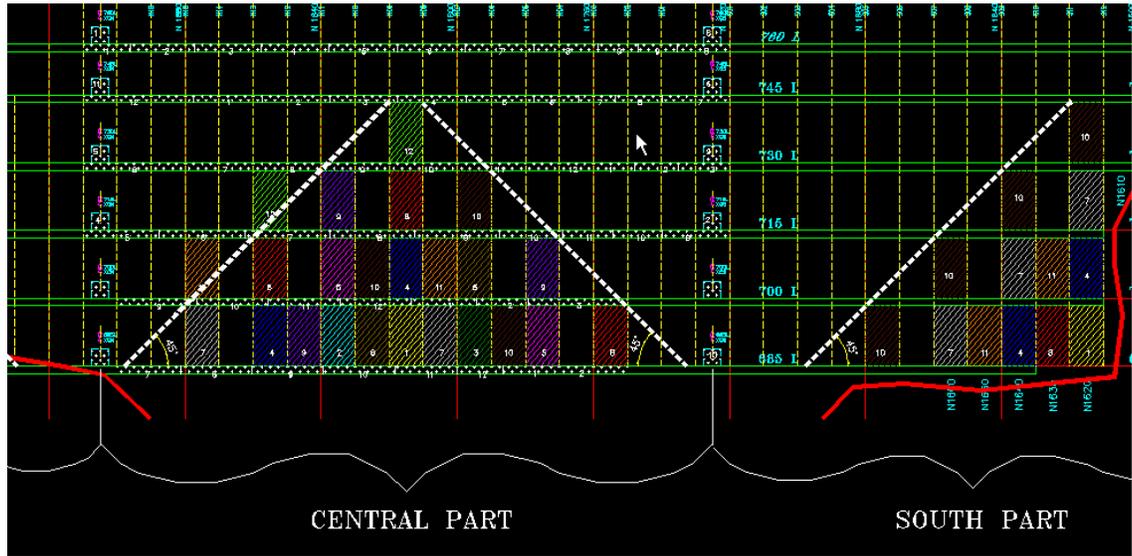
The mining method employed at CBI is sublevel retreat transverse and longitudinal long hole stoping with paste fill and loose or consolidated waste rock backfill application. The stopes are mined in primary, secondary, and tertiary sequencing. The primary and secondary stopes are mined as transverse and the tertiary as longitudinal stopes. The mining method has been designed for 100% extraction with complete pillar recovery while allowing no perceptible surface subsidence.

In the upper parts of the mine, stope sill drifts (both primary and secondary) are 7m wide (stope width) by 5m high and are driven on a 7m centre. In the lower parts of the mine, the sill drifts will be of the same cross section, but driven on a 10m centre (10m wide stopes). The length of the sill drifts depends on the thickness of the ore body. The sill drift length varies, and can be from 10m to 50m long. The average stope size in the upper part of the mine is 7,000 t to 8,000 t. In the lower part of the mine, the average stope size will be in a 5,000 t to 6,000 t range.

Sequencing of the mining method depending on the mining blocks is as follows:

- Retreat from the boundaries of the orebody to the 57m wide Central Pillar (Blocks 1&2, i.e. above 900 Level)
- Retreat from the 57m wide Central Pillar to the boundaries of the orebody (Block 3, i.e. 820-880 Levels)
- Retreat from centre to the boundaries at Central Part (between x/cuts) and retreat from the boundaries of the orebody to the Central Part at North and South Regions without any central pillar (Blocks 4 to 7, i.e. below 800 Level). Figure 4.3 shows a schematic mining sequence between 685-760 levels.
- Production from main levels up.
- Mining front at an overall angle of ~45 degrees (Figure 4.2).
- Alternating primary and secondary stopes.

- Secondary stopes are mined between primary stopes after consolidation of the primary type backfill (cemented waste and/or paste fill).
- Completion of a mining area by mining tertiary stopes in strike direction between development drifts.

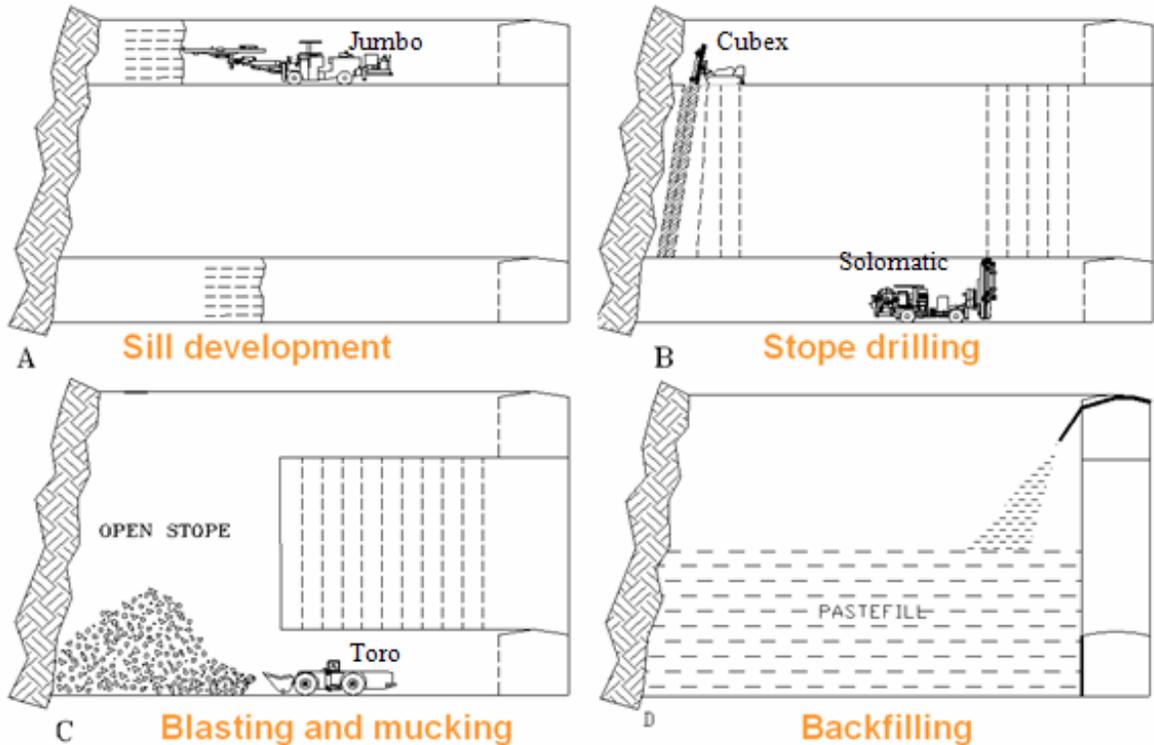


**Figure 4.2: Schematic Mining Sequence**

Stope production comprises extraction of a 15m or 10m high bench created between two sill drifts (Figure 4.3.A). Stope blast holes in the bench are drilled with Tamrock H695 Solomatic top hammer drills (Figure 4.3.B). Blast holes, of a diameter of 64mm to 89mm, are drilled on a variety of patterns depending on the ore and stope types. The blast holes can be drilled as up or down holes.

A slot raise is excavated between the sublevels at the end of the sill drifts with the use of a Cubex drill equipped with a V-30 Machine Roger Hammer (Figure 4.3.B). The Cubex drills a 203mm pilot hole from the upper to the lower level or vice versa, and then enlarges it with a 762mm diameter Machine Roger Hammer head. The rest of the slot raise is drilled with a Tamrock Solomatic drill and blasted out in steps to the full width of the stope to create a free breaking face.

The remainder of the bench is drilled and blasted in steps (row by row) retreating from the open slot (Figure 4.3.C). The main blasting agent is ANFO with NONEL initiation system. ANFO is transported from surface with Paus trucks and pneumatically injected to the blast holes. Blasting of stopes is carried out sequentially with blasting one or two rows at a time and mucking, until the stope excavation is complete (Figure 4.3.C). The mine has a central blasting system, and major stope blasts are executed at the end of day shifts.



**Figure 4.3: Mining Method and Sequence**

The ore is mucked by Toro loaders from the lower sill drift intermittently with drilling and blasting one or two fans at a time (Figure 4.3.C). All load-haul-dump machines (LHD) used for stope mucking are equipped with remote controlled features. After the stope has been mined out completely, it is filled with either paste or cemented rock/waste fill up to the floor level of the upper sill drift (Figure 4.3.D). The top of the backfilled stope becomes the mucking floor for the next lift.

Once the backfill in the primary stopes is completely cured, the pillars between the primary stopes can be mined as secondary stopes using the same stope preparation process as described above. The secondary stopes are backfilled with loose rock/waste fill. However, the first ~10m of the bottom level of each mining block, below which will be mined as blind stope, is backfilled with paste or consolidated rock/waste fill whether it is primary or secondary.

The tertiary stopes are longitudinal and are mined along the hangingwall or foot wall stope access drift. They are mined on a retreat pattern as soon as the primary and secondary stopes are mined out in a given mining block.

In the past, the overall stope sequencing in the upper parts of the mine began from the flanks (extremities) and progressed to the centre of the orebody and up the dip from the main levels. This sequencing created high stress concentration around the central parts in the upper levels of the mine. As a consequence of this high stress environment, parts of the developed blocks in the upper central zone collapsed. The ore within collapsed areas is treated as sterilized and has been removed from the reserves.

Below 880 Level, the mining sequence has been changed and ore extraction starts in the centre of the block and progresses outwards to the extremities of the orebody.

The mining blocks are not separated by traditional ore sill pillars, but by a row of primary and secondary stopes that have been mined out and filled with consolidated backfill. These primary and secondary stopes form sill pillar(s), allowing effective separation of the mining blocks. In such case, mining activities can be conducted in several blocks simultaneously without interference with each other.

The stope preparation process is based on “in-time” drifting, production drilling, blasting, and mucking philosophy. The reason for this is that, due to the relatively poor ground conditions, the excavations often deteriorate quickly. As a consequence, they require rehabilitation, which slows down extraction and increases production costs.

### **4.3 Backfilling**

Backfilling is an essential part of mining at CBI which allows relatively high extraction of the deposit and at the same time maintaining stability of the mine. Particularly, the regional stability of the weak hangingwall depends on timely backfill placement.

Several types of fill are used for backfilling: cemented rock/waste fill (CRF/CWF), cemented paste fill (PF), and uncemented waste fill (WF).

The mining sequencing requires that the primary stopes to be filled with consolidated fill (PF and/or CRF/CWF) to allow safe and maximum extraction of the secondary and tertiary stopes. The primary stopes are filled with CRF/CWF with ~5% cement content or PF with ~7-9% cement contents. The backfill cement content depends on stope requirements.

The majority of the secondary and tertiary stopes are backfilled with loose waste rock (uncemented waste rock), and occasionally these stopes require consolidated fill in order to maintain access for mining the remaining ore or creation of sills for mining underneath the remnant ores. The need for the partial use of consolidated backfill in the secondary and tertiary stopes results from the stope accesses being driven inside the ore.

Secondary stopes except for the brow portion, which will be exposed during tertiary extraction, are filled with uncemented development waste material or paste fill having 5% cement content. The brow portions that will be exposed during tertiary extraction are filled with CRF/CWF with 5% cement content or PF with 7-9% cement in order to minimize dilution.

Tertiary and longitudinal stopes are backfilled with CRF/CWF with 5% cement content and/or PF with 7% cement content.

Generally, the cement content of the CRF/CWF and PF is 5% to 7% respectively; however the stope geometry and the prevailing mining conditions dictate the final cement content in backfill.

The uppermost sill drifts on main levels require tight backfilling against the back to minimize spans and to improve regional stability. Application of paste fill, due to the excellent floatability of the paste mass, allows successful accomplishment of this task.

The use of waste rock as CWF for the most part facilitates disposal of waste from development mining, eliminating the need to truck or skip the material to surface waste stockpiles.

## **4.4 Mine Access and Infrastructure**

### **4.4.1 Ramp**

Current access to the underground operation for mobile equipment, personnel, and materials delivery is through a 5m x 5m decline that extends at -15% to the 640 level. The ramp was initially driven on the hanging wall side of the orebody and the portal is at the 1096m level. The ramp also provides access to the top and bottom of the aggregate backfill raises and serves as an exhaust way for ventilation. The upper portion of the ramp is located on the hangingwall side of the orebody down to the 800m Level. On the 800m level, the ramp location was switched to the footwall side from where it continues down to the lowest level of the mine. The service ramp is currently being deepened and planned to be connected with the new shaft bottom at 540m level by the end of 2006.

Additional access to the mine is also provided via an exploration ramp with a 9m<sup>2</sup> cross sectional area on a 17% gradient down to the 1000 level. This ramp is used as a return airway and accommodates paste fill delivery pipelines.

### **4.4.2 Shaft**

A 5.5m diameter vertical concrete lined shaft, located on the footwall side of the orebody, services the mine. The shaft was recently deepened by 295m and is now 570m deep. The shaft sinking contractor (Kopex) is currently working on the ore handling system and shaft bottom infrastructure. All the works and developing the ramp up to 620L for connection to the FWR going down by CBI is expected to be completed in 1<sup>st</sup> quarter of 2007.

The shaft collar is at the 1110m level and the bottom is at the 540m level. Current underground access to the shaft is at the 900m level. Access to the shaft on the 900m level is by an approximately 120m long cross cut. After the service ramp

connection with the lower part of the mine (end of 2006) is established, additional shaft access will be provided on the 800m, 570m and 540m levels. The shaft is equipped with two skips, a main cage, and a small cage for hoisting man.

The hoistroom is equipped with two winders. One winder is for hoisting two 5.67 tonne capacity skips and the second one for hoisting main cage. In addition to the skips and man cage, an auxiliary small cage is installed in the shaft for transporting man.

The rated hoisting capacity of the shaft is 260 tonnes of ore/waste per hour. The skips discharge ore and waste into two storage bins. A 200 tonne bin is assigned to ore and a 50 tonne bin to waste. Both bins can be used to handle ore.

From the shaft, the ore is transported by two Volvo A35 trucks to the ore stockpile shed located approximately 400m away. The shed has eight compartments each rated at a 3,500 tonne capacity.

The headframe is a sheet metal clad steel frame structure erected on a shaft concrete collar. The headframe support legs rest on steel reinforced concrete footings. One of the leg footings recently subsided by approximately 250mm. Reportedly, this was caused by neighboring hillside movement or existence of a cavity under the footing. Remedial work consisting of erecting a rock filled buffer against the hillside did not slow the subsidence process.

Another attempt using extensive grouting under subsided footing appears to have slowed down the subsidence process. The gap between the footing and the headframe leg was fitted with adjustable steel filler plate. A monitoring system was set up at the headframe for measuring and recording any further deformation.

As consequence of this event, the headframe is slightly bent at the top and hoist rope sheave wheel is off the centre line. The hoisting is apparently not affected by the headframe deformation. Allowing this situation to continue for longer time might cause premature wear of the cage shoes and guides.

## **4.5 Material Handling**

### **4.5.1 Ore and Waste Handling**

A fleet of six and eight cubic yard LHDs and 25t trucks handles ore mucking from development headings and stopes. The LHDs work in combination with Wagner MT 400 series mine trucks due to the long haulage distances from the most of the development faces and some of the stopes to the ore passes. The LHDs are equipped with ejection buckets and remote control features. Remote stope mucking is mandatory.

Until the middle of 1998 (before commissioning of the shaft), all ore was hauled via the service ramp directly to the ore storage bins on surface. The trucks now dump the ore at the two ore pass loading stations on the 960m, 940m and 920m levels. Haulage

distances on the 900m to 960m levels do not exceed 200 metres. Ore from the upper levels is hauled to the 960m level and from the lower levels to the 920m level and/or 900m level dump station.

The two ore passes each with a cross section of 10.2 m<sup>2</sup>, are located in the central pillar of the main ore zone (section N1760) and are part of the mine ore handling system. The ore passes are steel-concrete lined. The two ore pass system allows separate handling of three different ore types. The orebody consists of three types of ore – Yellow, Black, and Clastic ore. Clastic ore currently accounts for about 30% of the total ore mined and is mucked and hauled in campaigns as a separate material.

The ore passes have 400 tonne capacity each between sublevels and must be pulled constantly. Ore pass hang-ups rarely occur due to the excellent fragmentation of the generally friable ore.

On the 900 level, the ore is transferred by an ST 6C LHD from the ore passes to a feeder hopper with a grizzly, which limits the block size to 300mm x 300mm. The haulage distance from the two ore passes to the feeder hopper is 25m and 50m' respectively. Separation and handling of the different ore types is strictly observed. When the ore type changes, the feeder hopper is emptied completely before another ore type can enter the system.

Presently, one of the ore pass (Ore Pass #2) is out of order due to mining of the ore in this region. However, the new ore pass system below 790 level has been in operation by mid of August 2006.

Waste rock is hauled from the development faces by trucks either directly to stopes, as backfill material, or to surface for stockpiling and future use for backfilling.

#### **4.5.2 Shotcrete Delivery**

The mine uses a wet shotcrete, which is prepared on surface at a batch plant located close to the ramp portal. The batched shotcrete is transported in mixer trucks to the underground for application.

#### **4.5.3 Aggregate Delivery**

Two backfill raises for aggregate storage are located in the hangingwall. The raises are 3.1m in diameter and inclined at 85 degrees. The loading stations for both raises are at the 1080m level. One raise discharges on the 1040m level and the second on the 1020m level. The 1020 backfill station is not used due to water leaking problem through the raise.

Presently, the new backfill station (CWF station) between 770 and 730 levels is planned to be completed by the end of 2006.

#### **4.5.4 Materials and Fuel Delivery**

Consumable materials and supplies are transported from surface to underground work places by Paus trucks.

There are two diesel fuel stations, one of them is located near the ramp portal on surface, and second one is located in underground at 800 level next to underground workshop. All underground mobile fleet, including surface fleet, refuel at these stations. A diesel fuel line is currently installed from surface fuel tank down to 800 level fuel station. This system has been increased operating availability of the mobile equipment underground.

#### **4.5.5 Compressed Air Delivery**

Four compressors located on surface provide compressed air for the mine. Each unit is powered by a 160 kW motor and delivers 380 l/sec of compressed air at 10 bars pressure. Three pipelines, 100mm to 200mm in diameter, distribute compressed air to the different parts of the mine. One line is installed in the shaft, the second in the ventilation raise, and the third in the service ramp.

#### **4.5.6 Water Supply**

Fresh water is supplied to the mine from seven wells on the bank of the Buyuk Dere River. The wells have a supply capacity of 450 m<sup>3</sup>/h. Although potable water is supplied from Madenli municipality, water for consumption (drinking) is delivered in special plastic tubs or small bottles. Storage facilities for process water and potable water have a capacity of 1000 m<sup>3</sup> and 60 m<sup>3</sup>, respectively. The total water requirement of the mine and the mill is estimated at over 350 m<sup>3</sup>/h.

Water is supplied to the underground via three 50mm and 100mm diameter pipe lines installed in the shaft, ventilation raise and service ramp.

### **4.6 Ventilation**

Fresh air for primary ventilation to the mine is supplied through two downcast raises and the shaft at a combined maximum flow rate of 245 m<sup>3</sup>/s. The ventilation raises are equipped with a 220 kW fan each with a maximum capacity of 110 m<sup>3</sup>/s. The two ventilation raises are located on the hangingwall side, with a diameter of 3.6m each and inclination of 70 degrees. On surface, these raises are accessed by a horizontal drift.

Ventilation raise No.1, located at section N1730, is serving the mining area between 900 and 980 levels. Ventilation raise No.2, located at section N1710, ends at the 1000 level and ventilates mining areas above the 1000 level only.

The shaft is equipped with a 30 kW fan, which provides 25 m<sup>3</sup>/s fresh air through a 900mm diameter ventilation duct to the shaft bottom.

Several raises within the orebody, with diameters between 0.8m and 3.0m, serve as exhaust raises. Exhaust air is returned through the top levels of mining areas to the service and exploration ramps to surface.

Total ventilation requirement of the mine is calculated based on the total kW of underground diesel equipment in use in accordance with Ontario, Canada regulations (0.06 m<sup>3</sup>/s per kW). At CBI, Cogema fans are used due to their low noise generation. The ventilation network of the mine is regularly measured. Any adjustments and ventilation calculations are performed using VNETPC, software.

#### **4.7 Mine Drainage and Dewatering**

The Cayeli mine can be considered as a dry mine. Almost half of the underground water is generated from the used process water.

The current main dewatering pump is installed adjacent to the shaft on 900 level. The recently deepened shaft and shaft bottom development activities are handled through temporary pumping arrangements. After completion of these activities, a permanent setup will be installed at the deepest part of the mine to handle water from the lower levels.

All the mine water flows through drainage holes and ditches to the 900 level main dirty water sump and is pumped to surface through the shaft where dewatering pipeline installed. The main dewatering pump used is a 132 kW Geho pump, model ZPM 700. The pump can handle 65 m<sup>3</sup>/h of dirty water at a maximum operating pressure of 53 bars.

Furthermore, a standby pumping station on the 100 level pumps clear water to surface through a pipeline installed in the exploration ramp.

The total mine water pumped to surface on average is 25 m<sup>3</sup>/h. Process water accounts for approximately 40% to 45% of the total mine water pumped to surface.

#### **4.8 Maintenance**

There is a small underground maintenance shop for servicing equipment and handling miscellaneous repairs. There is also office, lunchroom, and small warehouse located in underground maintenance shop.

Most of the major repairs are done on surface in large maintenance shop. This shop is properly equipped to handle bigger jobs and can accommodate several pieces of

mobile equipment at the same time. Dry facilities and mine offices are located in the same building.

#### 4.9 Electric Energy

The mine's electrical main substation is connected to the national power grid by a single 31.5 kV, 30 MVA rated overhead power with the TEK substation north of the town of Madenli. The substation at Madenli is equipped with one 25 MVA transformer, and one 10 MVA back up unit.

Electric energy is delivered to the underground by 6.3 kV lines through the shaft and service ramp to the mine 300 or 500 kVA substations located on different levels and sublevels. The feed from the substations to the electrical equipment is reduced to 380 Volt.

#### 4.10 Ore Hoisting and Transport to Surface Stockpile

The underground skip loading arrangement consists of two conveyor belts (100m and 15m long) with a feed rate of 350 tonnes/hr. The conveyors transport the ore from the ore pass feed hopper and discharge it to a 50m<sup>3</sup> surge bin located at the skip loading station. The two skip loading hoppers can take 5.67 tonnes each. The skips with a volume of 1.89m<sup>3</sup> each operate at an average load of 5.35 tonnes. The rated capacity of the shaft, based on a hoisting speed of 7.7m per second, is 260 tonnes ore per hour.

At the headframe, the skipped ore is discharged into two storage bins. One of the storage bins, having a 200 tonne storage capacity, is assigned to ore and the other, with a 50 tonne storage capacity, is allocated to the waste rock. Both bins can be used for ore storage. The ability to use the waste bin for ore is important to avoid delay while the ore type changes and the 200 tonne ore bin is not empty. The waste bin then acts as an intermediate buffer. From the shaft, the ore is transported to the ore stockpiles by Volvo A35 trucks with a payload of 32 tonnes. The transport distance is approximately 400m (Figure 4.4).



Figure 4.4: Ore Transportation to Stockpiles

## 4.11 Mobile Equipment

The current mining fleet consists of enough quantities of equipment required for underground operations. The major underground mobile equipment fleet is listed in Table 4.1.

**Table 4.1: Underground Mobile Equipment List**

Type of Equipment	Make/Model	Number of Units
Jumbos	Atlas Copco 282 twin-boom	4
<b>Subtotal</b>		<b>4</b>
Production Drills	Cubex Megamatic ITH	1
	Gemsa	1
	Tamrock H629 Solomatic	2
	V-30 Machine Roger Hammers	2
<b>Subtotal</b>		<b>6</b>
Bolters	Memco MacLean	2
	Atlas Copco Two Boom&Basket Bolter	1
<b>Subtotal</b>		<b>3</b>
LHDs	Wagner ST8B	2
	Wagner ST6C	3
	Toro 1400	3
	JS 200	1
<b>Subtotal</b>		<b>9</b>
Trucks	Wagner MT 436B (33t)	8
<b>Subtotal</b>		<b>8</b>
Shotcrete Equipment	Normet Spraymec 6050 WPC	2
	Normet Unimixer (5m <sup>3</sup> )	2
	Normet Unimixer (7m <sup>3</sup> )	1
	Paus Mixer	1
<b>Subtotal</b>		<b>6</b>
Utility Vehicles	Fargo Scissors-lift Truck	3
	Paus Platform	5
	Paus ANFO Truck	2
	Personnel Carrier	1
	Paus Grouting Basket	1
<b>Subtotal</b>		<b>9</b>
<b>TOTAL</b>		<b>45</b>

## CHAPTER 5

### MINERAL RESOURCE ESTIMATES

#### 5.1 Geological Model

The geologic model is continuously being modified as new information is gained through drilling and development. Computerized model from the database using MineSight software was used for mineral resource and reserve estimations.

There are three main geologic domains in the deposit based primarily on the style of the mineralization. Each of these domains is further divided by the Scissor fault which separates the Main and Deep Ore zones. The domains are:

- Clastic Ore (which contacts with hangingwall tuff zone)
- Spec Ore (which includes all massive sulphides excluding the Clastic Ore portion)
- Stockwork Ore (which comprised of massive pyrite and veins of chalcopyrite in footwall zone due to the nature of the copper mineralization)

The geological interpretation of all material above and including the 775m level has been conducted on level plans. Plans prepared on 20m intervals above and including 800m level and on 15m intervals below 820m level. The information is gathered from underground geologic mapping from developments and diamond drilling/channel sampling interpretation.

Below 775m level, the geological interpretation and model of the majority of the Deep Ore zone was conducted on a series of vertical E-W cross sections spaced at 20m intervals, and the information is gathered from diamond drilling.

Three-dimensional wireframes were developed for all domains and tested for any gaps or overlaps. The final geological model contains the following six domains:

- Zone 1: Main Ore Zone, Clastic Ore (MOCO)
- Zone 2: Main Ore Zone, Spec Ore (MOSpec)
- Zone 3: Main Ore Zone, Stockwork Ore (MOStwk)
- Zone 4: Deep Ore Zone, Clastic Ore (DOCO)
- Zone 5: Deep Ore Zone, Spec Ore (DOSpec)
- Zone 6: Deep Ore Zone, Stockwork Ore (DOStwk)

## 5.2 Mineral Resource and Mineral Reserve Classification

Mineral Resources and Mineral Reserves presented herein are based on the classification into various categories. The category of an estimate implies confidence in the geological information available on the mineral deposit; the quality and quantity of data available on the deposit; the level of detail of the technical and economic information which has been generated about the deposit, and the interpretation of the data and information.

The in-situ Mineral Resources are sub-divided, in order of increasing geological confidence, into Inferred, Indicated and Measured categories, based on a combination of the number of samples used in the interpolation, the distance from the block and finally, the type of samples used. An Inferred Mineral Resource has a lower level of confidence than that applied to an Indicated Mineral Resource. An Indicated Mineral Resource has a higher level of confidence than an Inferred Mineral Resource but has a lower level of confidence than a Measured Mineral Resource.

Mineral reserves are sub-divided in order of increasing confidence into Probable Mineral Reserves and Proven Mineral Reserves. A Probable Mineral Reserve has a lower level of confidence than a Proven Mineral Reserve. Proven and Probable Mineral Reserves are derived from Measured and Indicated Resources respectively and have been shown that they can be mined and processed at a profit. These definitions have resulted from experience gained through past mining and result in confidence levels which are consistent with the definitions in the CIM Standards on Mineral Resources and Reserves (Appendix A) (Postle, Haystead, Clow, Hora, Vallee, and Jensen, 2000). These definitions are derived using all drill hole, channel and sludge sample data (Figure 5.1) (Parker, 2006).

The classification parameters are described as follows (Appendix A):

- **Measured Resource (Proven Reserve):** Blocks in the model in which the grade has been estimated using a minimum of three drill holes. All blocks in this category are located within a maximum distance of 10m from either an existing drift opening underground (Channel or Sludge sample) or a Stope Definition drill hole.
- **Indicated Resource (Probable Reserve):** Blocks in the model which do not meet the criteria for Measured resources but have had grades estimated using a minimum of three drill holes within the search ellipse, the closest of which is a maximum distance of 28m from the center of the block.
- **Inferred Resource:** Blocks in the model which do not meet the criteria for Measured or Indicated resources but have had grades interpolated by at least one drill hole within the search ellipse.

Based on these classification parameters, Resources are not considered to belong to the highest (measured) class until they have been either exposed with an underground drift or have been diamond drilled on 7m centers with Stope Definition holes.

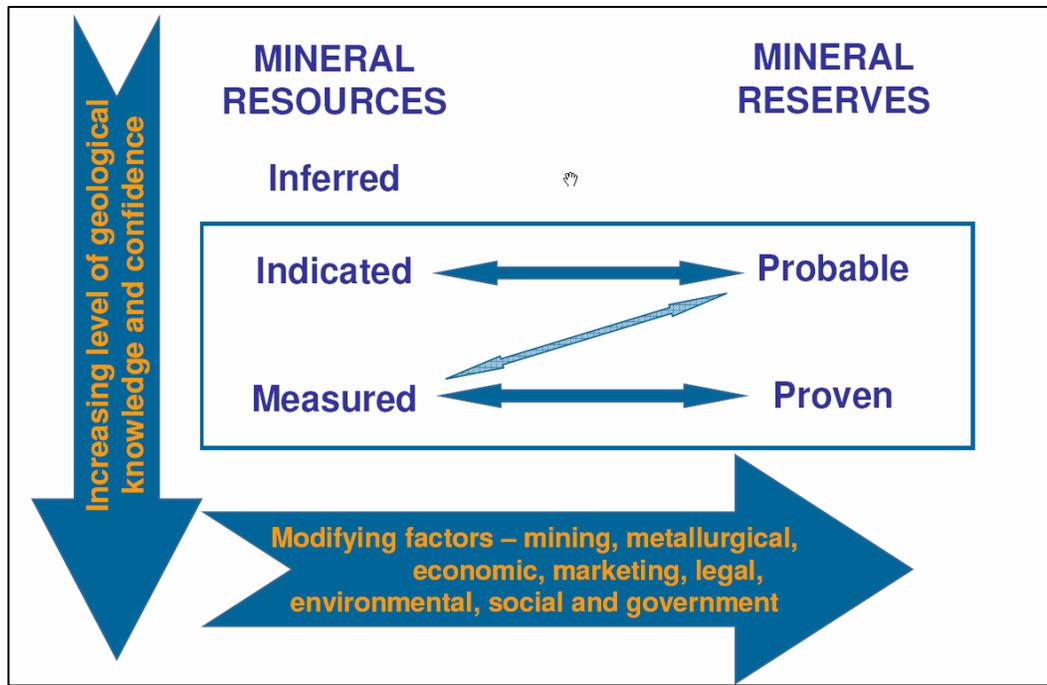


Figure 5.1: Mineral Resource vs. Mineral Reserve

### 5.3 Net Smelter Return and Equivalent Copper Calculations

Net Smelter Return (NSR) can be defined as the revenue to be expected from a given unit (tonne) of ore after it has been processed through the mill to produce saleable concentrate(s) and has left custody of the producing mine (Anonymous, 2005a). The NSR calculation incorporates the following operating parameters:

- Metal Prices
- Exchange Rates
- Refining Costs
- Smelting Costs
- Transport Costs
- Royalties

These parameters, together with the grades of the mineralized zone and the specific recoveries for the zone enable the calculation of the revenue. This revenue is the

NSR. NSR is a tool to assist in the determination of ore/waste boundaries for a mineralized zone under particular operating conditions. Material is considered to be “ore” if its NSR exceeds the unit site costs.

As a simple formula, the NSR can be summarized as:

$$NSR = \text{Revenue of recovered metals in situ} - (\text{Smelter Cost} + \text{Refinery Costs and Penalties} + \text{Royalties} + \text{Transport Costs})$$

In the past, for the purposes of the resource and reserve estimation, and since the copper is the most important metal in terms of its contribution to the NSR, CBI had been using, until December 2005, an equivalent copper grade (CuEq%) as a common parameter from which the cut-off was derived. The resource and reserve estimations were based on a 2.5% CuEq and the CuEq formula was:

$$CuEq\% = Cu\% + 0.37 * Zn\%$$

In December 2005, reporting of resource and reserve by using CuEq values was replaced with NSR method and the development and stope designs were performed by using NSR cut-off. The NSR value for each block of the model is calculated on the basis of its grades (Cu, Zn, Ag, and Au) and metal recoveries. Metal recoveries are obtained from the recovery curves based upon head grades (See APPENDIX B for the NSR calculation method).

The reserves are reported at a money equivalent of \$US 46 (NSR) per tonne of ore cut-off depending on the present mining cost.

#### **5.4 Grade, Tonnage and NSR Comparisons**

Grade and tonnage curves have been determined from the mineral resource at a series of CuEq cut-off limits (See APPENDIX C, Table C1 for grade and tonnage table). The results are shown in Fig 5.2. There is a logarithmic increase in tonnage with an arithmetic decrease in grade.

NSR and tonnage curves are also shown in Fig 5.3 (see APPENDIX C, Table C2 for NSR and tonnage table). However, when comparison made between NSR and CuEq, resource tonnages are higher according to NSR estimations than the estimations according to CuEq. This is because resource tonnages are calculated for each block of the model on the basis of its grades (Cu, Zn, Ag, and Au) and metal recoveries in NSR system while the calculations are done for only Cu and Zn grades in CuEq system. Therefore, a block which provides a profit with respect to NSR may not provide same profit with respect to CuEq.

The relationship between NSR and CuEq is also shown in Fig 5.4 (see APPENDIX D for the database table). The calculations are basically according to the long term copper and zinc prices and the mining costs. Also the calculations prepared

separately for the two main ore types, Spec Ore and Non-Spec ore. Any increase in copper and zinc prices will also increase total mineral resources and the profit. The fluctuations in Copper and Zinc prices are shown in Fig 5.5. (Copper and zinc prices by monthly since 1990 are also given in Appendix E).

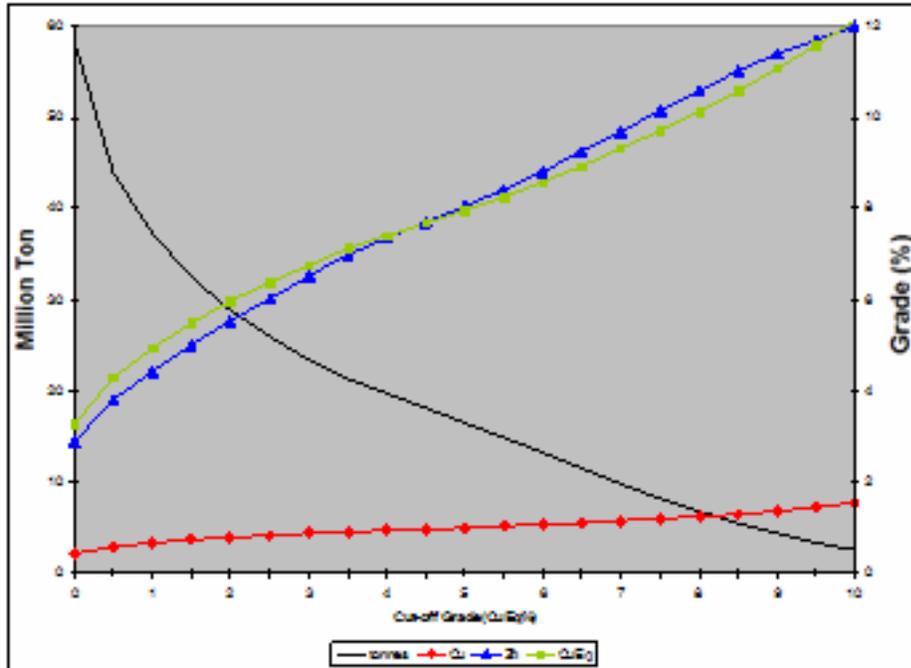


Figure 5.2: Undiluted Mineral Resource Grade/Tonnage Distribution

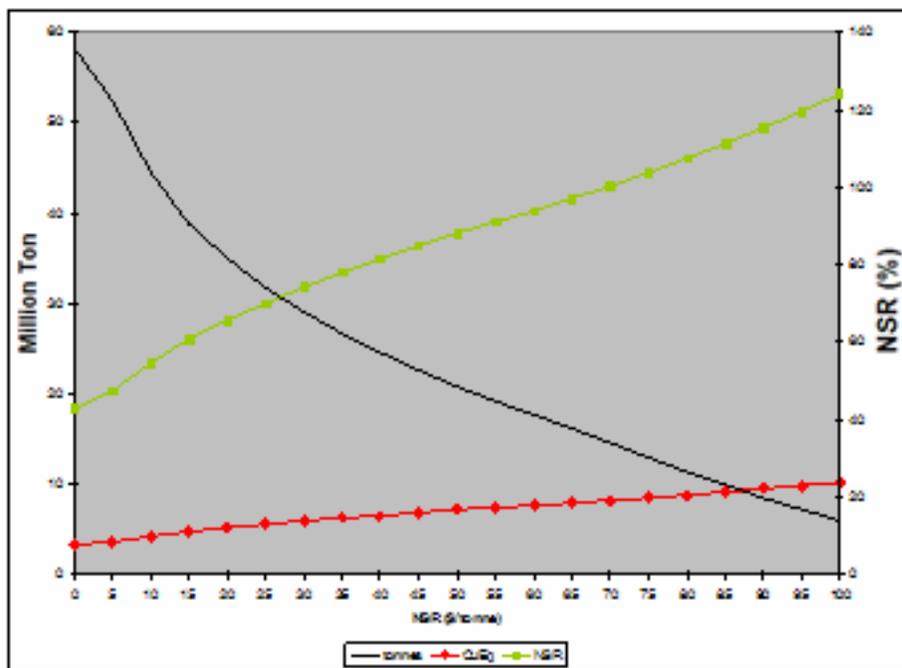


Figure 5.3: Undiluted Mineral Resource NSR/Tonnage Distribution

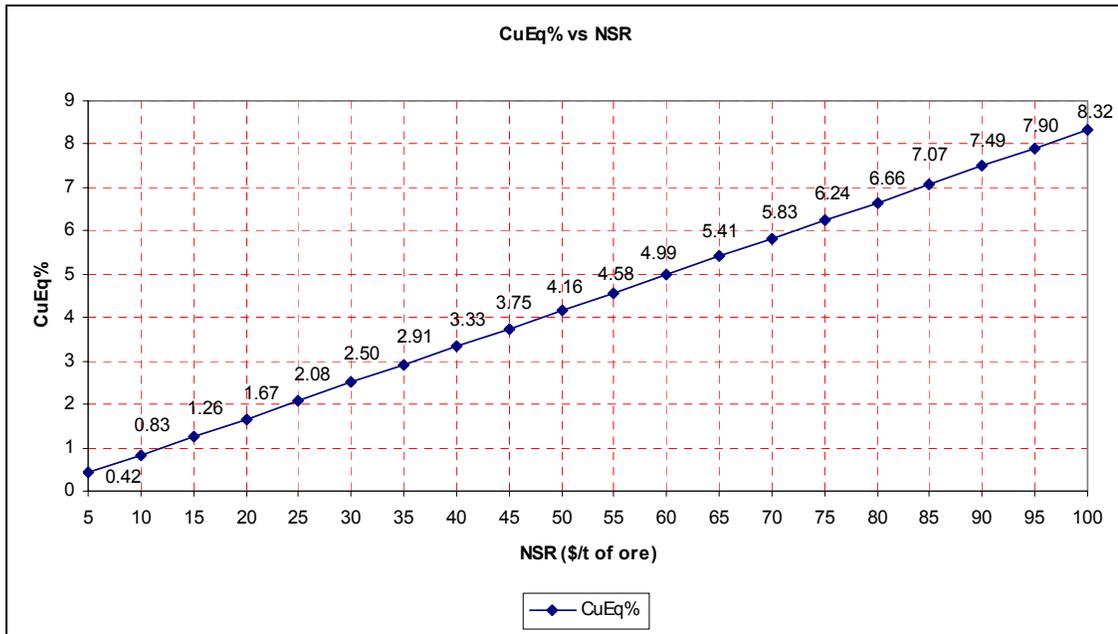


Figure 5.4: NSR versus CuEq

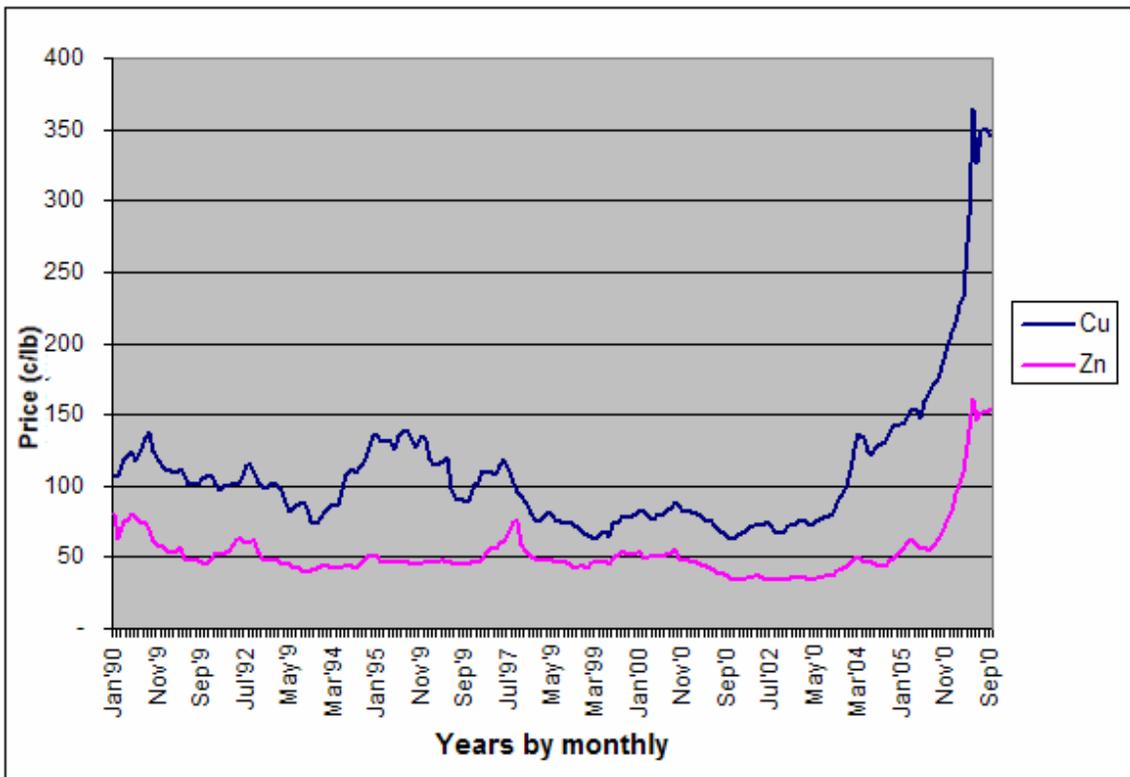


Figure 5.5: Copper and Zinc Prices History

## 5.5 Block Model Limits

A block model was developed based on the parameters in Table 5.1 (Anonymous, 2005a). Blocks in the model have been coded with a domain zone designation. Blocks which straddle an internal boundary between two zones are designated on a majority basis. The percentage of each block which occurs inside the geology domain solids is also stored in order to accurately determine the contained resources.

Table 5.1: Block Model Parameters

	Minimum	Maximum	Size	Number of Blocks
X (East)	800	1200	5 m	80
Y (North)	1400	2150	5 m	150
Z (Elevation)	500	1200	5 m	140

## 5.6 Mineral Resource – Tonnes and Grades

The undiluted Mineral Resources for the Cayeli deposit are calculated and listed in Table 5.2 (Anonymous, 2005a). The distribution of the various categories throughout the deposit is shown in Figure 5.6 (Anonymous, 2005a).

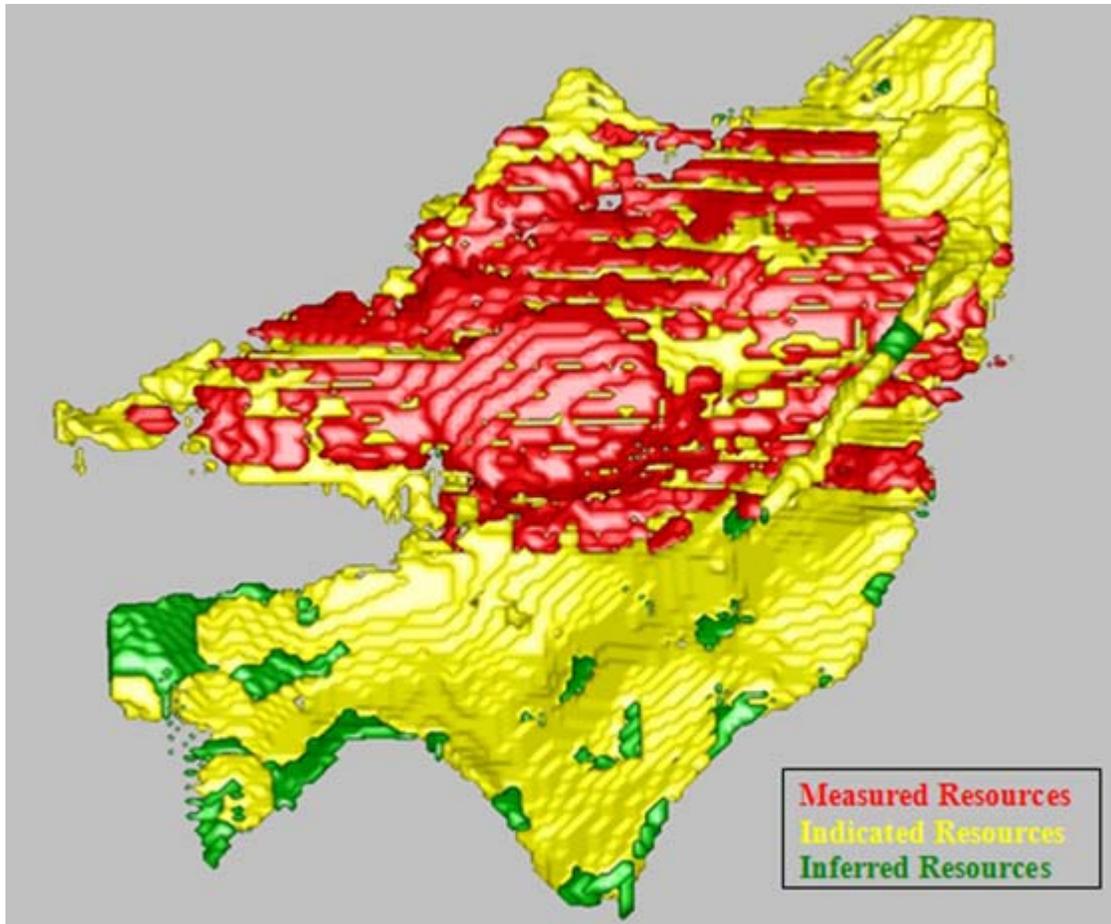
Table 5.2: Undiluted Mineral Resources (Inclusive of Mineral Reserves) in 2005 at a cut-off grade of \$35 NSR/tonne of ore (Anonymous, 2005a)

Category	Mtonnes	Cu %	Zn %	Ag g/t	Au g/t	Pb %	\$ NSR/t
Measured	6.41	4.10	5.84	45	0.66	0.31	78
Indicated	9.61	3.88	5.69	52	0.59	0.36	73
<b>Meas. + Ind.</b>	<b>16.02</b>	<b>3.97</b>	<b>5.75</b>	<b>49</b>	<b>0.62</b>	<b>0.34</b>	<b>75</b>

Inferred	Mtonnes	Cu %	Zn %	Ag g/t	Au g/t	Pb %	\$ NSR/t
Cayeli	0.71	3.55	3.15	28	0.52	0.20	61
Russian Adit	0.45	3.29	11.08	N/A	N/A	N/A	N/A
<b>Total Inferred</b>	<b>1.16</b>	<b>3.45</b>	<b>6.23</b>	<b>N/A</b>	<b>N/A</b>	<b>N/A</b>	<b>N/A</b>

**Notes :**

- 1) CIM definitions were followed for mineral resources.
- 2) Measured and indicated mineral resources are inclusive of mineral reserves.
- 3) Russian Adit inferred resources: Au and Ag have never been assayed.



**Figure 5.6: Distribution of Resource Classification**

The mineral resources were calculated at a cut-off of US\$35 per tonne, which is lower than the cut-off used to report mineral reserves (US\$46 per tonne) by 24%. It is considered to inventory material with potential to be mined at some future date, should higher metal prices and lower mining cost prevails.

### **5.7 Distribution of Resources by Ore Type**

The distribution of mineral resources by ore type is summarized in Table 5.3 (Anonymous, 2005a). The results show that 20% of the remaining resources is Clastic Ore, 28% is Black Ore, and 52% is Yellow Ore.

### **5.8 Comparison with Previous Resource Estimates**

The original (pre-mining) undiluted resource models from 2004 and 2005 are compared in order to see what relative changes may have taken place as a result of such factors as new data, new methodology, new geological interpretation, etc. The result of

the comparison is shown at a cut-off grade of \$35 NSR/tonne of ore in Table 5.4 (Anonymous, 2005a).

**Table 5.3: Mineral Resources by Ore Type in 2005 at a cut-off grade of \$35 NSR/tonne of ore**

Ore Type	Mtonnes	Cu %	Zn %	Ag g/t	Au g/t	Pb %	\$ NSR/t
Clastic	3.36	5.45	9.81	115	1.14	0.73	101
Black	4.73	3.33	9.77	65	0.68	0.50	78
Yellow	8.63	3.70	1.76	14	0.36	0.09	62
<b>Total</b>	<b>16.73</b>	<b>3.95</b>	<b>5.64</b>	<b>48</b>	<b>0.61</b>	<b>0.34</b>	<b>74</b>

**Table 5.4: Comparison of Mineral Resources: December 31, 2005 vs. 2004**

Category	December 31, 2005			December 31, 2004			Difference % (2005-2004)		
	Mtonnes	Cu %	Zn %	Mtonnes	Cu %	Zn %	Mtonnes	Cu %	Zn %
Measured	6.41	4.10	5.84	7.67	4.26	5.90	-16.4	-3.6	-1.0
Indicated	9.61	3.88	5.69	8.16	3.65	5.91	17.8	6.2	-3.7
<b>Meas. + Ind.</b>	<b>16.02</b>	<b>3.97</b>	<b>5.75</b>	<b>15.82</b>	<b>3.94</b>	<b>5.91</b>	<b>1.3</b>	<b>0.6</b>	<b>-2.6</b>

Inferred	Mtonnes	Cu %	Zn %	Mtonnes	Cu %	Zn %	Mtonnes	Cu %	Zn %
Cayeli	0.71	3.55	3.15	2.83	4.43	6.08	-75.1	-19.9	-48.2
Russian Adit	0.45	3.29	11.08	0.50	4.77	10.54	-10.4	-31.0	5.1
<b>Total Inferred</b>	<b>1.15</b>	<b>3.45</b>	<b>6.23</b>	<b>3.33</b>	<b>4.48</b>	<b>6.75</b>	<b>-65.4</b>	<b>-23.1</b>	<b>-7.7</b>

The changes in mineral resources between 2004 and 2005 are due to:

- An update of the interpretation of the mineralized envelope based on diamond drilling carried out this year,
- The removal of isolated blocks,
- The mining some 833,600 tonnes of ore in 2005,
- The shifting from CuEq to a NSR formula.

## CHAPTER 6

### MINERAL RESERVE ESTIMATES

#### 6.1 Mineral Reserves

The Mineral Reserves for the Cayeli deposit are calculated and listed in Table 6.1 (Anonymous, 2005a) by category. As it can be seen from this table, 40% of the remaining reserves is Proven and the rest 60% is Probable. Figure 6.1 shows the process of Mineral Reserve Estimation. All reserves have been calculated at a price of 110 c/lb for copper and 55 c/lb for zinc based on average money equivalent of US\$46/ton (NSR).

**Table 6.1: Mineral Reserves– in 2005 at a cut-off grade of \$46 NSR/tonne of ore**

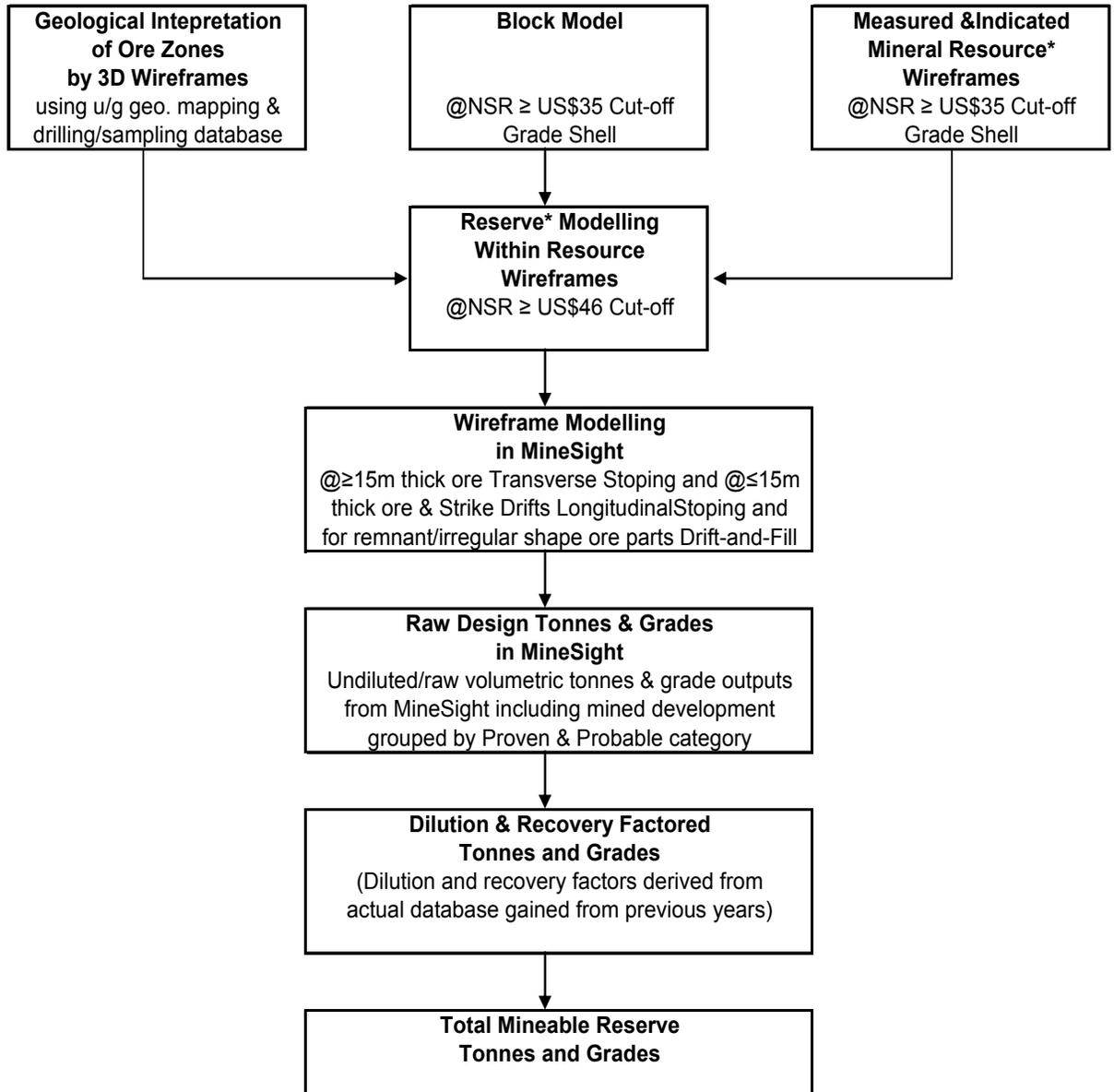
Category	Mtonnes	Cu %	Zn %	Ag g/t	Au g/t	Pb %	\$ NSR/t
Proven	4.70	3.77	5.85	44	0.59	0.30	73
Probable	6.90	3.57	5.88	52	0.53	0.36	69
<b>Total</b>	<b>11.60</b>	<b>3.65</b>	<b>5.87</b>	<b>49</b>	<b>0.56</b>	<b>0.34</b>	<b>70</b>

The mineable reserves are derived from measured and indicated resources. All the designs from Indicated Mineral Resource are categorized as Probable Ore Reserve and the designs from Measured Mineral Resource are categorized as Proven ore Reserve. There are no inferred resources included in the reserve (Figure 6.2).

There are three important parameters used to improve reserve estimations at CBI. They are mine design, dilution and recovery. All of these factors are very important because the long-term and short-term mine planning schedules are all derived from the reserve estimations. All the improvements are achieved by using 3-D mine software program, MineSight, which provides users with an easier and more qualitative approach to basically stope reconciliation compared to traditional calculations generally based on some assumptions.

#### 6.2 MineSight 3-D Mine Software

The MineSight modeling software has been developed by Mintec, Inc., based in Tucson, Arizona, USA. MineSight 3-D software is the main component of Mintec's comprehensive 3-dimensional mine design and geological modeling and evaluation software package, incorporating the MineSight 3-D graphical interface and the MineSight Compass program management interface. This software has been used at CBI since end of 2002. Detailed information can be obtained from the web site [www.mintec.com](http://www.mintec.com).



\* The reserves are estimated at a US\$46 per tonne of ore cut-off due to current high mining costs. But the resources are estimated using a lower cut-off of US\$ 35 per tonne due to the inventory material with potential to be mined at some future date with higher metal prices,

**Figure 6.1: Mineral Reserve Estimation Process**

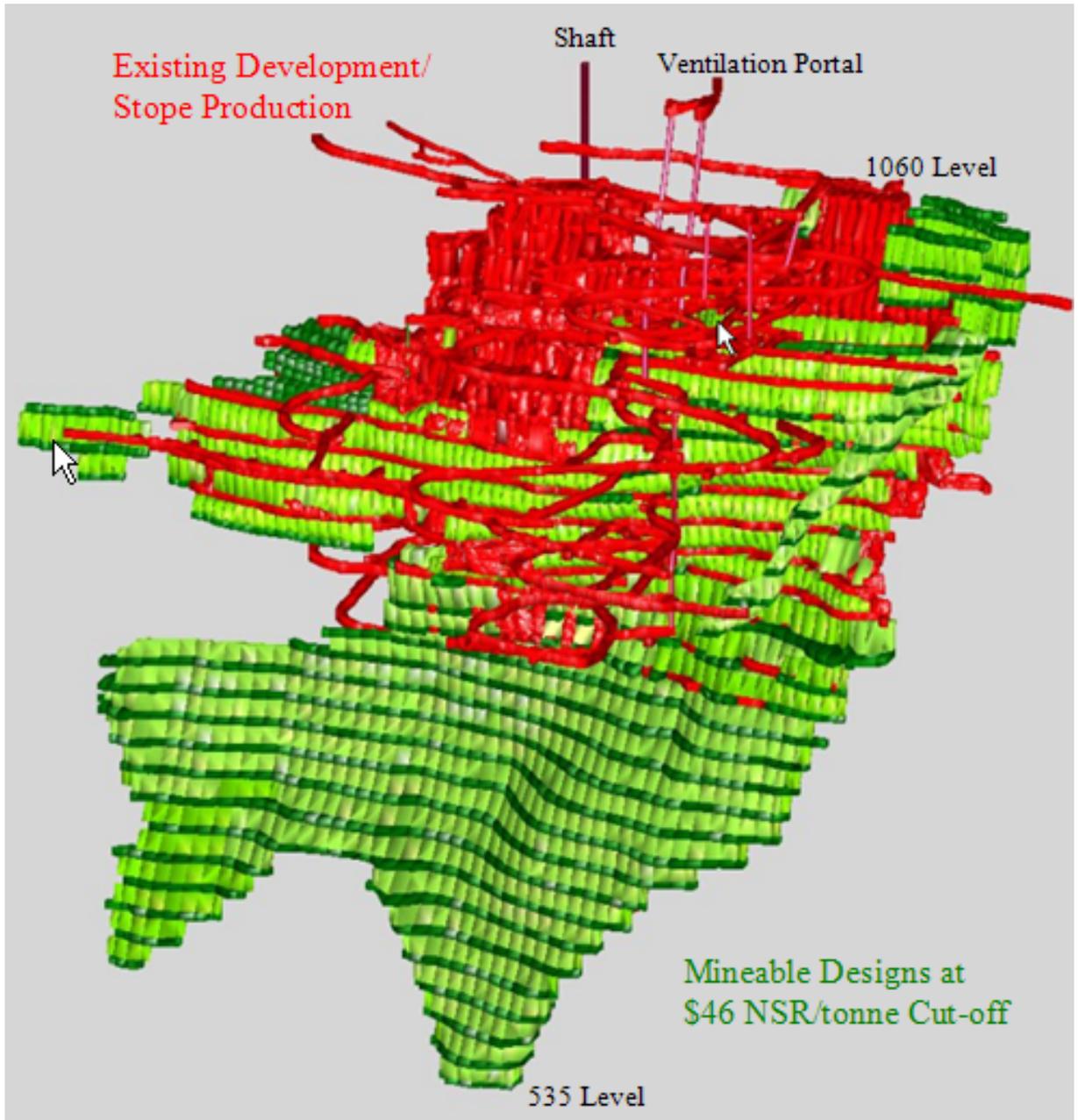


Figure 6.2: Mineral Reserves at a Cut-off Grade of \$46 NSR/tonne of Ore

### 6.3 Mine Design

Detailed mine designs have been developed for all economic material between the 1060 and 535 levels. The majority of the resource outside of these limits remains in the Inferred class and therefore, requires upgrading through future diamond drilling.

Mineral reserves have been developed using an equivalent cut-off limit of US\$46 NSR/tonne cut-off. Individual mining locations must support all local development costs and prove that it can be extracted at a profit. Any ore that can be incorporated in a stope with no extra development or ground support and has a net revenue greater than the marginal cost per tonne is included in mineral reserve tonnes.

Basically the mining method applied is sublevel stoping retreat with post backfilling to extract ore in the Main Ore zone and Deep Ore zone. In this method, the ore is extracted by Transverse and Longitudinal Stopping, which are carried out on 20m vertical sublevels above 800 level (800 level included) and 15m vertical sublevels below 800 level. For backfilling, cemented paste / waste rock is used.

A large proportion (+90%) of the Main Ore zone is extracted using Transverse Stopping (stope height is ~15m) due to the extreme thickness of the ore. An initial Strike Access drift is driven along hangingwall (h/w) contact on each level. Primary sill drifts are then driven, 7m wide and 14m intervals, to the footwall (f/w) contact. Ore between sill drifts at different levels (stope) is blasted by rows in order to retreat towards the mucking drift. If necessary and possible, ore is also blasted by ore type (Clastic, Spec, Stockwork) and mucked out entirely before blasting next row in which ore type is different. The transverse stopes in the Main zone are mined out in two/three parts due to extreme thickness of the ore (up to approximately 60m). Following the extraction of the primary transverse stopes, the openings are backfilled with either cemented rock/waste fill or paste fill. The secondary sill drifts and subsequent stopes are then taken out and filled with waste rock. The final step is to retreat back towards centre of the deposit, extracting the remaining material between the initial strike drifts using Longitudinal Stopping. This material is generally taken out in 15m long intervals in order to allow for backfilling and to reduce the amount of exposed hangingwall.

In the Deep Ore zone, a similar mining method as described above is used in all areas where the ore is greater than 15m in thickness. Narrower ore zones are extracted using the Longitudinal Stopping method. However, the drift/stope dimensions and development direction differ from the Main zone. Initial strike drifts are driven along footwall gradational contact on each level. Primary sill drifts are then driven, 10m wide and 20m intervals, to the h/w contact (Figure 6.3). Ore between sill drifts at different levels is blasted similar in the Main zone with approximately 10m stope height. The aim in Deep zone is to mine the transverse stopes without any split where h/w contact allow good ground conditions, i.e. dip of h/w contact is close to vertical. In areas where the dip becomes relatively flat (approximately 50 degrees), the complete ore zone from the h/w to f/w will be extracted using transverse stoping.

As proportion of the remaining reserve, approximately 24% of the Main zone will be extracted through Longitudinal Stopping and the other 76% through Transverse Stopping. The Deep Ore will have 14% Longitudinal and 86% Transverse Stopes.

#### 6.4 Creating Strings and Wireframes for the Mining Block

The NSR cut-off grades in the block model were used to control the extent of development during the mine design process. Three-dimensional wireframes have been developed which represent all planned strike and sill drifts and stope designs. There are several criteria for the creation of the wireframes:

- A cut-off grade of \$46 NSR/tonne of ore,
- The angle of stope not shallower than 50°,
- Wireframes designed as longitudinal stopes where ore thickness is less than 15m horizontally,
- In cases where isolated patches of resources exist, an economic analysis is conducted in order to ensure the ore mined supports the additional development costs.

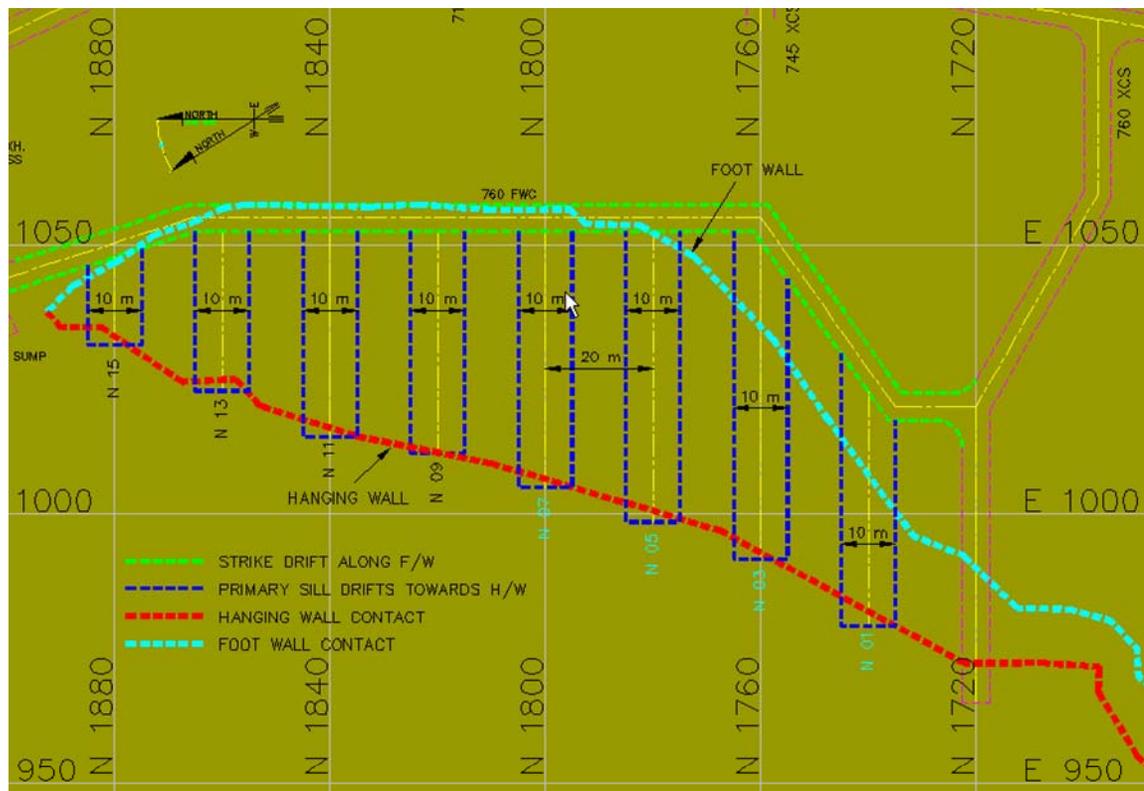
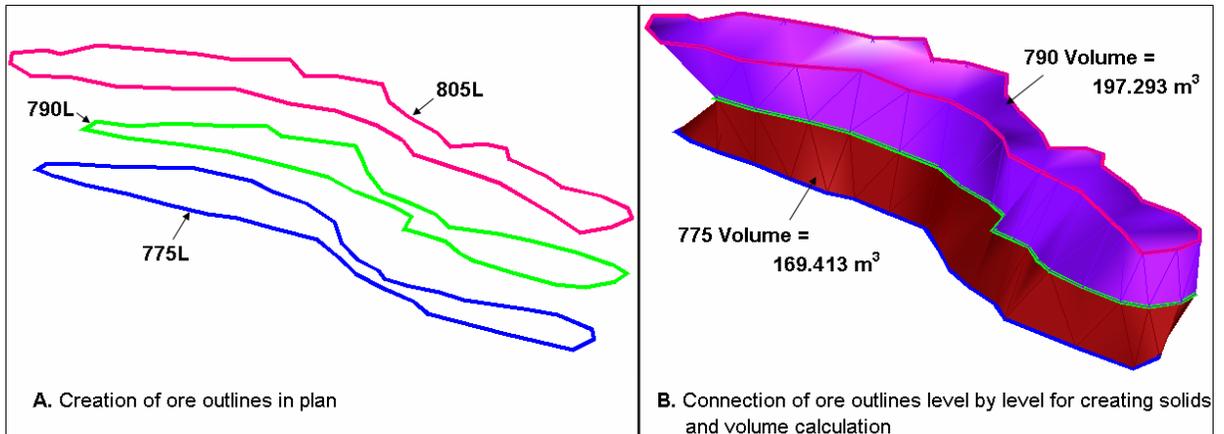


Figure 6.3: Ore Development in Deep Ore Zone (Plan View)

## 6.5 Conventional Method for Wireframe Creation

In conventional method, wireframes were created level by level basically by taking into care just the outlines of the ore body in plan. Then the outlines were linked to create the wireframes and then the open faces closed for solid creation. This is important for volume and tonnage calculations. Solid creation process was repeated for every level (Figure 6.4).



**Figure 6.4: Conventional Method for Wireframe Creation**

There was no other solid created in levels such that strike drifts, sill drifts and stopes. Each level had one solid contained all developments and stopes. Therefore, tonnage of the strike drifts, sill drifts and stopes was calculated as a ratio for each item in level tonnage (e.g. tonnages of strike drifts, sill drifts and stopes were estimated as about 10%, 30% and 60% of the total level tonnage respectively depending on the outline of the ore body in plan). The information gathered from this calculation was very rough because primary and secondary stope tonnages were also calculated as a ratio (as 50%-50% of the total stope tonnage) which plays the most important role in calculation of dilution and recovery factors.

## 6.6 New Method for Wireframe Creation

This system is based on creating wireframes individually for each working place in levels. In this system, at first, strike drifts are created and then sill drifts from the strike drifts are driven. After creation of strike drifts and sill drifts for each level, stope wireframes (primary/secondary stopes and tertiary/longitudinal stopes) are created between levels (Figure 6.5).

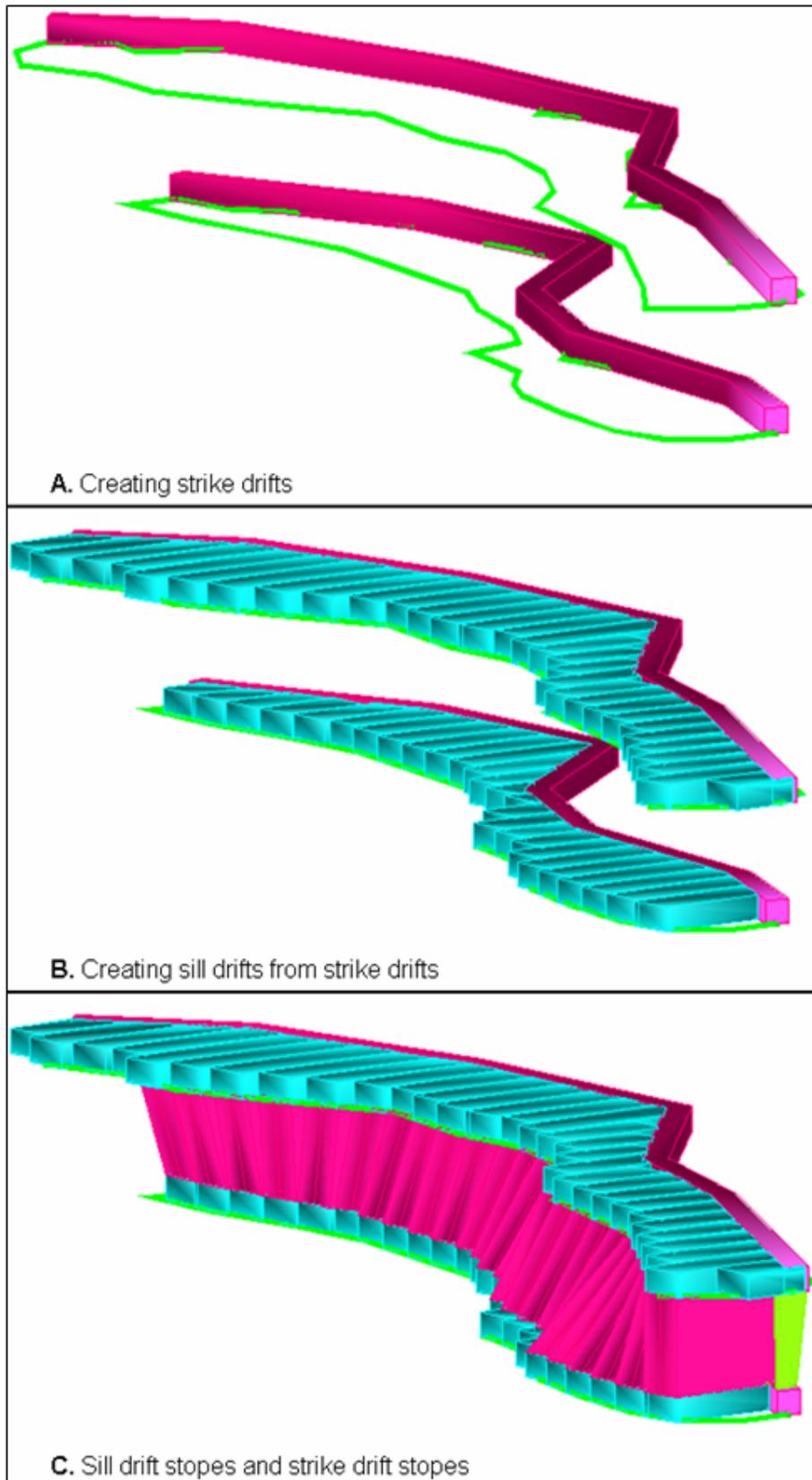


Figure 6.5: New Method for Wireframe Creation

In this system, an attribute (working place name) is given to each wireframe. Therefore, each wireframe has their attributes which serve us to understand type of the working place such as strike / primary / secondary drift and stope (Figure 6.6). As a result, calculating tonnages and grades individually for each working places will also serve us to find out more realistic dilution and recovery numbers because exact total tonnages for primary, secondary and tertiary (strike) drifts and stopes will be calculated in correct.

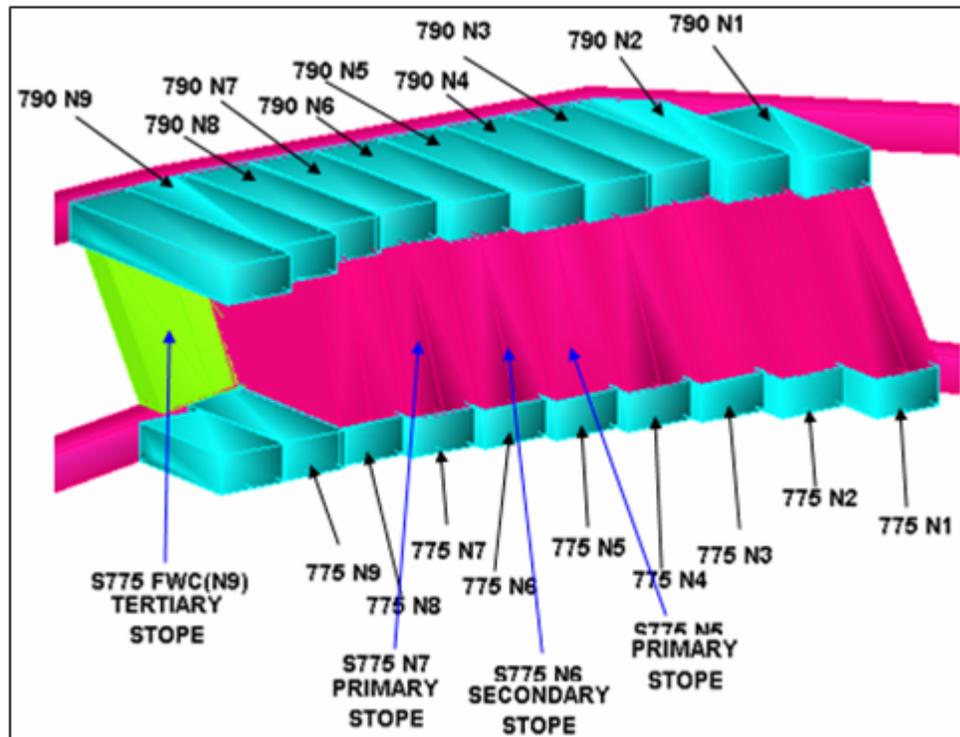


Figure 6.6: Attributes of Each Wireframe

## 6.7 Dilution Calculations

Dilution is the contamination of the ore by non-ore material (Anonymous, 2006). It lowers the quality of the mine product and increases the production cost as a result of handling and the processing of the contaminant. The consequences of this contamination are as follows:

- The actual amount of material extracted will be larger than what is necessary to obtain the same equivalent metal content.
- The grade of the run-of-mine ore will be lower than the estimated in-situ grade.

The consequences stated above directly increase the cost of production (i.e. cost per unit weight of metal mined) since the waste material must be: mucked; transported; crushed; processed and stored as tailings. Furthermore, a mill is designed to operate at a given mill feed grade; lower grade material can unbalance the system resulting in decreased mill recoveries. The mining of waste material also results in an opportunity cost since ore is displaced by waste within the overall mine/mill circuit. This displacement effectively increases the mine life which spreads the cash flow over a longer period of time, resulting in an overall decrease in net present value.

Dilution can occur in two ways: Production dilution and structural dilution (Figure 6.7) (Anonymous, 2006). Contamination of the ore by waste rock may be caused by irregular shape of ore-waste contacts, by the overlying caved waste rock in caving operations, by the mixing of the fill material in the filling operations during the mine production process. Structural type of dilution, such as several waste rock bands within the ore body, occurs inherently related to the geological structure of the ore where selective mining is not suitable.

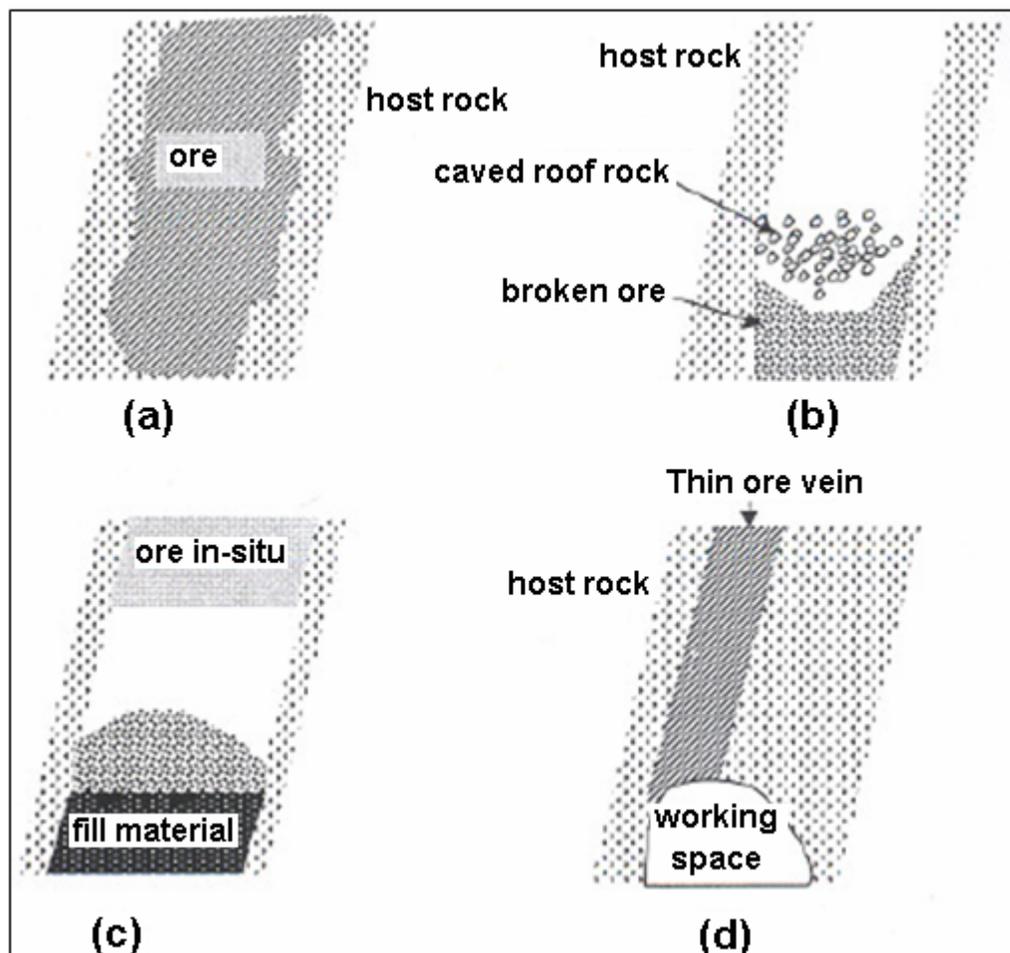


Figure 6.7: Types of Production Dilution of an Ore

There are two types of dilution that are identified, planned dilution and unplanned dilution (Figure 6.8) (Scoble and Moss, 1994). These come from the following sources:

➤ Planned Dilution

- “Internal” dilution from barren dykes and waste inclusions (note that dykes are often narrow and somewhat erratic and, as a result, cannot be effectively separated as waste during mining. Therefore, they are included in the resource estimate as part of the ore zone).
- “Design” dilution where waste material is mined in order to improve the geometry of a stope.
- “Hangingwall” dilution in both longitudinal stopes and some Deep Ore Transverse stopes.
- “Footwall” dilution (which is often low-grade material).

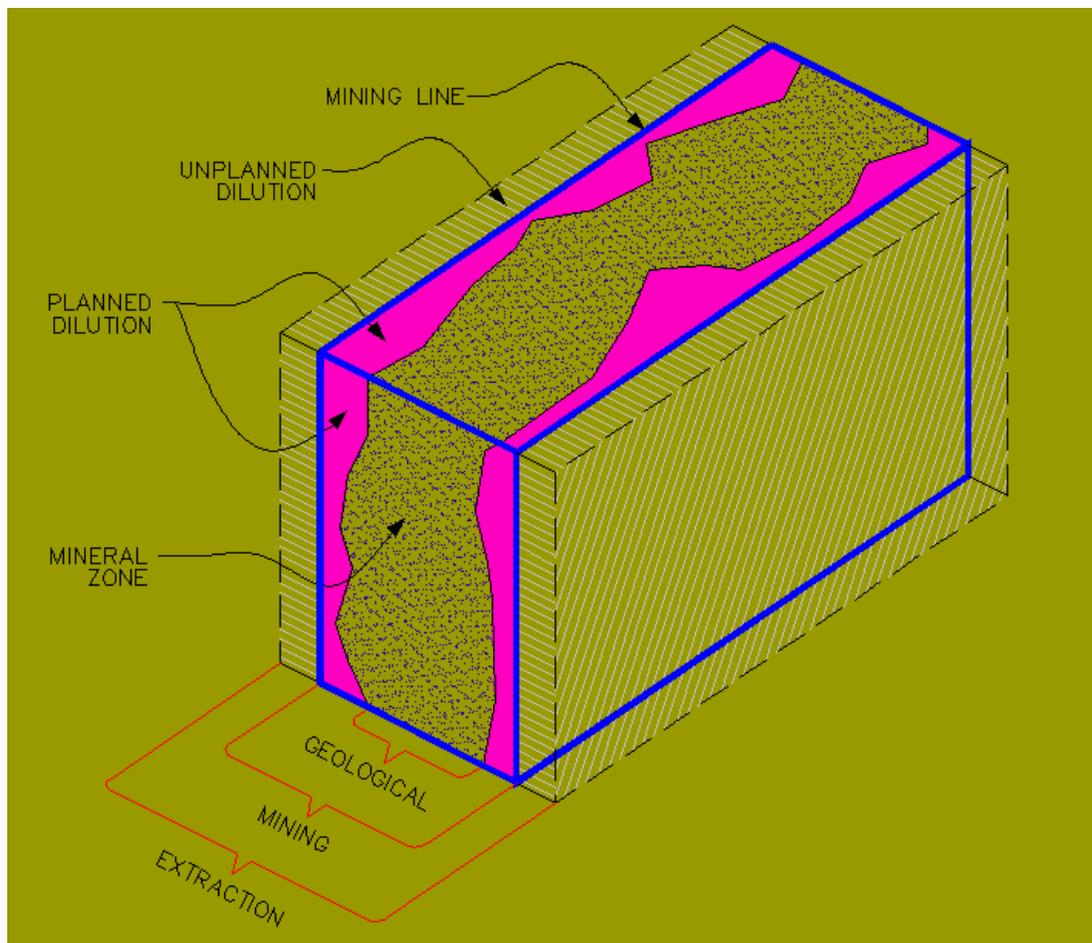


Figure 6.8: Planned and Unplanned Dilution

➤ Unplanned Dilution

- “Backfill” dilution from sidewalls (adjacent stopes) during extraction of secondary and tertiary stopes and from back of blind primary and secondary stopes.
- “Overbreak and/or sloughing” dilution from unstable wall rock induced by blasting of stope.

There are various methods for dilution calculation. Some important definition of dilutions is summarized as follows (Pakalnis, Poulin and Hadjigeorgiou, 1995):

$$\text{EQ1 Dilution} = (\text{Waste mined}) / (\text{Ore mined}) * 100$$

$$\text{EQ2 Dilution} = (\text{Waste mined}) / (\text{Ore mined} + \text{Waste mined}) * 100$$

$$\text{EQ3 Dilution} = (\text{Undiluted in-situ grade reserves}) / (\text{Mill head grades obtained from same tonnage}) * 100$$

EQ2 Dilution definition is used in CBI for dilution calculations. This can also be expressed as:

$$D = \frac{\text{Waste}}{\text{Ore} + \text{Waste}} * 100$$

## 6.8 Old System - Dilution and Recovery Calculations

In the past, dilution was applied to individual workplaces based on the following assumptions:

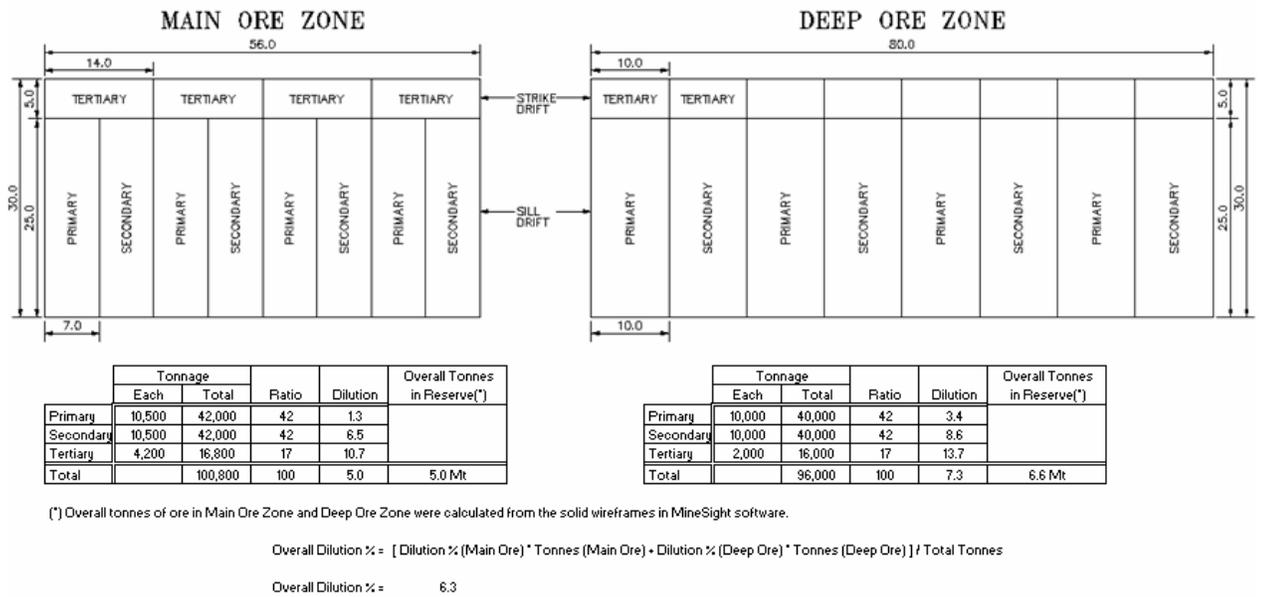
- The orebody was divided into two areas for the purposes of applying dilution (Above the 820 level-Main Ore Zone and below the 820 level-Deep Ore Zone).
- All dilution factors are calculated by tonnage (as opposed to volume).
- All dilution is included at zero grade.
- Average stope sizes for the Main Ore Zone and Deep Ore Zone were 40mx7mx15m and 30mx7mx15m respectively.
- At least one end of all the Transverse stopes is exposed to the H/W or F/W (or both, in case of some Deep Ore Transverse stopes). 0.8m of overbreak during stope blasting was assumed for the primary stopes.

- Secondary stopes had some backfill dilution from the sidewalls in addition to H/W and F/W dilution. This amount was assumed about 0.3m.
- For Tertiary/Longitudinal stopes, overbreaks from sidewalls above the 820 level and below 820 level were assumed as ~0.3m and ~0.4m respectively. The overbreak from just one face was assumed as 0.5m for both regions.

Dilution calculations for primary, secondary and tertiary/longitudinal stopes in Main Ore Zone and Deep Ore Zone were calculated separately and summarized in Table 6.2. For the overall dilution calculations, the ratio of tonnages was taken into care and these ratios were calculated by taking sample block in a level for each zone separately. Dimensions of the blocks (in average width and length) were as 30m x 56 m and 30 m x 80 m for Main Ore Zone and Deep Ore Zone respectively. In Figure 6.9, theoretical calculations can be seen. As a result, the overall average dilution for the mineable reserves was 6.3% depending on the ore tonnages by levels.

**Table 6.2: Dilution Calculations – Old System**

	Main Ore Zone	Deep Ore Zone
<b>Primary/Secondary Stopes</b>		
Stope Length	40 m	30 m
Stope Width	7 m	7 m
Stope Height	15 m	15 m
Ore Density	4 t/m <sup>3</sup>	4 t/m <sup>3</sup>
Waste Density	2.7 t/m <sup>3</sup>	2.7 t/m <sup>3</sup>
Stope Tonnage	16,800 t	12,600 t
<b>Tertiary/Longitudinal Stopes</b>		
Stope Length	20 m	20 m
Stope Width	5 m	5 m
Stope Height	15 m	15 m
Ore Density	4 t/m <sup>3</sup>	4 t/m <sup>3</sup>
Waste Density	2.7 t/m <sup>3</sup>	2.7 t/m <sup>3</sup>
Stope Tonnage	6,000 t	6,000 t
<b>Dilutions</b>		
	<b>Main Ore Zone</b>	<b>Deep Ore Zone</b>
<b>Primary</b>		
From face	213 t	425 t
	(0.75m from f/w)	(0.75m from f/w&h/w)
From sidewall	0 t	0 t
	(0.00m from sides)	(0.00m from sides)
<b>Total Dilution %</b>	<b>1.3</b>	<b>3.4</b>
<b>Secondary</b>		
From face	213 t	425 t
	(0.75m from f/w)	(0.75m from f/w&h/w)
From sidewall	875 t	656 t
	(0.27m from sides)	(0.27m from sides)
<b>Total Dilution %</b>	<b>6.5</b>	<b>8.6</b>
<b>Tertiary/Longitudinal</b>		
From face	101 t	101 t
	(0.50m from one face)	(0.50m from one face)
From sidewall	543 t	721 t
	(0.34m from sides)	(0.45m from sides)
<b>Total Dilution %</b>	<b>10.7</b>	<b>13.7</b>



**Figure 6.9: Calculation of Overall Dilution in Old System**

Overall, the average dilution factors are summarized in Table 6.3.

**Table 6.3: Dilution Factors – Old System**

Stope Type	Dilution Factor
Primary Transverse Stopes (dilution from one end, FW or HW)	2.5%
Secondary Transverse Stopes (dilution from one end & sidewalls)	7.7%
Tertiary / Longitudinal Stopes (dilution from one end & sidewalls)	12.4%
<b>Overall</b>	<b>6.3%</b>

For recovery in the past, it was assumed to mine out all of the ore wherever possible. Therefore, there was no recovery calculation done i.e. 100% of ore extraction was assumed.

## 6.9 New System - Dilution and Recovery Calculations

Dilution has been applied to individual workplaces based on the following criteria/assumptions:

- Calculations are depending on the actual stope productions.
- All dilution factors are calculated by tonnage (as opposed to volume).

- Calculations are based on the Cavity Monitoring System (CMS) data of stopes.
- All actual dilutions are calculated for secondary and tertiary stopes and some primary stopes.
- For primary stopes, generally assuming ~0.8m overbreak during stope blasting, dilution from one end (HW or FW) will be 2.0% (calculated according to the average stope length of ~25m, height of ~15m and width of 7m).
- Secondary and tertiary/longitudinal stopes have an average dilution of approximately 5% according to actual CMS survey data.
- Similar dilution factors are assumed for the deep ore zone (ore below the 820 level).
- All dilution is included at zero grade.
- Database used for dilution calculations is from CMS of stopes in 2005. A total of 85 stopes were used in the calculations which were mined out in 2005 (see Appendix F for the calculations, there is also some additional information was given about 2006 calculations as information).

Overall, the average dilution factors are summarized in Table 6.4.

**Table 6.4: Dilution Factors – New System**

<b>Stope Type</b>	<b>Dilution Factor</b>
Primary Transverse Stopes (dilution from one end, FW or HW)	2.0%
Secondary Transverse Stopes (dilution from one end & sidewalls)	5.0%
Tertiary / Longitudinal Stopes (dilution from one end & sidewalls)	5.0%
<b>Overall</b>	<b>4.5%</b>

### **6.10 Recovery Calculations - Ore Recovery / Loss**

Mining recovery is an allowance for the physical risks that occur in a stope during the extraction phase of the production cycle (Anonymous, 2005a). Mining recovery is only applied to the production stope tonnes and not the development tonnes as the development has been completed before the risk associated with the production cycle exists.

Planned and unplanned ore losses come from the following sources:

- Ground problems during advancing overcut/undercut drifts, which may cause stopping advance. The ore left behind may be sterilized, which may not be possible to recover (Figure 6.10A).
- Improper drift advances and blasting of stopes, which may cause underbreaks from sidewalls and from HW and FW faces (Figure 6.10B).
- An average of 1m pillar that is left at back in blind stopes for protecting from unwanted overbreaks from stope backs (Figure 6.10C).
- Losses in long stopes which are split into two and panelled out (Figure 6.10D).

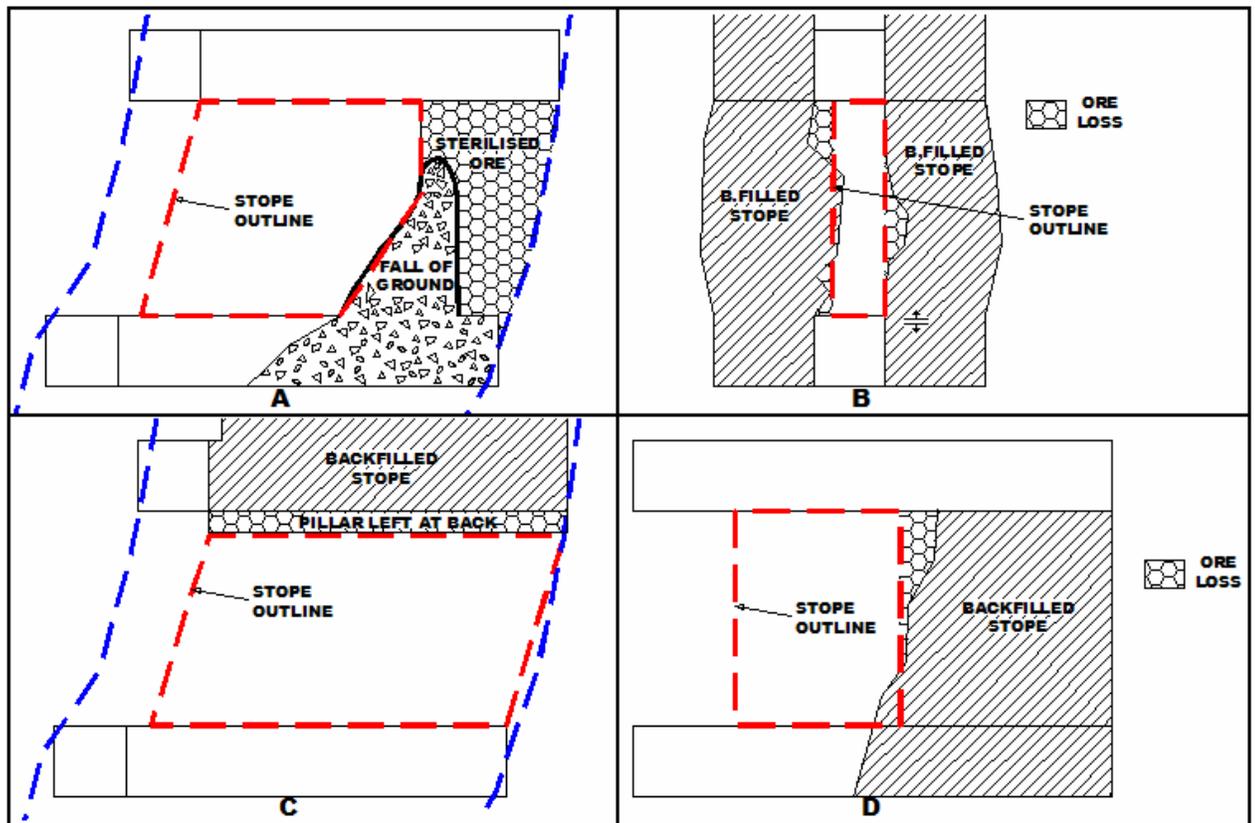


Figure 6.10: Recovery / Ore Loss Sources

The ore loss calculation is summarized as follow (Anonymous, 2005a):

$$\text{Ore Loss \%} = (\text{Ore undermining}) / (\text{Ore planned}) * 100$$

Overall, the average recovery factors are summarized in Table 6.5.

**Table 6.5: Recovery Factors**

Mining Method	Recovery Factor
Normal Stopes (primary and secondary)	95.0%
Blind Stopes (primary and secondary)	90.0%
Stopes in Central Pillar (blind, primary and secondary)	90.0%
<b>Overall</b>	<b>92.5%</b>

### 6.11 Cavity Monitoring System Database

CMS Cavity Monitoring System has been used at Cayeli mine since mid of 1999, but effective usage of this instrument has been started after MineSight 3D software installation. CMS has become one of the basic tools used by underground mine surveyors to determine the extend and progress of mining in an open stope environment.

CMS device has been developed by Optech, Canada (Optech Systems Corporation, 1996). It consists of a computer controlled, motorized scanning head that attaches to 12m long boom (Figure 6.11). The motorized servo-driven head includes reflectorless laser rangefinder, visible laser pointer and reading system providing inclination and rotational position of rangefinder. During a survey the boom with scanning head is inserted into the stope cavity to a position where the outline of the void is visible and can be surveyed (Figure 6.12).



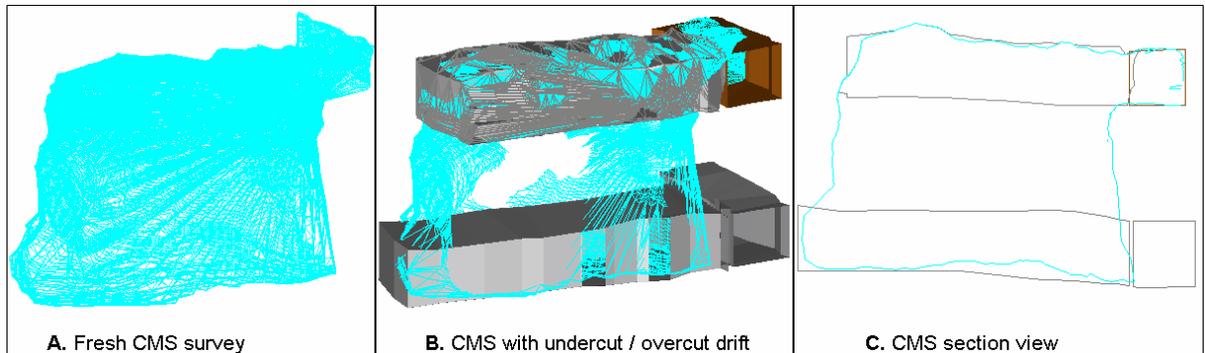
**Figure 6.11: Components of CMS**



**Figure 6.12: CMS in Stope for Survey**

Cavity Monitoring System (CMS) is being used to help gain a better understanding for which factors are most critical with regard to stope wall stability (Figure 6.13). A very thorough stope-by-stope database was maintained detailing the planned stope tonnage based on stope layouts, the actual mined ore based on CMS

surveys, as well as ore loss and backfill and host rock dilution. In 2005, a total of 85 stopes, both blind and conventional, in all categories, primary, secondary, and tertiary, were mined and analyzed.



**Figure 6.13: Results of CMS Survey in a Stope**

In each case, the stope solid is intersected with the CMS solid to calculate dilution and recovery. If the intersection includes volumes of paste fill, waste fill, or host rock, this tonnage is totaled and divided by the CMS tonnage to arrive at a dilution value for that stope.

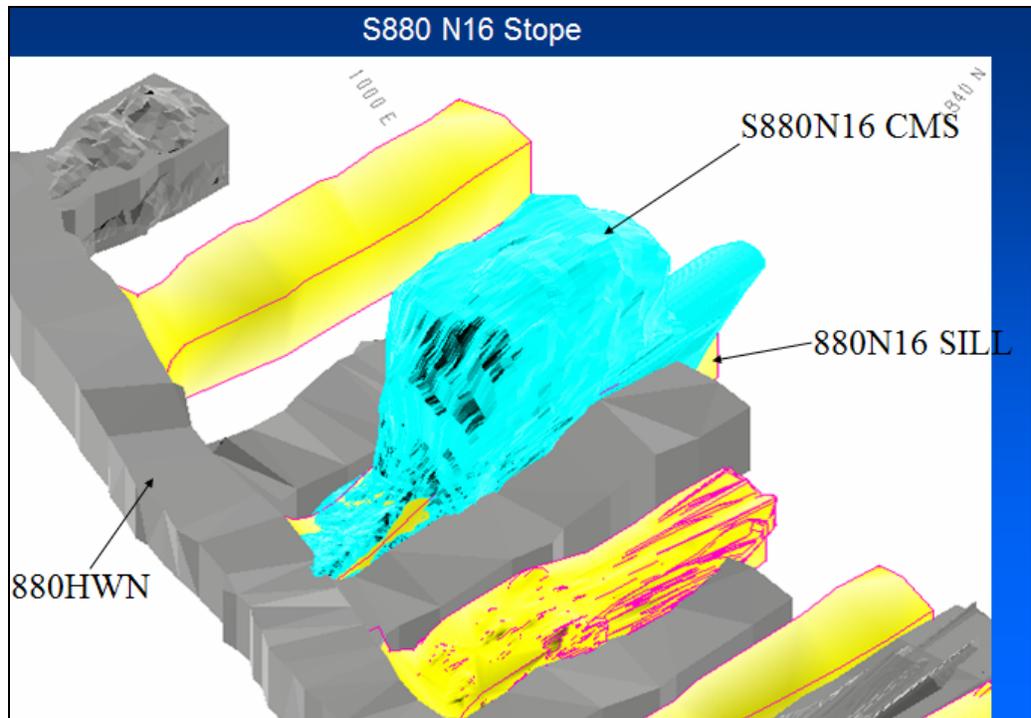
Calculating recoveries requires more discretion. For example, if a primary stope underbreaks, the intersection volume does not necessarily represent ore loss as this volume can be taken with the adjacent secondary or tertiary blasts. If a primary stope overbreaks, this simply means more tonnes are drawn, not a 'negative' ore loss offsetting true or loss within the same stope.

In 2005, the dilution and recovery figures, calculated in the above manner, were 4.5% and 92.5%, respectively. When applying this dilution to the CMS as-mined volumes for 2005, it was seen that an excellent correlation with the mill figures, indicating a validation of the block model and methodology for calculating dilution.

## **6.12 Dilution and Recovery Calculation Process**

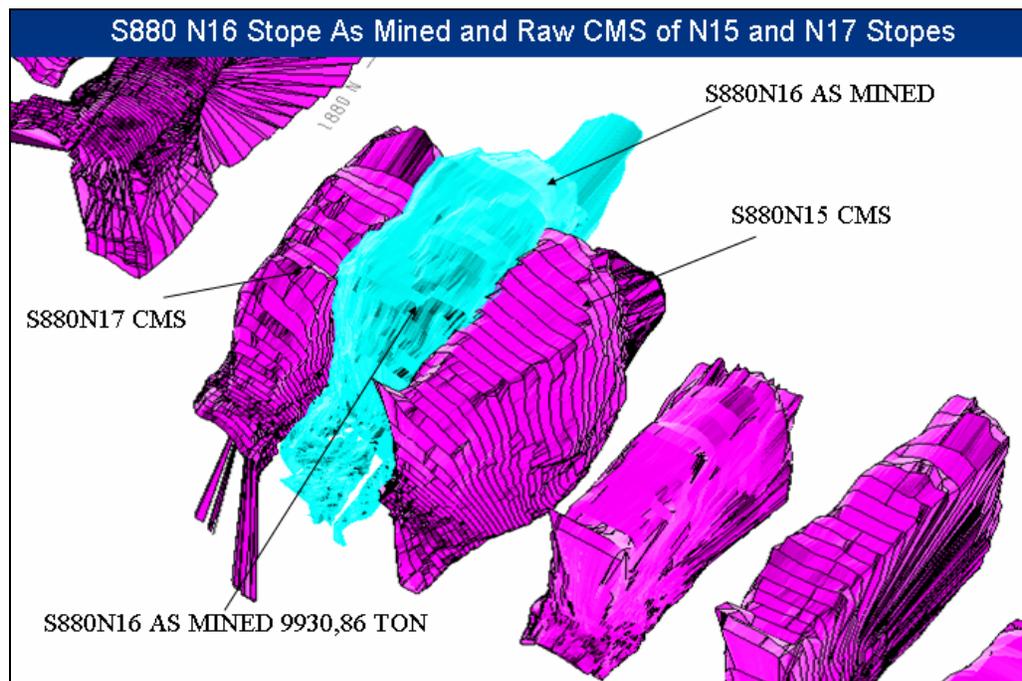
MineSight 3-D software program and Cavity Monitoring System are the basic tools for the calculation of dilution and recovery factors. The procedure for calculation of dilution and recovery/ore loss is as follows:

- (1) Conduction of CMS survey of a stope (In this example, secondary stope of S880 N16 CMS data imported in MineSight 3D-software) (Figure 6.14).



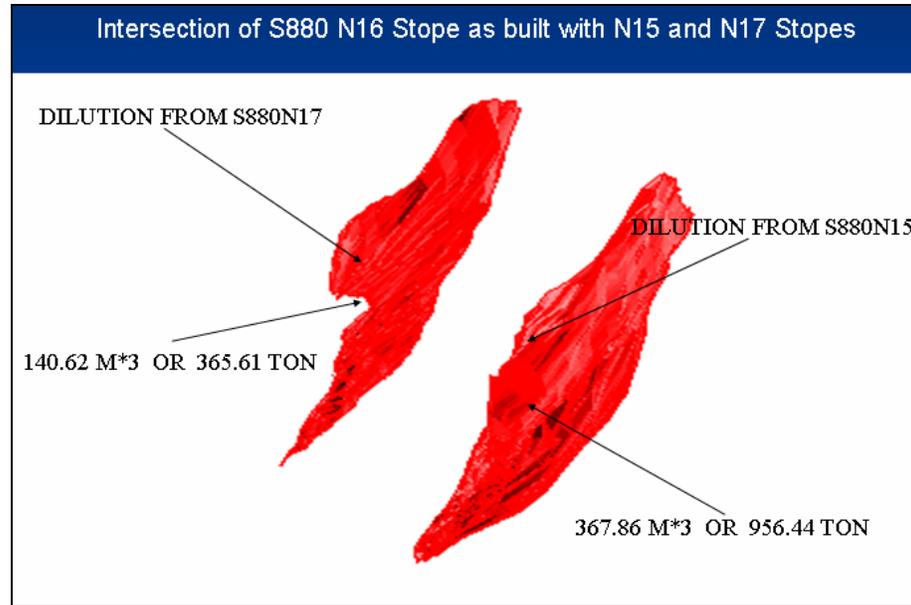
**Figure 6.14: Conduction of CMS Survey**

(2) CMS data of the adjacent stoppes imported (S880 N15 and S880 N17). Volume and tonnage of S880 N16 calculated from MineSight (Figure 6.15).



**Figure 6.15: Importing CMS of Adjacent Stoppes**

- (3) Solids (wireframes) of the adjacent stopes intersected with the S880 N16 stope CMS solid and tonnages of the intersected solids calculated (Figure 6.16).



**Figure 6.16: Intersection of the CMS Data with the CMS's of Adjacent Stopes**

$$\begin{aligned} \text{Dilution of S880 N16} &= (365.61\text{t} + 956.44\text{t})/9930.86\text{t} * 100 \\ &= 13.31\% \end{aligned}$$

- (4) For recovery/ore loss calculation, stope CMS data and the design solid of the same stope are imported (In this example, S880 N16 CMS data and design data imported) (Figure 6.17).
- (5) Solids of CMS data and the design data intersected and tonnages of the intersected solids calculated (Figure 6.18). In this method, planned solid is subtracted from the actual CMS solid.

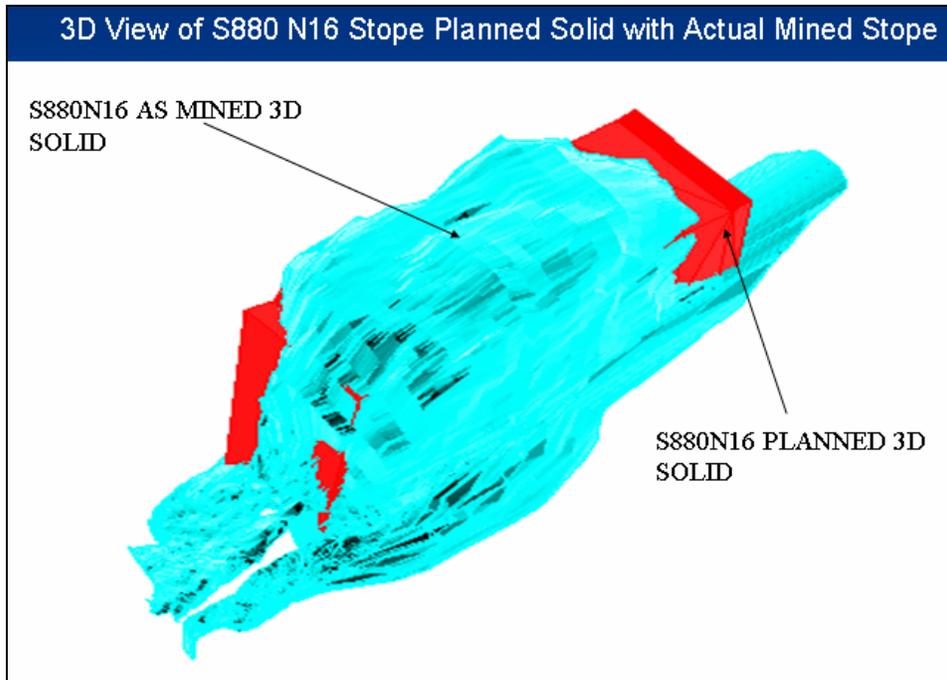


Figure 6.17: Importing Planned Solid



Figure 6.18: Subtraction of the Planned Solid from the CMS Data

$$\begin{aligned} \text{Ore Loss of S880 N16} &= 535\text{t} / 9930.86\text{t} * 100 \\ &= 5.39\% \end{aligned}$$

$$\text{So, the Recovery Factor is} = 94.61\%$$

Overall average dilution and recovery/ore loss ratios were calculated for the stopes mined out in 2005 from which CMS data were also gathered. Table showing the dilution and recovery/ore loss calculations were listed in Appendix F.

### 6.13 Reconciliation with Historical Production

Reconciliation comparisons between the diluted reserve model grades and actual grades were carried out on an individual workplace location basis throughout the 2005 production year (Anonymous, 2005b). In order to carry out the reconciliation, as mined volumes are accurately surveyed with CMS and intersected with the geological (undiluted) model to calculate actual tonnes and grades within the surveyed volumes. Dilution is then applied to the geological (undiluted) grades. The tonnes inherently include any resulting dilution. These figures are then compared to the actual milled tonnes and grades to obtain a relative difference.

The 2005 reserve model slightly underestimated copper and slightly over estimated zinc. Table 6.6 shows reconciliation between mill grades (actual) and diluted model grades for 2005, while Figure 6.19 shows the relative differences for copper and zinc grades from year 2003 to 2005. The yearly grade difference between mill actual grades and mine diluted model grades is a typical characteristic of a massive sulphide deposit.

**Table 6.6: Actual vs. Model Grade Reconciliation – 2005 Production Year (Anonymous, 2005b)**

<b>Metal</b>	<b>Actual Grade (%)</b>	<b>Diluted Model Grade (%)</b>	<b>Difference (%)</b>
Copper	3.840%	3.837%	-0.07%
Zinc	6.740%	6.813%	1.08%

On a short-term basis (daily, weekly, monthly) CBI reports that grade reconciliation between the geology model and mill grades is essential based on the broken ore stope sample grades, adjusted to mill grades. Stope grades for a specific month are adjusted according to the ratio of broken ore sample grade to mill grade. The adjusted grades become the ‘real’ grades and compared to a ‘best guess’ diluted block model for which dilution is visually estimated by a geology technician when visiting stopes. The estimated dilution factor does not correspond necessarily to the unplanned dilution factor and is not applied in every case. The estimated factor is generally lower than the unplanned dilution factor. The difference between the two is sometimes quite significant. Adjustment to block model tonnage is based on the truck/mill tonnage ratio.

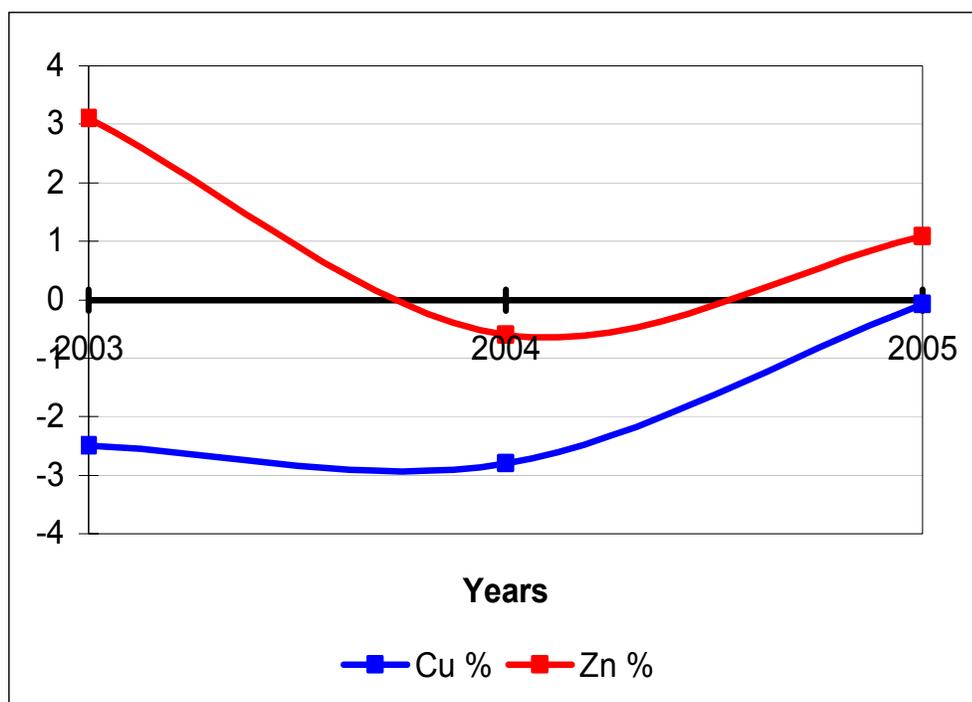


Figure 6.19: Copper and Zinc Grade Reconciliation from 2003 to 2005 Production

#### 6.14 Comparison with Previous Estimates

Table 6.7 compares the current mineral reserves with the previous estimates.

Table 6.7: Comparison of Mineral Reserves: December 31, 2005 vs. 2004 (Anonymous, 2005a)

Category	December 31, 2005			December 31, 2004			Variance % (2005-2004)		
	Mtonnes	Cu %	Zn %	Mtonnes	Cu %	Zn %	Mtonnes	Cu %	Zn %
Proven	4.70	3.77	5.85	5.44	4.01	5.69	-13.6	-5.9	2.9
Probable	6.90	3.57	5.88	8.85	3.06	5.06	-22.1	16.6	16.2
<b>Total</b>	<b>11.60</b>	<b>3.65</b>	<b>5.87</b>	<b>14.29</b>	<b>3.42</b>	<b>5.30</b>	<b>-18.9</b>	<b>6.7</b>	<b>10.7</b>

Note : Variance expressed as percentage change from December 31, 2004 estimates.

The overall changes (gain/loss) to the reserve during the year 2005 are presented in Table 6.8.

Stope definition drilling resulted in the transfer of the most probable reserves into proven reserves.

The total reserve loss, which represents 1.86 Mt, is considered sterilized and has been removed from the reserves. This includes approximately 1.2 Mt of ‘bits and pieces’ scattered throughout, or surrounding, the as-mined wireframes and no longer considered to be accessible. In addition, approximately 0.25 Mt have been removed from the reserves on the north sides of the levels 1020, 1040 and 1060. These tonnes are either sterilized due to falls of ground or their extraction would negatively effect the critical surface infrastructure such as the production hoist. Approximately 0.41 Mt of inferred resources have also been removed from the mineral reserves.

**Table 6.8: Gain (Loss) to 2005 Mineral Reserves**

<b>Metal</b>	<b>Mtonnes</b>	<b>Cu%</b>	<b>Zn%</b>
Reserve Dec 31, 2005	11.6	3.65	5.87
Reserve Dec 31, 2004	14.3	3.42	5.30
Reserve Loss in 2005	2.7	2.43	2.85
Ore Processed in 2005	0.83	3.84	6.74
Total Reserve Loss in 2005	1.86	1.80	1.11

### 6.15 Comparison of Dilution and Recovery Ratios : New vs. Old System

The approach developed for dilution and recovery ratios for mineral reserve estimations in 2006 were compared with the calculations in old system (Table 6.9).

**Table 6.9: Summary of Dilution and Recovery by Calculation System**

	Old System	New System
Dilution %	6.30	4.50
Recovery %	100	92.5

The comparison is based on the actual and planned stope tonnages and grades mined out in 2006. The stopes which are compatible one by one were taken into account for the calculations. The database, calculations and reconciliation of Actual vs. Plan results were summarized in Table 6.10, Table 6.11 and 6.12 respectively.

**Table 6.10: Database – Planned vs. Actual Stope Tonnes and Grades in 2006**

WORKING PLACES		PLAN *			ACTUAL		
		Tonne, t	Cu, %	Zn, %	Tonne, t	Cu, %	Zn, %
<b>HEADING</b>							
S1040 X/CUT	BP	2,987	3.19	11.73	1,754	3.35	11.21
S980 N10	BS	6,211	2.62	11.26	4,685	2.81	12.64
S960 C07E-PART1	BS	7,330	1.47	4.83	6,909	1.40	5.68
S960 C01E	BS	7,984	2.49	11.34	7,220	2.01	11.01
S940 CDN (N15-16)	BT	6,266	3.67	9.38	7,050	3.85	6.98
S940 C01E	S	8,690	3.32	7.10	9,364	3.44	7.66
S920 S02E	S	5,928	5.37	4.33	6,070	5.80	1.96
S920 C02W	P	4,327	3.14	13.29	3,125	2.50	11.14
S900 HWNW(N03-N04)	T	4,250	6.26	1.43	4,750	6.70	1.47
S880 N04-PART 2	BS	7,136	8.57	1.54	7,100	9.10	1.40
S880 S18	BS	4,757	3.98	6.13	5,900	3.68	9.90
S880 S14	BS	6,066	2.49	9.22	5,783	2.57	4.51
S860 HWS-P3	T	4,085	3.64	5.52	3,668	3.80	6.12
S840 S16	S	7,626	2.95	3.70	8,100	3.15	5.20
S800 N10	BP	3,325	3.78	0.19	3,800	4.00	0.72
S800 N12	BP	8,006	4.11	0.02	7,920	4.30	0.69
S790 N06	P	6,988	3.55	4.19	8,820	3.72	7.64
S790 N10	P	7,641	4.42	2.76	9,342	4.02	2.36
S775 N04	P	10,810	2.89	7.75	10,625	2.83	8.06
S775 N09	S	10,665	6.21	5.76	9,723	5.00	7.65
S775 N12	P	5,883	4.72	5.30	6,152	4.95	7.64
<b>TOTAL</b>		<b>136,961</b>	<b>3.96</b>	<b>5.95</b>	<b>137,860</b>	<b>3.97</b>	<b>6.06</b>

(\*) No Dilution and Recovery included.

**Table 6.11: Calculation of Tonnes and Grades Including Dilution and Recovery**

WORKING PLACES		PLAN * (NEW SYSTEM)			PLAN ** (OLD SYSTEM)		
		Tonne, t	Cu, %	Zn, %	Tonne, t	Cu, %	Zn, %
<b>HEADING</b>							
S1040 X/CUT	BP	2,887	3.05	11.23	3,175	3.00	11.04
S980 N10	BS	6,004	2.51	10.78	6,602	2.46	10.60
S960 C07E-PART1	BS	7,085	1.41	4.62	7,791	1.38	4.54
S960 C01E	BS	7,718	2.38	10.85	8,487	2.34	10.67
S940 CDN (N15-16)	BT	6,057	3.51	8.97	6,661	3.45	8.82
S940 C01E	S	8,400	3.18	6.79	9,237	3.12	6.68
S920 S02E	S	5,730	5.14	4.14	6,302	5.05	4.07
S920 C02W	P	4,183	3.00	12.72	4,600	2.95	12.50
S900 HWNW(N03-N04)	T	4,108	5.99	1.36	4,518	5.89	1.34
S880 N04-PART 2	BS	6,898	8.20	1.47	7,586	8.06	1.45
S880 S18	BS	4,598	3.81	5.87	5,057	3.74	5.77
S880 S14	BS	5,864	2.38	8.82	6,448	2.34	8.67
S860 HWS-P3	T	3,949	3.48	5.28	4,342	3.42	5.19
S840 S16	S	7,371	2.82	3.54	8,106	2.78	3.48
S800 N10	BP	3,214	3.62	0.18	3,534	3.56	0.18
S800 N12	BP	7,739	3.93	0.02	8,511	3.87	0.02
S790 N06	P	6,755	3.40	4.01	7,428	3.34	3.94
S790 N10	P	7,386	4.23	2.64	8,122	4.16	2.60
S775 N04	P	10,449	2.77	7.42	11,491	2.72	7.29
S775 N09	S	10,309	5.94	5.51	11,336	5.84	5.42
S775 N12	P	5,687	4.52	5.07	6,254	4.44	4.99
<b>TOTAL</b>		<b>132,390</b>	<b>3.79</b>	<b>5.69</b>	<b>145,590</b>	<b>3.72</b>	<b>5.60</b>

(\*) 4.5% Dilution and 92.5% Recovery included in new system.

(\*\*) 6.3% Dilution and 100.0% Recovery included in old system.

**Table 6.12: Actual vs. Plan Reconciliation – 2006 Production Year**

	Actual Prod'n.	New System	Differ. %
Tonnage	137,860	132,390	-3.97
Cu %	3.97	3.79	-4.48
Zinc %	6.06	5.69	-6.09

	Actual Prod'n.	Old System	Differ. %
Tonnage	137,860	145,590	5.61
Cu %	3.97	3.72	-6.10
Zinc %	6.06	5.60	-7.68

It can be seen from the tables that, the new approach provided closer results to the actual production. The biggest difference comes from the recovery of the ore mined out which was assumed to be 100% in the old system. The tonnages calculated by the new system provided ~1.2% better results when compared with the actual tonnages. The changes in copper and zinc grades were also relatively close to the each other. Both copper and zinc grades are ~1.8% better than the old system. The basic result in improvement of the calculations comes from using the actual surveyed database and MineSight 3D software.

## CHAPTER 7

### CONCLUSIONS AND RECOMMENDATIONS

Dilution and recovery/ore loss have very important role on mineral reserve estimation affecting the profitability of mining operations. However, it is very difficult quantify them. An approach developed for the calculation of dilution and ore recovery/loss based on the mine design in 3D-software and CMS monitoring database. All calculations were derived from MineSight software. The following conclusions can be drawn from this study:

1. The method of mine design is very important for identifying the dilution and recovery/ore loss factors depending on the type of the working places (as primary, secondary, tertiary).
2. The other important parameter is CMS stope survey system which helps gain a better understanding of stope geometry.
3. Dilution and Recovery factors are calculated according to the CMS database. As a result, the new approach developed for these factors gives better results i.e. the differences between actual and planned tonnages and grades are less than the results obtained from the old method. The results are as below:

	Actual Tonnes	Difference in New System	Difference in Old System
Tonnage	137.860	-4.13%	5.31%
Cu%	3.97	-4.69%	-6.50%
Zn%	6.06	-6.48%	-8.32%

The followings are recommended for further investigations:

1. The mine operation is dynamic so the dilution and recovery factors may change periodically in time and by the working place. Therefore additional data is required to verify the design zones and refine the approach.
2. Dilution and recovery factor calculations should go one step ahead that the calculations need to be done for each level and working place individually.

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**APPENDIX A**

**CANADIAN INSTITUTE OF MINING, METALLURGY AND PETROLEUM  
CIM STANDARDS ON MINERAL RESOURCES AND RESERVES  
DEFINITIONS AND GUIDELINES**

**Prepared By The  
CIM Standing Committee  
On Reserve Definitions**

**Adopted by CIM; Council August 20, 2000**

John Postle Bernie Haystead

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## **INTRODUCTION**

The Committee's proposed standards establish definitions and guidelines for the reporting of Exploration Information, Mineral Resources and Mineral Reserves in Canada and are identified as the "CIM Standards" and referred to as such hereafter in this document. To provide additional clarification to Qualified Persons, guidelines have been included with the respective definitions. All definitions are printed in bold text, whereas the guidelines are printed in italics. The CIM Standards are applicable to all minerals including industrial minerals, diamonds and other gemstones. Reserve definitions for bitumen, natural gas and oil are not included in these Standards. The CIM Standards are not intended to cover mineral inventory estimates that will be reported to government agencies.

## **CIM STANDARDS**

The CIM Standards presented herein provide guidelines for the classification of Mineral Resource and Mineral Reserve estimates into various categories. The category of an estimate implies confidence in the geological information available on the mineral deposit; the quality and quantity of data available on the deposit; the level of detail of the technical and economic information which has been generated about the deposit, and the interpretation of the data and information.

## **HISTORY**

The Canadian Institute of Mining, Metallurgy and Petroleum (CIM) published "Mineral Resource Reserve Classification: Categories, Definitions, and Guidelines" in September 1996.

This report, prepared by the CIM Ad Hoc Committee on Reserve Definitions, is now widely used as a reference and a system for classifying and reporting Resources and Reserves in Canada. Since the publication of that report there have been several meetings sponsored by the Council of Mining and Metallurgical Institutes (CMMI) of which CIM is a member, to develop a Resource/Reserve classification, definition and reporting system that would be similar in Australia, Canada, Great Britain, South Africa and the United States.

The recent history of the development of Resource and Reserve definitions in Canada was discussed in the Ad Hoc Committee Report and is summarized as follows:

- The most widely accepted Canadian reserve classification system through the period 1970 to date has been the one required by the Canadian Securities Administrators (CSA) under National Policy 2-A.
- Geological Circular 831, Principles of a Resource/Reserve Classification for Minerals, which was published in 1980 by the U.S. Bureau of Mines and the U.S. Geological Survey, introduced a classification system that distinguished between resources and reserves.
- The Australian Code for Reporting of Identified Mineral Resources and Ore Reserves (the JORC code), first published in 1989, was similar to the U.S. system in structure but included some important modifications, particularly by including reference to the competence of the person responsible for a resource or reserve estimate. This code prescribed reporting requirements.
- In 1991, CIM, through its Mineral Economics Society, formed a Special Committee on Reserve Definitions. The report of the Special Committee was presented to CIM Council in May 1994 and published in October 1994. In June 1994, CIM established an Ad Hoc Committee to review and revise the Special Committee Report.
- The Society of Mining Engineers in the United States issued “A Guide for Reporting Exploration Information, Resources and Reserves” in 1994.

The Ad Hoc Committee report was accepted by CIM Council in February 1996 and at that time Council established a Standing Committee (the Committee) on Reserve Definitions administered by the Mineral Economics Society. The Ad Hoc Committee Report was published in the September 1996 CIM Bulletin.

In 1993, CMMI sponsored an initiative to obtain consensus on the resource/reserve

definitions used in Australia, Canada, Great Britain, South Africa and the United States. The CMMI reserve definition committee met in 1994 and again in November 1997 in Denver, Colorado. At the Denver meeting in 1997, the representatives agreed on definitions for the major Mineral Resource and/or Reserve categories. The proposed CMMI definitions were published in the CIM Bulletin in February 1998.

The Australasian Institute of Mining and Metallurgy (AusIMM) and the Joint Ore Reserves Committee (JORC) of the AusIMM, the Australian Institute of Geoscientists and the Minerals Council of Australia published a revised draft JORC Code in July 1998. This document proposed the use of the CMMI definitions, with some wording changes. In January 1999, the JORC Code was published, to take effect in September 1999. The SME published revised definitions in January 1999 which follows the CMMI definitions. These definitions have not been adopted for use in the United States by the Securities and Exchange Commission, at this point.

The United Nations Economic Commission for Europe (UN-ECE) published a "United Nations International Framework - Classification for Reserves/Resources" in November 1996. This report is very complex and utilizes ten different categories for classifying resources and reserves. In October 1998, CMMI and UN-ECE representatives met and agreed to use the CMMI definitions in the UN-ECE classification system for the five categories of resources and reserves with the UN-ECE definitions for the remaining UN-ECE categories being retained and used for reporting national mineral inventories.

In Canada in June 1997, the Ontario Securities Commission (OSC) and the Toronto Stock Exchange (TSE) established the Mining Standards Task Force (MSTF). The MSTF released a draft report in June 1998 and a final report entitled "Setting New Standards" in January 1999. One of the primary recommendations of the MSTF Report was the "adoption, by the Canadian Securities Administrators in National Instrument 43-101, of the CIM guidelines for the estimation, classification and reporting of resources and reserves, as amended from time to time". On July 3, 1998, the Canadian Security Administrators (CSA) published a first draft of National Instrument 43-101 (NI 43-101) as the replacement for National Policy 2-A and National Policy 22. A second draft was published on March 27, 2000. The CIM

and the CIM Standing Committee have provided substantial commentary on the 43-101 drafts, particularly in the area of Mineral Resource and Mineral Reserve definitions.

The following proposed CIM standards include many significant changes to the CIM Ad Hoc Committee Report including the inclusion of modified CMMI definitions for Resource and Reserve categories and the elimination of the Possible Reserve category. In addition, these proposed standards have used the JORC Code description material for guidelines for reports that include discussion of tonnage and grades of mine fill, stockpiles, remnants, pillars and low grade mineralization with appropriate modifications. The proposed CIM Standards also reference Paper 88 -21 of the Geological Survey of Canada for the reporting of coal resources and reserves and the report, Reporting of Diamond Exploration Results, Identified Mineral Resources and Ore Reserves published by the Association of Professional Engineers, Geologists and Geophysicists of the Northwest Territories.

## **DEFINITIONS**

Throughout the CIM Standards, where appropriate, 'quality' may be substituted for 'grade' and 'volume' may be substituted for 'tonnage'

### **Qualified Person**

Mineral Resource and Mineral Reserve estimates and resulting Technical Reports must be prepared by or under the direction of, and dated and signed by, a Qualified Person.

**A "Qualified Person" means an individual who is an engineer or geoscientist with at least five years of experience in mineral exploration, mine development, production activities and project assessment, or any combination thereof, including experience relevant to the subject matter of the project or report and is a member in good standing of a Self-Regulating Organization.**

*The Qualified Person(s) should be clearly satisfied that they could face their peers and demonstrate competence and relevant experience in the commodity, type of deposit and*

*situation under consideration. If doubt exists, the person must either seek or obtain opinions from other colleagues or demonstrate that he or she has obtained assistance from experts in areas where he or she lacked the necessary expertise.*

*Determination of what constitutes relevant experience can be a difficult area and common sense has to be exercised. For example, in estimating Mineral Resources for vein gold mineralization, experience in a high-nugget, vein-type mineralization such as tin, uranium etc. should be relevant whereas experience in massive base metal deposits may not be. As a second example, for a person to qualify as a Qualified Person in the estimation of Mineral Reserves for alluvial gold deposits, he or she would need to have relevant experience in the evaluation and extraction of such deposits. Experience with placer deposits containing minerals other than gold, may not necessarily provide appropriate relevant experience for gold.*

*In addition to experience in the style of mineralization, a Qualified Person preparing or taking responsibility for Mineral Resource estimates must have sufficient experience in the sampling, assaying, or other property testing techniques that are relevant to the deposit under consideration in order to be aware of problems that could affect the reliability of the data. Some appreciation of extraction and processing techniques applicable to that deposit type might also be important.*

*Estimation of Mineral Resources is often a team effort, for example, involving one person or team collecting the data and another person or team preparing the Mineral Resource estimate. Within this team, geologists usually occupy the pivotal role. Estimation of Mineral Reserves is almost always a team effort involving a number of technical disciplines, and within this team mining engineers have an important role. Documentation for a Mineral Resource and Mineral Reserve estimate must be compiled by, or under the supervision of, a Qualified Person(s), whether a geologist, mining engineer or member of another discipline. It is recommended that, where there is a clear division of responsibilities within a team, each Qualified Person should accept responsibility for his or her particular contribution. For example, one Qualified Person could accept responsibility for the collection of Mineral Resource data, another for the Mineral Reserve estimation process, another for the mining study, and the project leader*

*could accept responsibility for the overall document. It is important that the Qualified Person accepting overall responsibility for a Mineral Resource and/or Mineral Reserve estimate and supporting documentation, which has been prepared in whole or in part by others, is satisfied that the other contributors are Qualified Persons with respect to the work for which they are taking responsibility and such persons are provided adequate documentation.*

## **Preliminary Feasibility Study**

The CIM Standards describe completion of a Preliminary Feasibility Study as the minimum prerequisite for the conversion of Mineral Resources to Mineral Reserves.

**A Preliminary Feasibility Study is a comprehensive study of the viability of a mineral project that has advanced to a stage where the mining method, in the case of underground mining, or the pit configuration, in the case of an open pit, has been established, and where an effective method of mineral processing has been determined. This Study must include a financial analysis based on reasonable assumptions of technical, engineering, operating, and economic factors and evaluation of other relevant factors which are sufficient for a Qualified Person acting reasonably, to determine if all or part of the Mineral Resource may be classified as a Mineral Reserve.**

## **Exploration Information**

**For the purposes of this report, Exploration Information is a term used to describe information derived from initial activities undertaken to locate and investigate a prospect or deposit and resulting estimates of tonnage and grade that cannot be classified as a Mineral Resource or a Mineral Reserve. If a Qualified Person reports Exploration Information in the form of tonnage and grade, it must be clearly stated that these estimates are conceptual or order of magnitude.**

*It is recognized that in the review and compilation of data on a project or property, previous or historical estimates of tonnage and grade, not meeting the minimum*

*requirement for Mineral Resources, may be encountered. If these estimates are referenced, it must be clearly stated that these estimates are order-of-magnitude and expressed so as not to misrepresent them as an estimate of Mineral Resources or Mineral Reserves.*

## **Mineral Resource**

*Mineral Resources are sub-divided, in order of increasing geological confidence, into Inferred, Indicated and Measured categories. An Inferred Mineral Resource has a lower level of confidence than that applied to an Indicated Mineral Resource. An Indicated Mineral Resource has a higher level of confidence than an Inferred Mineral Resource but has a lower level of confidence than a Measured Mineral Resource.*

**A Mineral Resource is a concentration or occurrence of natural, solid, inorganic or fossilized organic material in or on the Earth's crust in such form and quantity and of such a grade or quality that it has reasonable prospects for economic extraction. The location, quantity, grade, geological characteristics and continuity of a Mineral Resource are known, estimated or interpreted from specific geological evidence and knowledge.**

*The term Mineral Resource covers mineralization and natural material of intrinsic economic interest which has been identified and estimated through exploration and sampling and within which Mineral Reserves may subsequently be defined by the consideration and application of technical, economic, legal, environmental, socio-economic and governmental factors. The phrase 'reasonable prospects for economic extraction' implies a judgement by the Qualified Person in respect of the technical and economic factors likely to influence the prospect of economic extraction. A Mineral Resource is an inventory of mineralization that under realistically assumed and justifiable technical and economic conditions, might become economically extractable. These assumptions must be presented explicitly in both public and technical reports.*

## **Inferred Mineral Resource**

**An 'Inferred Mineral Resource' is that part of a Mineral Resource for which**

**quantity and grade or quality can be estimated on the basis of geological evidence and limited sampling and reasonably assumed, but not verified, geological and grade continuity. The estimate is based on limited information and sampling gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes.**

*Due to the uncertainty which may attach to Inferred Mineral Resources, it cannot be assumed that all or any part of an Inferred Mineral Resource will be upgraded to an Indicated or Measured Mineral Resource as a result of continued exploration. Confidence in the estimate is insufficient to allow the meaningful application of technical and economic parameters or to enable an evaluation of economic viability worthy of public disclosure. Inferred Mineral Resources must be excluded from estimates forming the basis of feasibility or other economic studies.*

## **Indicated Mineral Resource**

**An 'Indicated Mineral Resource' is that part of a Mineral Resource for which quantity, grade or quality, densities, shape and physical characteristics, can be estimated with a level of confidence sufficient to allow the appropriate application of technical and economic parameters, to support mine planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes that are spaced closely enough for geological and grade continuity to be reasonably assumed.**

*Mineralization may be classified as an Indicated Mineral Resource by the Qualified Person when, the nature, quality, quantity and distribution of data are such as to allow confident interpretation of the geological framework and to reasonably assume the continuity of mineralization. The Qualified Person must recognize the importance of the Indicated Mineral Resource category to the advancement of the feasibility of the project. An Indicated Mineral Resource estimate is of sufficient quality to support a Preliminary Feasibility Study which can serve as the basis for major development decisions.*

## **Measured Mineral Resource**

**A 'Measured Mineral Resource' is that part of a Mineral Resource for which quantity, grade or quality, densities, shape, physical characteristics are so well established that they can be estimated with confidence sufficient to allow the appropriate application of technical and economic parameters, to support production planning and evaluation of the economic viability of the deposit. The estimate is based on detailed and reliable exploration, sampling and testing information gathered through appropriate techniques from locations such as outcrops, trenches, pits, workings and drill holes that are spaced closely enough to confirm both geological and grade continuity.**

*Mineralization or other natural material of economic interest may be classified as a Measured Mineral Resource by the Qualified Person when the nature, quality, quantity and distribution of data are such that the tonnage and grade of the mineralization can be estimated to within close limits and that variation from the estimate would not significantly affect potential economic viability. This category requires a high level of confidence in, and understanding of, the geology and controls of the mineral deposit.*

## **Mineral Reserve**

*Mineral Reserves are sub-divided in order of increasing confidence into Probable Mineral Reserves and Proven Mineral Reserves. A Probable Mineral Reserve has a lower level of confidence than a Proven Mineral Reserve.*

**A Mineral Reserve is the economically mineable part of a Measured or Indicated Mineral Resource demonstrated by at least a Preliminary Feasibility Study. This Study must include adequate information on mining, processing, metallurgical, economic and other relevant factors that demonstrate, at the time of reporting, that economic extraction can be justified. A Mineral Reserve includes diluting materials and allowances for losses that may occur when the material is mined.**

*Mineral Reserves are those parts of Mineral Resources which, after the application of all mining factors, result in an estimated tonnage and grade which, in the opinion of the Qualified Person(s) making the estimates, is the basis of an economically viable project after taking account of all relevant processing, metallurgical, economic, marketing, legal, environment, socio-economic and government factors. Mineral Reserves are inclusive of diluting material that will be mined in conjunction with the Mineral Reserves and delivered to the treatment plant or equivalent facility. The term 'Mineral Reserve' need not necessarily signify that extraction facilities are in place or operative or that all governmental approvals have been received. It does signify that there are reasonable expectations of such approvals.*

### **Probable Mineral Reserve**

**A 'Probable Mineral Reserve' is the economically mineable part of an Indicated, and in some circumstances a Measured Mineral Resource demonstrated by at least a Preliminary Feasibility Study. This Study must include adequate information on mining, processing, metallurgical, economic, and other relevant factors that demonstrate, at the time of reporting, that economic extraction can be justified.**

### **Proven Mineral Reserve**

**A 'Proven Mineral Reserve' is the economically mineable part of a Measured Mineral Resource demonstrated by at least a Preliminary Feasibility Study. This Study must include adequate information on mining, processing, metallurgical, economic, and other relevant factors that demonstrate, at the time of reporting, that economic extraction is justified.**

*Application of the Proven Mineral reserve category implies that the Qualified Person has the highest degree of confidence in the estimate with the consequent expectation in the minds of the readers of the report. The term should be restricted to that part of the deposit where production planning is taking place and for which any variation in the estimate would not significantly affect potential economic viability.*

## RESOURCE AND RESERVE CLASSIFICATION

Technical Reports dealing with estimates of Mineral Resources and Mineral Reserves must use only the terms and the definitions contained herein. Figure A.1, displays the relationship between the Mineral Resource and Mineral Reserve categories.

The CIM Standards provide for a direct relationship between Indicated Mineral Resources and Probable Mineral Reserves and between Measured Mineral Resources and Proven Mineral Reserves. In other words, the level of geoscientific confidence for Probable Mineral Reserves is the same as that required for the in situ determination of Indicated Mineral Resources and for Proven Mineral Reserves is the same as that required for the in situ determination of Measured Mineral Resources.

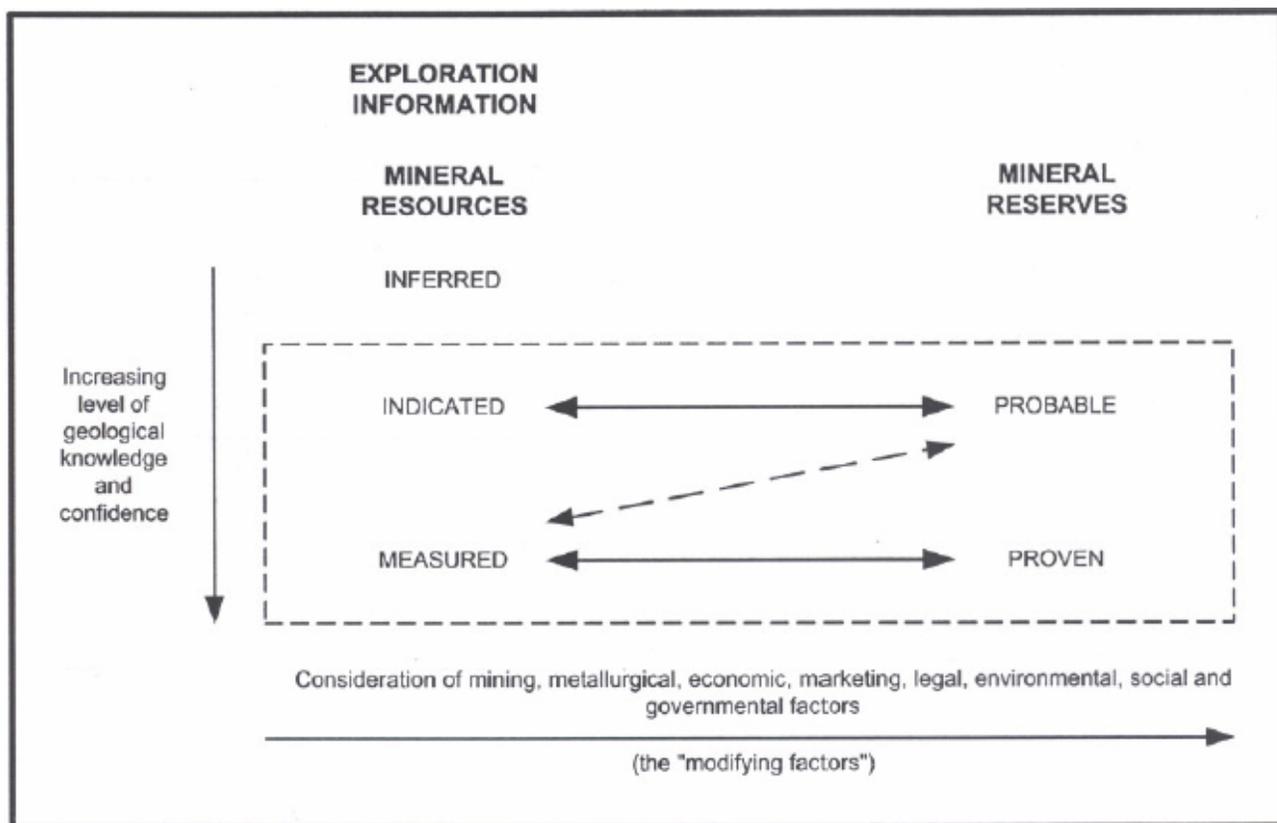


Figure A1: Relationship Between Mineral Resources and Mineral Reserves

*Figure A.1 sets out the framework for classifying tonnage and grade estimates so as to reflect different levels of geological confidence and different degrees of technical and economic evaluation. Mineral Resources can be estimated by a Qualified Person, with input from persons in other disciplines, as necessary, on the basis of geoscientific information and reasonable assumptions of technical and economic factors likely to influence the prospect of economic extraction. Mineral Reserves, which are a modified sub-set of the Indicated and Measured Mineral Resources (shown within the dashed outline in Figure A.1), require consideration of factors affecting profitable extraction, including mining, processing, metallurgical, economic, marketing, legal, environmental, socio-economic and governmental factors, and should be estimated with input from a range of disciplines. Additional testwork, e.g. metallurgy, mining, environmental is required to classify a resource as a reserve.*

*In certain situations, Measured Mineral Resources could convert to Probable Mineral Reserves because of uncertainties associated with the modifying factors that are taken into account in the conversion from Mineral Resources to Mineral Reserves. This relationship is shown by the dashed arrow in Figure A.1 (although the trend of the dashed arrow includes a vertical component, it does not, in this instance, imply a reduction in the level of geological knowledge or confidence). In such a situation these modifying factors should be fully explained. Under no circumstances can an Indicated Resources convert directly to Proven Reserves.*

**In certain situations previously reported Mineral Reserves could revert to Mineral Resources. It is not intended that re-classification from Mineral Reserves to Mineral Resources should be applied as a result of changes expected to be of a short term or temporary nature, or where company management has made a deliberate decision to operate in the short term on a noneconomic basis. Examples of such situations might be a commodity price drop expected to be of short duration, mine emergency of a non-permanent nature, transport strike etc.**

## **GUIDANCE FOR REPORTING MINERAL RESOURCE AND MINERAL RESERVE INFORMATION**

Qualified Persons preparing public reports must follow the requirements in Form 43-101FI of National Instrument 43-101, a preliminary draft of which was published by the Canadian Securities Administrators on March 24, 2000. A copy of the draft Form is available on the following websites: [www.osc.gov.ca](http://www.osc.gov.ca); [www.bcsc.bc.ca](http://www.bcsc.bc.ca); [www.albertasecurities.com](http://www.albertasecurities.com) and [www.cvmq.com](http://www.cvmq.com). The following discussion is included for additional guidance when preparing a Technical Report.

For the CIM Standards a Technical Report is defined as a report that contains the relevant supporting documentation, estimation procedures and description of the Exploration Information, or the Mineral Resources/and Mineral Reserve estimate. The CIM standards recognize the importance of quality Resource and Reserve estimates to the profitable operation of a mine. The CIM Standards encourage practitioners to strive for excellence in the preparation of these estimates.

A Technical Report, with documentation describing the estimates of Mineral Resources and Mineral Reserves must be prepared by or under the direction of, and dated and signed by, a Qualified Person(s). When undertaking exploration programs and generating information required to prepare Mineral Resource and Mineral Reserve estimates, Qualified Persons must comply with the Mineral Exploration "Best Practices" Guidelines prepared by the Mineral Industry Best Practices Committee (Table A2).

*Qualified Persons are encouraged to provide information that is as comprehensive as possible in their Technical Reports on Exploration Information, Mineral Resources and Mineral Reserves. Table A1 provides, in a summary form, a list of the main criteria which should be considered when reporting Exploration Information, Mineral Resources and Mineral Reserve estimates. All of these criteria need not be discussed unless they materially affect estimation or classification of the Mineral Resources and Mineral Reserves. Certain fundamental data such as commodity price used, cut-off grade (where applicable) must be disclosed.*

*Table A1 is a checklist, and is not prescriptive. While it may not be necessary to*

*comment on each item in the table, the need for comment on each item should be considered. It is essential to discuss any matters that might materially affect the reader's understanding of the estimates being reported. Problems encountered in the collection of data or with the sufficiency of data must be clearly disclosed at all times, particularly when they affect directly the reliability of, or confidence in, a statement of Exploration Information or an estimate of Mineral Resources and Mineral Reserves; for example, poor sample recovery, poor repeatability of assay or laboratory results, limited information on tonnage factors etc.*

*Mineral Resource or Mineral Reserve estimates are sometimes reported after adjustment by cutting of high grades or after the application of modifying factors arising from reconciliation with mill data. If any of the data are materially adjusted or modified for the purpose of making the estimate, the nature of the adjustment or modification should be clearly described.*

*Mineral Resource and Mineral Reserve estimates are not precise calculations, being dependent on the interpretation of limited information on the location, shape and continuity of the occurrence and on the available sampling results. To emphasize the imprecise nature of a Mineral Resource or Mineral Reserve estimate, the final result should always be referred to as an estimate, not a calculation.*

*Reporting of tonnage and grade figures should reflect the order of accuracy of the estimate by rounding off to appropriately significant figures. There will be occasions, however, where rounding to one significant figure may be necessary in order to convey properly the uncertainties in estimation. This would usually be the case with Inferred Mineral Resources.*

Technical Reports of a Mineral Resource must specify one or more of the categories of 'Inferred', 'Indicated' and 'Measured' and Technical Reports of Mineral Reserves must specify one or both of the categories of 'Proven' and 'Probable'. Categories must not be reported in a combined form unless details for the individual categories are also provided. Inferred Mineral Resources cannot be combined with other categories and must always be reported separately. Mineral Resources must never be added to Mineral

Reserves and reported as total Resources and Reserves. Mineral Resources and Mineral Reserves must not be reported in terms of contained metal or mineral content unless corresponding tonnages, grades and mining, mineral processing and metallurgical recoveries are also presented.

In situations where estimates for both Mineral Resources and Mineral Reserves are reported, a clarifying statement must be included in the report that clearly indicates whether Mineral Reserves are part of the Mineral Resource or if they have been removed from the Mineral Resources. Mineral Resources and Mineral Reserves must be reported on a site by site basis.

*The CIM Standards recognize that there are legitimate reasons, in some situations, for reporting Mineral Resources inclusive of Mineral Reserves (the Australian approach) and, in other situations, for reporting Mineral Resources additional to Mineral Reserves (the South African and United States approach). The CIM Standards do not express a preference but do require that reporting companies make it clear which form of reporting has been adopted. A single form of reporting should be used in a report. Appropriate forms of clarifying statements may be:*

*‘The Measured and Indicated Mineral Resources are inclusive of those Mineral Resources modified to produce the Mineral Reserves.’*

or

*‘The Measured and Indicated Mineral Resources are additional to the Mineral Reserves.’*

*Inferred Mineral Resources are, by definition, always additional to Mineral Reserves.*

*Mineral Reserves may incorporate material (dilution) which is not part of the original Mineral Resource or exclude material (mining losses) that is included in the original Mineral Resource. It is essential that these fundamental differences between Mineral Resources and Mineral Reserves be noted and caution exercised when attempting to draw conclusions from a comparison of the two.*

*In preparing a Mineral Reserve report, the relevant Mineral Resource report on which it is based should first be developed. This can be reconciled with the Mineral Resource report estimated for the previous comparable period and differences (due, for example, to mine production, exploration, etc.) identified. The application of mining and- other criteria to the Mineral Resource can then be made to develop the Mineral Reserve statement that can also be reconciled with the previous comparable report. A detailed account of differences between estimates is not essential, but sufficient comment should be made to enable significant variances to be understood by the reader. Reconciliation of estimates with production whenever possible is required.*

*Where Mineral Reserve estimates are reported, information on assumed metal or mineral prices, operating costs and mineral processing/metallurgical recovery factors is very important, and should always be included in Technical Reports.*

Reports must continue to refer to the appropriate category or categories of Mineral Resources until technical feasibility and economic viability have been established. If re-evaluation indicates that the Mineral Reserves are no longer viable, the Mineral Reserves may be reclassified as Mineral Resources, if appropriate, or removed from Mineral Resource and Mineral Reserve statements.

The Committee is generally opposed to the reporting of metal equivalence. However, if reporting is carried out in this way, the appropriate correlation formulae including assumed metal prices, metallurgical recovery, comparative smelter charges, likely losses, payable metals, etc. must be included.

*Mineralized stope fill and stockpiles of mineralized material should be considered to be similar to in situ mineralization when reporting Mineral Resources and Mineral Reserves. Consequently the Qualified Person assessing the fill or stockpiles must use the basis of classification outlined in the CIM Standards. In most cases, the opinion of a mining engineer should be sought when making judgements about the mineability of fill, remnants and pillars. If there are not reasonable prospects for the eventual economic extraction of a particular portion of the fill or stockpile, this material cannot be classified as either Mineral Resources or Mineral Reserves. If some portion is currently sub-economic but there is a reasonable expectation that it will become economic, then*

*this material may be classified as a Mineral Resource. Such stockpile material may include old dumps and tailings material. If technical and economic studies of at least a Preliminary Feasibility Study standard have demonstrated that economic extraction could reasonably be justified under realistically assumed conditions, the material may be classified as a Mineral Reserve.*

*The above guidelines apply equally to low grade in situ mineralization, sometimes referred to as 'mineralized waste' or 'marginal grade material', and often intended for stockpiling and treatment towards the end of mine life. For clarity of understanding, it is recommended that tonnage and grade estimates of such material be itemized separately in Technical Reports, although they may be aggregated with total Mineral Resource and Mineral Reserve figures.*

*Stockpiles are defined to include both surface and underground stockpiles, including broken ore in stopes, and can include ore currently in the ore storage system. Mineralized material being processed (including leaching), if reported, should be reported separately.*

*Mineralized remnants, shaft pillars and mining pillars which are potentially mineable are in situ mineralization and consequently are included in the CIM Standards definitions of Mineral Resources and Mineral Reserves. Mineralized remnants, shaft pillars and mining pillars which are not potentially mineable must not be included in Mineral Resource and Mineral Reserve statements.*

## **REPORTING OF COAL RESERVES**

Coal resource and reserve estimates should conform to the definitions and guidelines on Paper 88-21 of the Geological Survey of Canada: "A Standardized Coal Resource/Reserve Reporting System for Canada".

## **REPORTING OF INDUSTRIAL MINERALS**

When reporting Mineral Resource and Mineral Reserve estimates relating to an

industrial mineral site, the Qualified Person(s) must make the reader aware of certain special properties of these commodities. **An Industrial Mineral is any rock, mineral or other naturally occurring substance of economic value, exclusive of metallic ores, mineral fuels and gemstones; that is one of the non-metallic minerals.** To assist Qualified Persons, the following guidelines are presented.

*The quality of industrial mineral deposits is typically measured by physical and/or chemical properties. The properties may be defined by standard industry specifications that must be considered in the classification of Mineral Resources and/or Mineral Reserves.*

*Before a tonnage and quality and/or value per tonne estimate of an industrial mineral deposit can be classified as a Mineral Resource, there must be recognition by the Qualified Person preparing the tonnage and quality estimate that there is a viable market for the product or that a market can be reasonably developed.*

*Before any part of an industrial mineral deposit can be classified as a Mineral Reserve the Qualified Person preparing the tonnage and quality and/or value per tonne estimate must assure himself or herself that the mineral can be sold at a profit through review of specific and identifiable markets for the product.*

*When the quality of any industrial minerals is defined by standard industry specifications and these specifications are used to estimate the value of a tonne of product or products, the industry standard used must be identified. The methods for estimating the value must be explained.*

## **REPORTING OF DIAMONDS AND GEMSTONES**

Mineral Resource and Reserves estimates of diamonds or gemstones must conform to the definitions and guidelines found in "Reporting of Diamond Exploration Results, Identified Mineral Resources and Ore Reserves" published by the Association of Professional Engineers, Geologists and Geophysicists of the Northwest Territories.

*Reports of diamonds or gemstones recovered from sampling programs must specify the number and total weight of stones (in carats for diamonds) recovered. Details of the type and size of samples which produced the diamonds must also be specified including the lower cut-off sieve size and type of sieve used in the recovery. Of equal or greater importance to the total weight of diamonds is diamond value which depends on the colour, size, and proportion of gem and near gem quality of stones recovered. The weight of diamonds recovered may only be omitted from the report when the diamonds are less than 0.5 mm in size (i.e. when the diamonds recovered are microdiamonds).*

*For Technical Reports dealing with diamond or other gemstone mineralization, it is also a requirement of the CIM Standards that, if a valuation(s) of a parcel of diamonds or gemstones is reported, the person(s) or organization valuing the parcel must be named in the report and their professional valuation experience, competency and independence must be stated. If a valuation of a parcel of diamonds is reported, the weight in carats and size range of the contained diamonds must be stated and the value of the diamonds must be estimated in US dollars per carat. If the valuation(s) is not independent, this must be clearly stated.*

*Diamond valuation is a highly specialized process and value can only be reliably estimated for large parcels (at least 2,000 carats) of diamonds from a single deposit. The reliability of valuations of parcels smaller than 2,000 carats decreases as the size of the parcels decreases to the point where valuations placed on a small number of diamonds from exploration samples are likely to be misleading.*

**Table A1:**

Table A1 is a checklist that may be used by Qualified Persons may use when estimating Mineral Resources and Mineral Reserves. Relevance and materiality are overriding principles that determine what information should be presented with the estimates. It is important to report any matters that might materially affect a reader's understanding or interpretation of the results or estimates being reported.

<b>CHECKLIST FOR THE ESTIMATION OF MINERAL RESOURCES</b>	
Database integrity	Measures taken to ensure that data has not been corrupted by, for example, transcription or keying errors, between its initial collection and its use for Mineral Resource estimation purposes. Data validation and due diligence procedures used.
Geological interpretation	Nature of the data used and of any assumptions made. The effect, if any, of alternative interpretations on Mineral Resource estimation. The use of geology in guiding and controlling Mineral Resource estimation. The factors affecting continuity both of grade and geology.
Estimation and modelling techniques	The estimation technique(s) and key assumptions, including treatment of extreme grade values, interpolation parameters, maximum distance of extrapolation from data points, must be appropriate and consistent with best mineral industry practice. The availability of check estimates, previous estimates and/or mine production records and whether the Mineral Resource estimate must take appropriate account of such data. The assumptions made regarding recovery of by-products. In the case of block model interpolation, the block size in relation to the average sample spacing and the search employed. Any assumptions behind modelling of selective mining units (e.g. non-linear kriging). The process of validation, the checking process used, the comparison of model data to drillhole data, and use of reconciliation data if available. The software and version used for computer generated estimates should be identified. When computer techniques are used in Mineral Resource or Mineral Reserve estimation, verification by other techniques is required.
Cut-off grades or parameters, and cutting of high assays	The basis of the cut-off grade(s) or quality parameters applied. If high values have been cut, the level of cutting must be explained and justified. The effect of cutting high grades on the Mineral Resource estimate must be discussed.
Mining factors or assumptions	Assumptions made regarding possible mining methods, minimum mining dimensions and internal (or, if applicable, external) mining dilution.
Metallurgical factors or assumptions	The basis for assumptions or predictions regarding metallurgical amenability.
Tonnage factors (in situ bulk densities) bulk densities)	The determination method used, the frequency of the measurements, the nature, size and representativeness of the samples must be stated.
Classification	The basis for the classification of the Mineral Resources into varying confidence categories. Appropriate account must be taken of all relevant factors. i.e. relative confidence in tonnage/grade estimations, confidence in continuity of geology and recoverable mineral and metal values, quality, quantity and distribution of the data. All Qualified Persons involved in a Mineral Resource estimate must sign off.
Audits or reviews	The results of any audits or reviews of Mineral Resource estimates.

(Table A1 continued)

<b>ESTIMATION OF MINERAL RESERVES</b>	
Mineral Resource estimate for conversion to Mineral Reserves	Description of the Mineral Resource estimate used as a basis for the conversion to an Mineral Reserve. Clear statement as to whether the Mineral Resources are reported additional to, or inclusive of, the Mineral Reserves.
Cut-off grades or parameters	The basis of the cut-off grade(s) or quality parameters applied, including the basis, if appropriate, of equivalent metal formulae. The cut-off grade parameter may be economic value per block rather than mineral or metal grade.
Mining factors or assumptions	The method and assumptions used to convert the Mineral Resource to a Mineral Reserve. The choice of, the nature and the appropriateness of the selected mining method(s) and other mining parameters including associated design issues such as pre-strip, access, etc. The assumptions made regarding geotechnical parameters (e.g. pit slopes, stope sizes, etc.), grade control and pre-production drilling. The major assumptions made and Mineral Resource model used for pit optimisation (if appropriate). The mining dilution factors, mining recovery factors, and minimum mining widths used and the infrastructure requirements of the selected mining methods. Results of bulk sampling and/or test mining must be reported.
Metallurgical and processing factors or assumptions	The metallurgical process proposed and the confirmation of the applicability of that process to the style of mineralization. Whether the metallurgical process is well-tested and "commercialized" technology. The nature, amount and representativeness of metallurgical testwork undertaken and the metallurgical recovery factors applied. Any assumptions or allowances made for deleterious elements: The existence of any bulk sample or pilot scale testwork and the degree to which such samples are representative of the Mineral Reserve as a whole.
Cost and revenue factors	The derivation of, or assumptions made, regarding projected capital and operating costs. The assumptions made regarding revenue including head grade, metal or commodity price(s), exchange rates, transportation and treatment charges, penalties, etc.. The allowances made for royalties payable, both Government and private and, if material, taxes or sales restrictions. Comparisons of operating and capital costs with other similar operations should be made if appropriate.
Market assessment	The demand, supply and stock situation for the particular commodity, consumption trends and factors likely to affect supply and demand into the future. A customer and competitor analysis along with the identification of likely market windows for the product. Price and volume forecasts and the basis for these forecasts. For industrial minerals the customer specification, testing and acceptance requirements prior to a supply contract.
Others	The effect, if any, of natural risk, infrastructure, environmental, legal, marketing, social or governmental factors on the likely viability of a project and/or on the estimation and classification of the Mineral Reserves. The status of titles and approvals critical to the viability of the project, such as mining leases, discharge permits, government and statutory approvals.
Classification	The basis for the classification of the Mineral Reserves into varying confidence categories. The proportion of Probable Mineral Reserves which have been derived from Measured Mineral Resources (if any). Appropriate sign-off by all Qualified Persons involved in a Mineral Reserve estimate is required.
Audits or reviews	The results of any audits or reviews of Mineral Reserve estimates.

**Table A1a:**

<b>ADDITIONAL GUIDANCE FOR THE REPORTING OF SAMPLING TECHNIQUES AND DATA</b>	
<b>CRITERIA</b>	<b>EXPLANATION</b>
Drilling techniques	Drill type (e.g. core, reverse circulation, cable tool rotary air blast, auger, etc.) and details (e.g. core diameter, triple or standard tube, face-sampling bit or other type, etc.). Measures taken to maximize sample recovery and establish representative nature of the samples.
Logging	Core and chip samples must be logged to a level of detail to support appropriate Mineral Resource estimation, mining studies and processing/metallurgical studies. Logging must be quantitative in nature. Core (or trenching, channel etc.) photography. Logging must include where possible the collection of structural data (core samples, rock quality and description).
Drill sample recovery	Core and chip sample recoveries must be properly recorded and results assessed. Establish whether a relationship exists between sample recovery and grade and whether sample bias may have occurred due to preferential loss/gain of fine/coarse material.
Other sampling techniques	Nature and quality of sampling (e.g. channel, random, chips etc.) and measures taken to establish sample representivity.
Sub-sampling techniques and sample preparation	If core, whether cut or sawn and whether quarter, half or all core taken. If non-core, whether riffled, tube sampled, rotary split etc. and whether sampled wet or dry. For all sample types, the nature, quality and appropriateness of the sample preparation technique. Quality control procedures adopted for all sub-sampling stages to maximize representivity of samples. Measures taken to establish that the sampling is representative of the in situ material collected. Confirmation that sample sizes are appropriate to the grain size of the material being sampled.
Quality of assay data and laboratory tests	The nature, quality and appropriateness of the assaying and laboratory procedures used and whether the technique is considered partial or total. Nature of quality assurance procedures adopted (e.g. Standards, blanks, duplicates, external laboratory checks) and whether acceptable levels of accuracy (i.e. lack of bias) and precision have been established.
Verification of sampling and assaying	The verification of significant intersections by either independent or alternative company personnel. The use of twinned holes.
Location of data points	Accuracy and quality of surveys used to locate drill holes (collar and down-hole surveys), trenches, mine workings and other locations used in Mineral Resource estimation. Quality and adequacy of topographic control.
Data density and distribution	The data density and distribution must be sufficient to establish the degree of geological and grade continuity appropriate for the Mineral Resource and Mineral Reserve estimation procedure(s) and classifications applied. Whether sample compositing has been applied

**Table A1b:**

<b>ADDITIONAL GUIDANCE FOR THE REPORTING OF EXPLORATION RESULTS</b>	
Mineral title and land tenure status	Type, reference name/number, location and ownership including agreements or material issues with third parties such as joint ventures, partnerships, overriding royalties, native title interests, historical sites, wilderness or national park and environmental settings. In particular the security of the tenure held at the time of reporting along with any known impediments to obtaining a licence to operate in the area.
Exploration work done by other parties	Acknowledgment and appraisal of previous exploration by other parties, previous audits, reviews and valuation reports
Geology	Deposit type, geological setting and style of mineralization.
Data aggregation methods	Weighting averaging techniques, maximum and minimum grade truncations (i.e. cutting of high grades) and cut-off grades are material and must be stated. Where aggregate intercepts incorporate short lengths of high grade results and longer lengths of low grade results, the procedure used for such aggregation must be stated and some typical examples of such aggregations should be shown in detail. Assumptions used for any use of metal equivalency and the date of the metal equivalency calculation must be clearly stated.
Diagrams	Where possible, maps and sections (with scales) and tabulations of intercepts should be included for any material discovery.
Other substantive exploration data	Other data, if meaningful and material, should be reported including (but not limited to): geological observations; geophysical survey results; geochemical survey results; bulk samples - size and method of treatment; metallurgical test results; bulk density, groundwater, geotechnical and rock characteristics; potential deleterious or contaminating substances.

**Table A2:**

<b>Exploration Best Practices Guidelines</b>	
<p><i><b>Preamble:</b> These guidelines have been prepared to assist the Qualified Person(s) in the planning and supervision of exploration programs which will be reported under National Instrument 43-101. Such exploration programs must be under the supervision of the Qualified Person who will be responsible and accountable for the planning, execution and interpretation of all exploration activity as well as the implementation of quality assurance programs and reporting. These guidelines are also recommended for use in the planning and execution of exploration programs which will not be reported under NI 43-101. This set of broad guidelines or "best practices" has been drawn up to ensure a consistently high quality of work that will maintain public confidence and assist securities regulators. The guidelines are not intended to inhibit the original thinking or application of new approaches, that are fundamental to successful mineral exploration.</i></p> <p><i>Results should be summarized and reported in a Technical Report of good professional quality in accordance with the National Instrument 43-101 and Form 1 contained in that instrument.</i></p> <p><i>All exploration work from which public reporting will ensue must be designed and carried out under the supervision of a Qualified Person ("QP"). A QP is defined in National Instrument 43-101 as an individual who is an engineer or geoscientist with at least five (5) years' experience in mineral exploration, mine development, mine operation or project assessment, has experience relevant to the subject matter of the project or report and is a member in good standing of a recognized professional association.</i></p>	
1. Qualified Person	The Qualified Person may base the exploration program on such geological premises and interpretation of existing information as the QP(s) may decide and select such exploration methods and tools as the QP(s) may judge to be appropriate. In planning, implementing and supervising any exploration work, the Qualified Person should ensure that the practices followed are based on criteria that are generally accepted in the industry or that can reasonably be justified on scientific or technical grounds.
2. Geological Concept	The geological premise on which the exploration work is conducted including the deposit type, geological setting and style of mineralization sought, should be supported by relevant field data and a reasoned scientific approach.
3. Quality Assurance and Control	Throughout the process of mineral exploration, the QP(s) should ensure that a quality assurance program is in place and that any required quality control measures are implemented. Quality assurance programs should be systematic and apply to all types of data acquisition, across the full range of values measured and not only high or unusual results.
4. Exploration Methods & Data Collection	Field work is to be planned and implemented under the direct supervision of a QP(s). Data should be properly recorded and documented at appropriate scales. All data points should be accurately located with respect to known reference points. The QP(s) supervising this work should ensure that any work by employees, contractors or consultants is done by competent personnel and that appropriate quality assurance programs and security procedures are practised. Whenever several persons carry out similar duties or when the data has been collected over a period of time, care should be taken to ensure the quality and consistency of the data being used.
5. Records and Data Verification	The exploration process including planning, mapping, sampling, sample preparation, sample security and analysis or testing should be accompanied by detailed record keeping setting out the procedures followed, the results obtained and the abbreviations used. In addition to paper records, digital storage is encouraged in a standard format on a reliable medium. A program of data verification should be in place to confirm the validity of exploration data that are entered into the database. A summary of records should be included in a periodic technical report produced and signed by the QP(s). Practices used should be well documented and justified.

(Table A2 continued)

6. Sampling	<p>The practices and procedures used in each sampling program should be appropriate for the objectives of the program. All sampling programs should be carried out in a careful and diligent manner using scientifically established sampling practices designed and tested to ensure that the results are representative and reliable. Samples should be collected under the supervision of a QP(s). Quality control programs appropriate to the type of sample and the mineralization should be planned and implemented. These programs should include such measures as external blanks, standards and duplicate samples. Where the volume of individual samples is reduced prior to shipping to a laboratory for analysis, appropriate reduction procedures to obtain representative subsamples should be applied and verified.</p>
7. Drilling	<p>The drilling method will be selected by a QP(s) and should be appropriate to the material being investigated, the objective of the program and local drilling conditions. The drill hole size selected should provide sufficient representative sample material for analysis and reference. Surface and downhole locational surveys should be undertaken using techniques appropriate for the hole size, angle and length of holes. A representative fraction of the drill sample material should be retained, however if material is not retained, the QP(s) should report and explain the reason for this decision.</p> <p>Drill logs, forms or software specifically suited to the type of drilling, the particular geological situation, and the minerals "being sought, should be used for detailed geological logging of core or cuttings. Logs should be appropriately detailed for the type of drilling being conducted, the geological setting, type of mineralization, and geotechnical conditions. Core or sample recoveries should be noted on the logs. Cross sections depicting basic geology and hole data, including correlation with surface geology and any nearby holes should be developed and updated as drilling proceeds. Any downhole geophysical information or other such surveys should also be kept with the drill log. A photographic record of the core is recommended, where appropriate.</p>
8. Sample Security	<p>The security of samples from sample acquisition to analysis is a vital component of the sampling process. Procedures should include the use of secure core logging, sampling, storage and preparation facilities, as appropriate, and the prompt, secure and direct shipping of samples to the laboratories. The QP(s) should endeavour to put in place the best security procedures practical, given the geographic and topographic conditions and the logistics created by the site location.</p>
9. Sample Preparation	<p>The selection of sample preparation procedures should be approved by the QP and should be appropriate to the material being tested, the elements being analyzed and should be subject to the security measures as stated above. All samples that are reduced or split should be processed in a manner such that the fraction analyzed or tested is as representative of the whole sample as possible. Representative fractions of the material to be analyzed or tested should be retained for an appropriate period of time, as decided by the QP. Quality control checks should be undertaken as determined by the QP.</p>
10. Analysis and Testing	<p>Analysis and testing of samples should be done by a reputable and preferably accredited laboratory qualified for the particular material to be analyzed or tested. The selection of a laboratory, testing or mineral processing facility and the analytical methods used will be the responsibility of the QP. The analytical methods chosen must be documented and justified. All analytical or test results should be supported by duly signed certificates or technical reports issued by the laboratory or testing facility and should be accompanied by a statement of the methods used. The reliability of the analytical and testing results should be measured using the results of the quality control samples inserted in the process by the QP. Duplicate analyses at other laboratories should be undertaken.</p>

(Table A2 continued)

11. Interpretation	<p>A comprehensive and ongoing interpretation of all the exploration data is an essential activity at all stages of the project and should be undertaken to assess the results of the work.</p> <p>This interpretation should be based on all of the information collected to date, be systematic and thorough, describe and document the interpretation and discuss any information that appears at variance with the selected interpretation. The density of the exploration data should be critically assessed as to its ability to support the qualitative and quantitative conclusions.</p>
12. Mineral Resource and Reserve Estimation	<p>Estimation of a mineral resource and a mineral reserve are both fundamental steps in project development. The classification and categorization of these estimates must be done in accordance with National Instrument 43-101 and be prepared by a QP(s). The methods and parameters used in making these estimates should be in accordance with the principles generally accepted in Canada and should be presented and justified with the estimate. A mineral resource can be estimated for material where the geological characteristics and the continuity are known or reasonably assumed and where there is the potential for production at a profit. Reserves can be estimated when a positive prefeasibility or feasibility study as defined by NI 43-101 has established the technical, economic and other relevant factors that indicate that these resources can be produced at a profit. Reserve estimates should be based on input and information from a multidisciplinary team under the direction of QP(s).</p>
13. Environment, Safety and Community Relations	<p>All field work should be conducted in a safe, professional manner with due regard for the environment, the concerns of local communities and with regulatory requirements. An environmental program, including baseline studies, appropriate to the stage of the project should be carried out.</p>
14. Recommendations	<p>The interpretation and assessment of the program results at the end of each phase should determine if the program objectives have been met and if further work is justified. Any plan for further work should identify exploration targets, recommend an exploration program and present a budget and schedule. Any changes in working hypotheses and objectives should be recorded.</p>
15. Technical Reporting	<p>A comprehensive technical report signed by the QP(s) should be prepared on completion of a particular phase or stage of work following the format presented in Form 1 of the National Instrument 43-101.</p>

## APPENDIX B

### NSR CALCULATION METHOD

The NSR calculations have been done for Non-Spec ore and Spec-Ore separately due to different characteristics of the ore and recovery factors. Some assumptions were done according to Mill 2006 Five Year Plan and Long Term Reserve Prices and Cost.

**Table B1. Assumptions on Net Smelter Return (NSR) Calculations**

ASSUMPTIONS	NON-SPEC ORE	SPEC ORE	REMARKS
Feed Grade Cu (%)	3.27%	3.43%	From Five-Year Plan
Feed Grade Zn (%)	7.02%	4.07%	From Five-Year Plan
Copper Equivalent, CuEq (%)*	5.96%	4.58%	
Copper in Copper Concentrate (%)	21.00%	25.19%	From Mill Five-Year Plan
Zinc in Copper Concentrate (%)	7.56%	4.14%	From Mill Five-Year Plan
Gold in Copper Concentrate (g/t)	1.26	0.72	From Mill Five-Year Plan
Silver in Copper Concentrate (g/t)	126.00	72.00	From Mill Five-Year Plan
Lead in Copper Concentrate (%)	2.01%	0.67%	From Mill Five-Year Plan
Zinc in Zinc Concentrate (%)	51.29%	51.21%	From Mill Five-Year Plan
Silver in Zinc Concentrate (g)	130.29	95.61	From Mill Five-Year Plan
Copper Recovery (%)	73.40%	87.60%	From Mill Five-Year Plan
Zinc Recovery (%)	74.00%	70.90%	From Mill Five-Year Plan
Copper Price (c/lb)	110	110	From Long Term Reserves Price
Copper Price (\$/mt)	2425.1	2425.1	From Long Term Reserves Price
Zinc Price (c/lb)	55	55	From Long Term Reserves Price
Gold Price (US\$/oz)	450	450	From Long Term Reserves Price
Silver Price (US\$/oz)	5.6	5.6	From Long Term Reserves Price
Tonnes of Cu Conc per Tonne of Ore	0.1142943	0.1192807	
Copper Treatment Charge (\$/t conc)	90	90	From Long Term Reserves Price
Copper Refining Charge (c/lb pay Cu)	9	9	From Long Term Reserves Price
Copper Freight (\$/t conc)	37	37	From Marketing
Tonnes of Zn Conc per Tonne of Ore	0.1012829	0.0563490	
Zinc Treatment Charge (\$/t conc)	175	175	From Long Term Reserves Cost
Zinc Freight (\$/t conc)	27	27	From Marketing
Gold Refining Charge (\$/oz)	5	5	From Long Term Reserves Cost
Silver Refining Charge (\$/oz)	0.4	0.4	From Long Term Reserves Cost

Table B2. Spec Ore and Non-Spec Ore NSR Calculations

	NON-SPEC ORE		SPEC ORE	
	tonne conc \$/dmt	tonne ore \$/dmt	tonne conc \$/dmt	tonne ore \$/dmt
<b>PAYABLE METALS</b>				
Copper in Copper Concentrate	485.02	55.43	586.63	69.97
Silver in Copper Concentrate Credit	17.28	1.98	7.56	0.90
Gold in Copper Concentrate Credit	3.76	0.43	0.00	0.00
Zinc in Zinc Concentrate	524.91	53.16	523.94	29.52
Silver in Zinc Concentrate Credit	4.66	0.47	0.29	0.02
<b>TOTAL</b>	<b>1035.63</b>	<b>111.48</b>	<b>1118.42</b>	<b>100.42</b>
Copper Price Participation	-8.82	-1.01	-10.67	-1.27
<b>DEDUCTIONS</b>				
Copper Treatment Charge	-90.00	-10.29	-90.00	-10.74
Copper Refining Charges				
Cu (\$/dmt)	-39.68	-4.54	-48.00	-5.73
Ag	-1.23	-0.14	-0.54	-0.06
Au	-0.04	0.00	0.00	0.00
Penalties Zn+Pb in Cu Concentrate	-12.14	-1.39	-1.28	-0.15
Zinc Treatment Charge	-175.00	-17.72	-175.00	-9.86
Zinc Price Participation	-34.01	-3.44	-34.01	-1.92
<b>CIF VALUE (US\$/dmt)</b>	<b>674.71</b>	<b>72.94</b>	<b>758.93</b>	<b>70.69</b>
Copper Freight	-40.22	-4.60	-40.22	-4.80
Zinc Freight	-29.35	-2.97	-29.35	-1.65
<b>NSR VALUE (US\$/dmt)</b>	<b>605.14</b>	<b>65.38</b>	<b>689.37</b>	<b>64.24</b>
<b>CuEq Calculation:</b>				
1% Cu, 0% Zn, NSR =	<b>10.97</b>		<b>14.03</b>	
0% Cu, 1% Zn, NSR =	<b>4.20</b>		<b>3.96</b>	
CuEq% =	Cu% + (4.20 / 10.97) * Zn%		Cu% + (3.96 / 14.03) * Zn%	
CuEq% =	Cu% + 0.38 * Zn%		Cu% + 0.28 * Zn%	

## APPENDIX C

### MINERAL RESOURCE TONNES AT A SERIES OF CUEQ CUT-OFF AND NSR LIMITS

**Table C1: Mineral Resource Tonnes at a Series of CuEq Cut-off Limits**

Cutoff	Mtonnes	EQCU	CU	ZN	AG	AU
0.00	58.31	3.29	2.22	2.89	22.70	0.54
0.50	43.99	4.30	2.89	3.81	30.00	0.58
1.00	37.27	4.95	3.31	4.43	35.00	0.61
1.50	32.50	5.50	3.65	5.00	39.80	0.65
2.00	28.82	5.97	3.93	5.54	44.40	0.69
2.50	25.93	6.39	4.16	6.03	48.70	0.73
3.00	23.48	6.77	4.36	6.53	52.70	0.77
3.50	21.35	7.13	4.54	6.99	56.40	0.80
4.00	19.68	7.41	4.69	7.36	59.40	0.82
4.50	18.08	7.69	4.84	7.72	62.30	0.84
5.00	16.53	7.97	4.98	8.06	65.10	0.86
5.50	14.92	8.26	5.14	8.43	68.00	0.88
6.00	13.26	8.58	5.31	8.81	71.30	0.91
6.50	11.50	8.93	5.51	9.25	74.70	0.94
7.00	9.80	9.31	5.73	9.70	78.10	0.97
7.50	8.21	9.71	5.96	10.16	81.30	1.00
8.00	6.75	10.14	6.22	10.60	84.00	1.02
8.50	5.47	10.59	6.51	11.02	87.20	1.05
9.00	4.34	11.07	6.85	11.40	90.60	1.07
9.50	3.39	11.58	7.25	11.71	94.20	1.09
10.00	2.59	12.15	7.71	12.00	98.60	1.10
10.50	2.02	12.70	8.20	12.18	103.60	1.10
11.00	1.59	13.22	8.68	12.28	108.60	1.10
11.50	1.25	13.76	9.22	12.26	113.40	1.10
12.00	1.01	14.24	9.72	12.23	117.10	1.08
12.50	0.80	14.78	10.23	12.30	123.00	1.07
13.00	0.62	15.36	10.82	12.28	129.70	1.06
13.50	0.50	15.88	11.36	12.21	137.20	1.03
14.00	0.42	16.32	11.74	12.36	145.60	1.03
14.50	0.34	16.74	12.17	12.35	151.50	1.02
15.00	0.28	17.17	12.56	12.44	158.80	1.03
15.50	0.23	17.61	13.09	12.23	164.60	1.05
16.00	0.19	18.01	13.44	12.34	170.70	1.06
16.50	0.15	18.42	13.92	12.18	177.10	1.08
17.00	0.13	18.79	14.33	12.06	179.50	1.09
17.50	0.10	19.31	14.95	11.79	184.20	1.11
18.00	0.07	19.82	15.54	11.56	187.40	1.11
18.50	0.06	20.26	16.12	11.17	190.90	1.13
19.00	0.04	20.65	16.84	10.29	184.70	1.12
19.50	0.03	21.28	17.68	9.71	186.80	1.14
20.00	0.02	21.77	18.42	9.06	188.50	1.15
20.50	0.02	22.23	18.91	8.95	191.20	1.16
21.00	0.02	22.41	19.12	8.88	189.40	1.16
21.50	0.01	22.93	19.71	8.72	194.00	1.20
22.00	0.01	23.42	20.24	8.58	195.90	1.25
22.50	0.01	23.73	20.61	8.46	196.10	1.17
23.00	0.00	24.26	21.12	8.47	198.30	1.11
23.50	0.00	24.41	21.40	8.13	199.10	1.10
24.00	0.00	24.98	22.30	7.21	197.80	1.24
24.50	0.00	25.19	22.48	7.32	198.00	1.19
25.00	0.00	25.52	23.13	6.45	197.00	1.29
25.50	0.00	25.84	23.28	6.91	194.00	1.11

**Table C2: Mineral Resource Tonnes at a Series of NSR Cut-off Limits**

Cutoff	Mtonnes	NSR	CU	ZN	AG	AU
0.00	58.31	43.00	2.22	2.89	22.70	0.54
5.00	52.46	47.40	2.46	3.21	25.20	0.55
10.00	44.45	54.70	2.87	3.77	29.70	0.58
15.00	38.88	60.80	3.21	4.26	33.60	0.60
20.00	35.07	65.60	3.47	4.66	37.10	0.63
25.00	31.77	70.10	3.71	5.08	40.60	0.66
30.00	29.04	74.20	3.92	5.46	43.90	0.69
35.00	26.65	78.00	4.12	5.84	47.10	0.71
40.00	24.56	81.50	4.30	6.20	50.10	0.74
45.00	22.62	84.90	4.47	6.55	53.00	0.76
50.00	20.81	88.20	4.64	6.91	55.70	0.78
55.00	19.24	91.10	4.80	7.20	58.20	0.80
60.00	17.75	94.00	4.96	7.46	60.40	0.81
65.00	16.22	97.00	5.12	7.72	62.70	0.83
70.00	14.64	100.30	5.30	7.98	64.90	0.85
75.00	13.01	103.80	5.50	8.25	67.10	0.87
80.00	11.43	107.50	5.72	8.49	68.90	0.89
85.00	9.96	111.30	5.94	8.74	70.60	0.90
90.00	8.51	115.40	6.20	8.95	71.90	0.92
95.00	7.19	119.70	6.47	9.14	73.30	0.92
100.00	5.98	124.30	6.79	9.31	74.90	0.93
105.00	4.91	129.20	7.15	9.38	76.10	0.94
110.00	4.00	134.30	7.53	9.41	77.40	0.93
115.00	3.24	139.50	7.94	9.39	79.20	0.93
120.00	2.66	144.50	8.35	9.37	81.70	0.92
125.00	2.17	149.50	8.76	9.41	84.60	0.92
130.00	1.78	154.60	9.21	9.32	87.10	0.90
135.00	1.45	159.60	9.63	9.33	89.90	0.88
140.00	1.18	164.80	10.05	9.36	93.10	0.88
145.00	0.95	170.30	10.55	9.26	96.50	0.86
150.00	0.78	175.40	11.01	9.20	100.70	0.84
155.00	0.65	180.20	11.39	9.39	107.10	0.84
160.00	0.55	184.30	11.74	9.42	110.70	0.83
165.00	0.47	188.60	12.11	9.39	113.70	0.83
170.00	0.39	192.60	12.49	9.34	117.40	0.83
175.00	0.33	196.40	12.84	9.46	122.70	0.85
180.00	0.27	200.60	13.25	9.41	126.60	0.84
185.00	0.22	205.30	13.71	9.41	132.10	0.86
190.00	0.18	209.30	14.06	9.38	134.60	0.87
195.00	0.14	213.80	14.47	9.26	138.50	0.89
200.00	0.11	218.00	14.85	9.07	138.10	0.88
205.00	0.09	221.80	15.29	8.76	140.80	0.90
210.00	0.07	225.90	15.83	8.47	140.40	0.91
215.00	0.05	230.40	16.23	8.38	142.70	0.93
220.00	0.04	234.80	16.74	8.04	148.20	0.92
225.00	0.03	240.90	17.51	8.55	161.60	1.00
230.00	0.02	244.50	18.01	8.66	169.30	1.04
235.00	0.01	250.50	18.87	8.61	179.00	1.09
240.00	0.01	253.90	19.47	8.34	181.80	1.12
245.00	0.01	258.70	19.87	8.00	177.40	1.14
250.00	0.01	263.70	20.43	8.02	181.40	1.12
255.00	0.00	267.20	20.74	7.92	180.30	1.05
260.00	0.003432	270.00	21.02	7.40	177.50	1.05
265.00	0.002448	273.20	21.36	6.47	165.10	1.09
270.00	0.001521	277.00	22.48	7.32	198.00	1.19
275.00	0.001016	280.50	23.13	6.45	197.00	1.29
280.00	0.000504	284.00	23.28	6.91	194.00	1.11

## APPENDIX D

### RELATIONSHIP BETWEEN NSR AND CUEQ

**Table D1: NSR vs. CuEq Database**

NSR (\$/t ore)	Spec Ore			Non-Spec Ore			Average
	Cu%	Zn%	CuEq %	Cu%	Zn%	CuEq %	CuEq*
5	0.27	0.32	0.27	0.25	0.55	0.25	0.26
10	0.54	0.64	0.54	0.50	1.08	0.50	0.51
15	0.80	0.95	0.80	0.75	1.65	0.75	0.77
20	1.07	1.27	1.07	1.01	2.13	1.01	1.03
25	1.33	1.60	1.33	1.25	2.68	1.25	1.28
30	1.60	1.91	1.60	1.51	3.20	1.51	1.55
35	1.86	2.25	1.86	1.72	3.84	1.72	1.78
40	2.13	2.55	2.13	1.96	4.40	1.96	2.03
45	2.39	2.90	2.39	2.21	4.95	2.21	2.28
50	2.67	3.17	2.67	2.48	5.43	2.48	2.56
55	2.93	3.52	2.93	2.75	5.91	2.75	2.82
60	3.20	3.82	3.20	2.98	6.50	2.98	3.07
65	3.47	4.12	3.47	3.25	7.00	3.25	3.34
70	3.74	4.45	3.74	3.53	7.44	3.53	3.61
75	4.00	4.77	4.00	3.77	8.01	3.77	3.86
80	4.27	5.08	4.27	4.00	8.60	4.00	4.11
85	4.54	5.38	4.54	4.26	9.11	4.26	4.37
90	4.80	5.72	4.80	4.51	9.65	4.51	4.63
95	5.07	6.03	5.07	4.79	10.11	4.79	4.90
100	5.34	6.34	5.34	5.01	10.72	5.01	5.14

\*Average CuEq% calculated by assuming 60% of ore mined is non-spec and 40% mined is spec ore as per the 2006 Five Milling Plan.

CuEq for Spec Ore =  $Cu\% + 0.28 * Zn\%$   
 CuEq for Non-Spec Ore =  $Cu\% + 0.38 * Zn\%$

**APPENDIX E**

**COPPER AND ZINC PRICES SINCE 1990**

**Table E1: Copper Prices**

LME Cu Cash Monthly Averages FROM 1990											
Month	c/lb	\$/mt	Month	c/lb	\$/mt	Month	c/lb	\$/mt	Month	c/lb	\$/mt
Jan'90	107.30	2,365.56	May'94	97.55	2,150.60	Sep'98	74.74	1,647.64	Jan'03	74.74	1,647.66
Feb'90	107.10	2,361.15	Jun'94	107.24	2,364.20	Oct'98	71.96	1,586.39	Feb'03	76.38	1,683.80
Mar'90	119.00	2,623.50	Jul'94	111.50	2,458.19	Nov'98	71.39	1,573.95	Mar'03	75.25	1,658.98
Apr'90	121.90	2,687.43	Aug'94	109.15	2,406.23	Dec'98	66.84	1,473.57	Apr'03	72.01	1,587.48
May'90	124.30	2,740.34	Sep'94	113.67	2,505.93	Jan'99	64.92	1,431.18	May'03	74.76	1,648.28
Jun'90	117.10	2,581.61	Oct'94	115.56	2,547.67	Feb'99	63.99	1,410.78	Jun'03	76.50	1,686.50
Jul'90	125.50	2,766.80	Nov'94	127.12	2,802.45	Mar'99	62.52	1,378.35	Jul'03	77.56	1,710.00
Aug'90	133.90	2,951.99	Dec'94	135.41	2,985.30	Apr'99	66.50	1,466.00	Aug'03	79.85	1,760.28
Sep'90	137.40	3,029.15	Jan'95	136.48	3,008.93	May'99	68.55	1,511.16	Sep'03	81.17	1,789.52
Oct'90	124.40	2,742.55	Feb'95	130.53	2,877.65	Jun'99	64.52	1,422.48	Oct'03	87.11	1,920.54
Nov'90	117.30	2,586.02	Mar'95	132.63	2,924.04	Jul'99	74.39	1,640.00	Nov'03	93.23	2,055.43
Dec'90	113.00	2,491.22	Apr'95	131.70	2,903.50	Aug'99	74.73	1,647.62	Dec'03	99.85	2,201.29
Jan'91	111.00	2,447.13	May'95	125.80	2,773.31	Sep'99	79.39	1,750.34	Jan'04	109.93	2,423.57
Feb'91	110.90	2,444.92	Jun'95	135.83	2,994.64	Oct'99	78.20	1,724.12	Feb'04	125.17	2,759.53
Mar'91	109.60	2,416.26	Jul'95	139.51	3,075.67	Nov'99	78.36	1,727.55	Mar'04	136.47	3,008.72
Apr'91	112.00	2,469.17	Aug'95	137.75	3,036.84	Dec'99	80.05	1,764.75	Apr'04	133.75	2,948.73
May'91	107.70	2,374.38	Sep'95	132.25	2,915.52	Jan'00	83.64	1,843.98	May'04	123.99	2,733.50
Jun'91	100.50	2,215.64	Oct'95	127.62	2,813.55	Feb'00	81.68	1,800.83	Jun'04	121.87	2,686.70
Jul'91	101.20	2,231.08	Nov'95	135.05	2,977.36	Mar'00	78.90	1,739.39	Jul'04	127.39	2,808.43
Aug'91	101.20	2,231.08	Dec'95	132.73	2,926.26	Apr'00	76.15	1,678.75	Aug'04	129.10	2,846.10
Sep'91	105.30	2,321.46	Jan'96	118.68	2,616.41	May'00	80.99	1,785.62	Sep'04	131.31	2,894.86
Oct'91	107.10	2,361.15	Feb'96	115.11	2,537.71	Jun'00	79.52	1,753.18	Oct'04	136.63	3,012.24
Nov'91	107.80	2,376.58	Mar'96	116.17	2,561.02	Jul'00	81.62	1,799.36	Nov'04	141.65	3,122.80
Dec'91	100.40	2,213.44	Apr'96	117.74	2,595.78	Aug'00	84.18	1,855.86	Dec'04	142.68	3,145.45
Jan'92	97.10	2,140.69	May'96	120.58	2,658.26	Sep'00	88.92	1,960.40	Jan'05	143.79	3,170.00
Feb'92	100.00	2,204.62	Jun'96	98.58	2,173.40	Oct'00	86.12	1,898.59	Feb'05	147.59	3,253.70
Mar'92	101.10	2,228.87	Jul'96	90.06	1,985.57	Nov'00	81.42	1,795.11	Mar'05	153.30	3,379.60
Apr'92	100.50	2,215.64	Aug'96	91.11	2,008.57	Dec'00	83.94	1,850.55	Apr'05	153.97	3,394.48
May'92	100.60	2,217.85	Sep'96	88.06	1,941.45	Jan'01	81.08	1,787.50	May'05	147.38	3,249.10
Jun'92	104.20	2,297.21	Oct'96	88.96	1,961.17	Feb'01	80.09	1,765.65	Jun'05	159.85	3,524.07
Jul'92	114.40	2,522.09	Nov'96	101.19	2,230.86	Mar'01	78.87	1,738.77	Jul'05	163.94	3,614.21
Aug'92	114.00	2,513.27	Dec'96	102.88	2,268.08	Apr'01	75.49	1,664.16	Aug'05	172.26	3,797.75
Sep'92	109.80	2,420.67	Jan'97	110.45	2,434.93	May'01	76.30	1,682.21	Sep'05	174.99	3,857.84
Oct'92	102.20	2,253.12	Feb'97	109.13	2,405.85	Jun'01	72.96	1,608.45	Oct'05	184.15	4,059.76
Nov'92	97.90	2,158.32	Mar'97	109.13	2,421.29	Jul'01	69.18	1,525.20	Nov'05	193.65	4,269.34
Dec'92	100.20	2,209.03	Apr'97	108.46	2,391.18	Aug'01	66.43	1,464.43	Dec'05	207.60	4,576.78
Jan'93	102.40	2,257.53	May'97	114.05	2,514.33	Sep'01	64.70	1,426.33	Jan'06	214.75	4,734.33
Feb'93	100.40	2,213.44	Jun'97	118.51	2,612.62	Oct'01	62.47	1,377.28	Feb'06	226.00	4,982.40
Mar'93	97.60	2,151.71	Jul'97	111.15	2,450.46	Nov'01	64.76	1,427.73	Mar'06	231.46	5,102.85
Apr'93	88.50	1,951.09	Aug'97	102.11	2,251.20	Dec'01	66.76	1,471.74	Apr'06	289.75	6,387.78
May'93	81.40	1,794.56	Sep'97	95.59	2,107.30	Jan'02	68.22	1,503.95	May'06	364.95	8,045.86
Jun'93	84.10	1,854.09	Oct'97	93.09	2,052.26	Feb'02	70.85	1,561.90	Jun'06	326.48	7,197.61
Jul'93	87.40	1,926.84	Nov'97	86.97	1,917.45	Mar'02	72.80	1,604.88	Jul'06	349.82	7,712.10
Aug'93	88.30	1,946.68	Dec'97	79.94	1,762.33	Apr'02	72.14	1,590.33	Aug'06	349.07	7,695.66
Sep'93	84.50	1,862.90	Jan'98	76.59	1,688.45	May'02	72.38	1,595.68	Sep'06	344.84	7,602.36
Oct'93	74.70	1,646.85	Feb'98	75.51	1,664.80	Jun'02	74.73	1,647.53	Oct'06		
Nov'93	73.90	1,629.21	Mar'98	79.29	1,747.98	Jul'02	72.10	1,589.46	Nov'06		
Dec'93	78.20	1,724.01	Apr'98	81.69	1,800.90	Aug'02	67.11	1,479.55	Dec'06		
Jan'94	81.89	1,805.35	May'98	78.59	1,732.53	Sep'02	67.07	1,478.71	Jan'07		
Feb'94	84.66	1,866.40	Jun'98	75.32	1,660.52	Oct'02	67.30	1,483.76	Feb'07		
Mar'94	86.86	1,914.87	Jul'98	74.89	1,651.04	Nov'02	71.77	1,582.29	Mar'07		
Apr'94	85.36	1,881.82	Aug'98	73.52	1,620.93	Dec'02	72.38	1,595.68	Apr'07		

Table E2: Zinc Prices

LME Zn Cash Monthly Averages FROM 1990											
Month	c/lb	\$/mt	Month	c/lb	\$/mt	Month	c/lb	\$/mt	Month	c/lb	\$/mt
Jan'90	79.90	1,761.49	May'94	43.36	955.93	Sep'98	45.38	1,000.36	Jan'03	35.44	781.41
Feb'90	63.30	1,395.52	Jun'94	43.84	966.57	Oct'98	42.66	940.48	Feb'03	35.61	785.15
Mar'90	75.60	1,666.69	Jul'94	43.75	964.40	Nov'98	43.87	967.12	Mar'03	35.88	790.95
Apr'90	76.50	1,686.53	Aug'94	42.88	945.34	Dec'98	43.51	959.19	Apr'03	34.23	754.65
May'90	80.60	1,776.92	Sep'94	45.03	992.80	Jan'99	42.31	932.75	May'03	35.18	775.65
Jun'90	77.80	1,715.19	Oct'94	48.03	1,058.90	Feb'99	46.15	1,017.33	Jun'03	35.87	790.69
Jul'90	74.30	1,638.03	Nov'94	52.26	1,152.05	Mar'99	46.72	1,030.00	Jul'03	37.54	827.54
Aug'90	73.30	1,615.99	Dec'94	50.57	1,114.78	Apr'99	46.22	1,019.00	Aug'03	37.10	817.88
Sep'90	69.80	1,538.83	Jan'95	52.47	1,156.86	May'99	47.21	1,040.74	Sep'03	37.11	818.18
Oct'90	61.40	1,353.64	Feb'95	46.84	1,032.60	Jun'99	45.38	1,000.48	Oct'03	40.73	897.96
Nov'90	58.00	1,278.68	Mar'95	46.39	1,022.61	Jul'99	48.63	1,072.14	Nov'03	41.48	914.53
Dec'90	57.40	1,265.45	Apr'95	48.16	1,061.83	Aug'99	51.28	1,130.60	Dec'03	44.35	977.76
Jan'91	54.70	1,205.93	May'95	47.02	1,036.55	Sep'99	54.15	1,193.75	Jan'04	46.13	1,017.00
Feb'91	53.90	1,188.29	Jun'95	45.82	1,010.12	Oct'99	52.11	1,148.74	Feb'04	49.34	1,087.68
Mar'91	54.40	1,199.31	Jul'95	46.59	1,027.07	Nov'99	52.03	1,147.16	Mar'04	50.16	1,105.78
Apr'91	57.00	1,256.63	Aug'95	46.03	1,014.77	Dec'99	53.69	1,183.75	Apr'04	46.84	1,032.73
May'91	49.50	1,091.29	Sep'95	44.75	986.57	Jan'00	53.47	1,178.80	May'04	46.64	1,028.29
Jun'91	48.20	1,062.63	Oct'95	44.43	979.50	Feb'00	49.66	1,094.88	Jun'04	46.33	1,021.45
Jul'91	48.20	1,062.63	Nov'95	46.77	1,031.02	Mar'00	50.64	1,116.35	Jul'04	44.83	988.32
Aug'91	47.50	1,047.20	Dec'95	46.20	1,018.45	Apr'00	51.15	1,127.64	Aug'04	44.26	975.81
Sep'91	46.40	1,022.94	Jan'96	46.24	1,019.39	May'00	52.47	1,156.83	Sep'04	44.23	975.18
Oct'91	45.00	992.08	Feb'96	47.00	1,036.17	Jun'00	50.71	1,117.93	Oct'04	48.31	1,064.95
Nov'91	49.60	1,093.49	Mar'96	48.28	1,064.29	Jul'00	51.54	1,136.21	Nov'04	49.70	1,095.64
Dec'91	53.90	1,188.29	Apr'96	47.43	1,045.73	Aug'00	53.06	1,169.80	Dec'04	53.53	1,180.21
Jan'92	52.40	1,155.22	May'96	47.00	1,036.14	Sep'00	55.54	1,224.40	Jan'05	56.54	1,246.38
Feb'92	51.30	1,130.97	Jun'96	45.76	1,008.85	Oct'00	49.71	1,095.86	Feb'05	60.16	1,326.18
Mar'92	55.00	1,212.54	Jul'96	45.38	1,000.39	Nov'00	48.04	1,059.05	Mar'05	62.49	1,377.69
Apr'92	59.20	1,305.14	Aug'96	45.69	1,007.24	Dec'00	47.91	1,059.79	Apr'05	58.97	1,300.14
May'92	62.30	1,373.48	Sep'96	45.39	1,000.64	Jan'01	46.87	1,033.36	May'05	56.41	1,243.63
Jun'92	62.90	1,386.71	Oct'96	45.52	1,003.46	Feb'01	46.31	1,020.88	Jun'05	57.87	1,275.73
Jul'92	59.90	1,320.57	Nov'96	47.48	1,046.83	Mar'01	45.57	1,004.73	Jul'05	54.18	1,194.43
Aug'92	61.70	1,360.25	Dec'96	47.02	1,036.63	Apr'01	43.97	969.45	Aug'05	58.89	1,298.39
Sep'92	62.00	1,366.86	Jan'97	49.30	1,086.91	May'01	42.55	937.95	Sep'05	63.39	1,397.52
Oct'92	52.80	1,164.04	Feb'97	53.51	1,179.75	Jun'01	40.59	894.93	Oct'05	67.51	1,488.38
Nov'92	47.50	1,047.20	Mar'97	56.94	1,255.24	Jul'01	38.67	852.41	Nov'05	73.07	1,610.93
Dec'92	48.00	1,058.22	Apr'97	56.28	1,240.75	Aug'01	37.56	828.07	Dec'05	82.27	1,813.69
Jan'93	48.10	1,060.42	May'97	59.46	1,310.93	Sep'01	36.22	798.55	Jan'06	94.81	2,090.31
Feb'93	48.80	1,075.86	Jun'97	61.44	1,354.52	Oct'01	34.54	761.50	Feb'06	100.67	2,219.38
Mar'93	45.20	996.49	Jul'97	68.90	1,518.89	Nov'01	35.06	772.91	Mar'06	109.63	2,416.91
Apr'93	45.60	1,005.31	Aug'97	75.04	1,654.40	Dec'01	34.23	754.68	Apr'06	139.92	3,084.78
May'93	44.50	981.06	Sep'97	74.47	1,641.73	Jan'02	35.98	793.23	May'06	161.74	3,565.69
Jun'93	42.00	925.94	Oct'97	58.09	1,280.59	Feb'02	34.98	771.25	Jun'06	146.31	3,225.68
Jul'93	42.10	928.15	Nov'97	53.22	1,173.35	Mar'02	37.16	819.30	Jul'06	151.49	3,339.86
Aug'93	40.10	884.05	Dec'97	50.00	1,102.19	Apr'02	36.66	808.17	Aug'06	151.83	3,347.30
Sep'93	39.70	875.23	Jan'98	49.77	1,097.20	May'02	34.91	769.55	Sep'06	154.36	3,403.02
Oct'93	41.50	914.92	Feb'98	47.36	1,044.00	Jun'02	34.79	767.08	Oct'06		
Nov'93	42.10	928.15	Mar'98	47.52	1,047.64	Jul'02	36.05	794.85	Nov'06		
Dec'93	44.20	974.44	Apr'98	49.76	1,096.95	Aug'02	33.91	747.60	Dec'06		
Jan'94	45.23	997.05	May'98	48.13	1,061.11	Sep'02	34.30	756.24	Jan'07		
Feb'94	43.96	969.20	Jun'98	45.81	1,009.82	Oct'02	34.23	754.67	Feb'07		
Mar'94	42.47	936.22	Jul'98	47.19	1,040.26	Nov'02	34.71	765.26	Mar'07		
Apr'94	41.91	924.03	Aug'98	46.71	1,029.80	Dec'02	36.19	797.74	Apr'07		

**APPENDIX F**

**DILUTION AND ORE LOSS/RECOVERY CALCULATIONS**

**Table F1: Dilution / Ore Loss Calculations in 2005**

DILUTION / ORE LOSS CALCULATIONS IN 2005									
MONTH / YEAR	Stope Name	Stope Type	Planned Solid (tonnes)	Surveyed (CMS) Solid (tonnes)	Difference (tonnes)	Outerwaste Mined (tonnes)	Undermining (Ore Loss) (tonnes)	Dilution %	Ore Loss %
01/05	S820 N07	BS	3,700	5,200	1,500	272	486	5.23	13.14
01/05	S880 N06-PART 2	BS	7,650	17,109	9,459	2,157	1,068	12.61	13.96
01/05	S880 N16	BS	4,900	9,930	5,030	1,322	535	13.31	10.92
01/05	S880 N21-PART 1	P	5,400	6,645	1,245		1,706		31.59
01/05	S880 S10	BS	4,600	7,661	3,061	101	208	1.32	4.52
01/05	S920 C06	P	9,800	9,560	-240				2.23
01/05	S920 N26	P	2,700	5,684	2,984	49	89	0.86	3.30
01/05	S960 CDN-PART 4	T	6,100	10,043	3,943	0		0.00	
	<b>SUB-TOTAL</b>		<b>44,850</b>	<b>71,832</b>	<b>26,982</b>	<b>3,901</b>	<b>4,311</b>	<b>7.01</b>	<b>9.61</b>
02/05	S820 HWS (S21-S20)	T	3,070	660	-2,410	0		0.00	
02/05	S840 S13	P	3,495	3,523	28		151		4.32
02/05	S880 FOG	S	2,000	4,425	2,425	516		11.66	
02/05	S920 C02E	P	6,425	6,030	-395		386		6.01
02/05	S940 C06-PART 1	P	6,100	9,085	2,985		425		6.97
02/05	S980 N12	P	7,358	9,512	2,154	32	431	0.34	5.86
	<b>SUB-TOTAL</b>		<b>28,448</b>	<b>33,235</b>	<b>4,787</b>	<b>548</b>	<b>1,393</b>	<b>3.75</b>	<b>4.90</b>
03/05	S820 N13	BS	3,000	2,871	-129	2	243	0.07	8.10
03/05	S820 S07-PART 1	BS	3,500	3,875	375				
03/05	S820 S19	P	2,500	2,130	-370		355		14.20
03/05	S880 N04-PART 1	BS	6,000	9,188	3,188	285	12	3.10	0.20
03/05	S880 N19-PART 2	P	2,590	2,314	-276	79		3.41	
03/05	S880 S15	BP	6,300	8,199	1,899				
03/05	S900 N21-PART 1	BS	1,300	1,778	478	5	437	0.28	33.62
03/05	S920 N23E	BS	3,400	2,924	-476	78	326	2.67	9.59
03/05	S980 N07	BP	5,300	5,389	89		346		6.53
03/05	S900 HWS	T	1,300	3,361	2,061	0	333	0.00	25.62
03/05	S900 CDN DUMP	T	1,000	1,834	834	120		6.54	
	<b>SUB-TOTAL</b>		<b>36,190</b>	<b>43,863</b>	<b>7,673</b>	<b>569</b>	<b>2,052</b>	<b>2.34</b>	<b>5.67</b>
04/05	S820 S10	BS	4,100	4,000	-100	175	372	4.38	9.07
04/05	S860 N23-PART 1	P	4,262	4,000	-262		293		6.87
04/05	S860 N25	P	2,250	3,293	1,043				
04/05	S880 S19	BP	5,210	4,325	-885		797		15.30
04/05	S900 CDN 20E	P	5,300	3,579	-1,721		2,153		40.62
04/05	S940 C02	P	9,500	7,979	-1,521		568		5.98
04/05	S960 CDN-PART 5	T	6,000	6,000		0		0.00	
	<b>SUB-TOTAL</b>		<b>36,622</b>	<b>33,176</b>	<b>-3,446</b>	<b>175</b>	<b>4,183</b>	<b>1.75</b>	<b>11.42</b>
05/05	S1040 S01	BP	3,987	4,578	591		657		16.48
05/05	S820 S17	P	3,600	3,147	-453		575		15.97
05/05	S860 N18	S	8,800	9,314	514	325	950	3.49	10.80
05/05	S860 N23	P	7,800	8,739	939		874		11.21
05/05	S860 S13	BP	4,047	4,503	456		605		14.95
05/05	S900 HWNW (N10-N11)	T	5,200	2,900	-2,300	0		0.00	
05/05	S900 HWNE (N22-N21)	T	8,000	7,768	-232	221	1,143	2.85	14.29
05/05	S940 C06-PART 2	P	3,600	3,313	-287				
05/05	S980 N11	BS	6,800	7,847	1,047	994	748	12.67	11.00
	<b>SUB-TOTAL</b>		<b>51,834</b>	<b>52,109</b>	<b>275</b>	<b>1,540</b>	<b>5,552</b>	<b>5.53</b>	<b>10.71</b>
06/05	S820 HWN (N12-N11)	T	5,242	3,486	-1,756	0	529	0.00	10.09
06/05	S820 HWS (S19-S20)	T	1,850	2,441	591	0	517	0.00	27.95
06/05	S860 N23-PART 2	P	3,100	5,218	2,118				
06/05	S880 S13-PART 1	BP	2,400	4,583	2,183				
06/05	S900 HWNE(N20-N19)	T	5,250	8,703	3,453	654	550	7.51	10.48
06/05	S900 HWNE(N11-N12)	T	5,200	2,900	-2,300	0		0.00	
06/05	S900 HWS (S25-S23)	T	8,500	8,087	-413	0	550	0.00	6.47
	<b>SUB-TOTAL</b>		<b>31,542</b>	<b>35,418</b>	<b>3,876</b>	<b>654</b>	<b>2,146</b>	<b>2.55</b>	<b>6.80</b>

**Table F1: Dilution / Ore Loss Calculations in 2005 (Continued)**

DILUTION / ORE LOSS CALCULATIONS IN 2005									
MONTH / YEAR	Stope Name	Stope Type	Planned Solid (tonnes)	Surveyed (CMS) Solid (tonnes)	Difference (tonnes)	Outerwaste Mined (tonnes)	Undermining (Ore Loss) (tonnes)	Dilution %	Ore Loss %
07/05	S820 S12	P	2,250	2,366	116		432		19.20
07/05	S880 N21-PART 2	P	3,100	4,628	1,528				
07/05	S900 HWNE(N17-N18)	T	5,180	5,999	819	60	1,544	1.00	29.81
07/05	S900 HWNW (N07-N08)	T	1,831	1,818	-13	0	370	0.00	20.21
07/05	S920 C04	P	7,900	11,762	3,862				
07/05	S920 S01	P	7,405	9,425	2,020		216		2.92
07/05	S960 C02	P	8,100	10,482	2,382		300		3.70
	<b>SUB-TOTAL</b>		<b>35,766</b>	<b>46,480</b>	<b>10,714</b>	<b>60</b>	<b>2,862</b>	<b>0.77</b>	<b>8.00</b>
08/05	S1040 N1640	S	7,432	7,208	-224	109	1,397	1.51	18.80
08/05	S840 HWS	T	1,433	1,784	351				
08/05	S880 HWS (S23-S21)	T	5,365	8,174	2,809		1,175		21.90
08/05	S900 N19W-PART 1	BS	4,361	6,154	1,793	466	706	7.57	16.19
08/05	S920 C07-PART 1	S	8,000	9,143	1,143	262	1,177	2.87	14.71
08/05	S960 C06-PART 1	BP	6,650	9,074	2,424		181		2.72
08/05	S880 N23-PART 1	BP	4,922	5,569	647				
	<b>SUB-TOTAL</b>		<b>38,163</b>	<b>47,106</b>	<b>8,943</b>	<b>837</b>	<b>4,636</b>	<b>3.72</b>	<b>12.15</b>
09/05	S775 N08	P	8,976	11,661	2,685		235		2.62
09/05	S840 S12	S	8,600	12,613	4,013	327	734	2.59	8.53
09/05	S880 S13-PART 2	BP	3,856	4,569	713		194		5.03
09/05	S920 CDN (N21-N19)	T	5,106	6,926	1,820	35	478	0.51	9.36
09/05	S940 S01	P	6,000	10,928	4,928	0	93	0.00	1.55
09/05	S980 N08	BS	4,227	5,369	1,142	224	149	4.17	3.52
	<b>SUB-TOTAL</b>		<b>36,765</b>	<b>52,066</b>	<b>15,301</b>	<b>586</b>	<b>1,883</b>	<b>1.64</b>	<b>5.12</b>
10/05	S820 HWN (N10-N09)	T	4,121	5,579	1,458	421	129	7.55	3.13
10/05	S840 S17	BP	1,700	2,684	984		299		17.59
10/05	S860 N20	S	5,480	9,116	3,636	1,155	450	12.67	8.21
10/05	S880 S20	BS	4,570	5,021	451	260	110	5.18	2.41
10/05	S900 CDN (N21-N19)	T	3,385	8,035	4,650	1,688		21.01	
10/05	S920 C07-PART 2	S	4,296	8,713	4,417	278	66	3.19	1.54
10/05	S960 C06-PART 2	BP	4,605	10,491	5,886	145	304	1.38	6.60
	<b>SUB-TOTAL</b>		<b>28,157</b>	<b>49,639</b>	<b>21,482</b>	<b>3,947</b>	<b>1,358</b>	<b>8.41</b>	<b>4.82</b>
11/05	S775 N10	P	6,150	9,527	3,377		25		0.41
11/05	S840 S14	S	6,800	9,579	2,779	0		0.00	
11/05	S880 S17	BP	4,397	3,790	-607	0	532	0.00	12.10
11/05	S900 HWNW (N05-N06)	BT	3,274	3,925	651	0	0	0.00	
11/05	S900 N19-PART 2	BS	1,065	1,913	848	100	100	5.23	9.39
	<b>SUB-TOTAL</b>		<b>21,686</b>	<b>28,734</b>	<b>7,048</b>	<b>100</b>	<b>657</b>	<b>0.52</b>	<b>3.03</b>
12/05	S860 S12	S	9,200	15,906	6,706	920		5.78	
12/05	S880 N25-PART 1	BP	5,500	9,950	4,450				
12/05	S900 S02-PART 1	S	3,150	3,449	299	214	511	6.20	16.22
12/05	S920 CDN (N18-N17)	T	6,043	9,250	3,207				
12/05	S960 S01	BP	7,402	12,477	5,075				
	<b>SUB-TOTAL</b>		<b>31,295</b>	<b>51,032</b>	<b>19,737</b>	<b>1,134</b>	<b>511</b>	<b>5.86</b>	<b>1.63</b>

DILUTION AND RECOVERY/ORE LOSS SUMMARY IN 2005 MINE PRODUCTION			
DILUTION		RECOVERY/ORE LOSS	
Total Surveyed Stope Tonnage :	309,615 t	Total Planned Stope Tonnage :	421,318 t
Total Outer Waste Mined Tonnage :	14,051 t	Total Ore Loss Tonnage :	31,544 t
Dilution % :	4.54	Ore Loss % :	7.49
		Ore Recovery % :	92.51

**Note 1: Dilution and Ore Loss calculations are based on the formulas below.**

$$\text{Ore Loss \%} = \text{Undermining} / \text{Planned} * 100$$

$$\text{Dilution \%} = \text{Outer waste} / \text{Surveyed} * 100$$

**Note 2: For overall calculations, dilution calculations done for all secondary and tertiary stopes and some primary stopes where waste mined tonnage calculations available.**

**Table F2: Dilution / Ore Loss Calculations in 2006 (for the first 6 months)**

DILUTION / ORE LOSS CALCULATIONS IN 2006 (6 MONTH)									
MONTH / YEAR	Stope Name	Stope Type	Planned Solid (tonnes)	Surveyed (CMS) Solid (tonnes)	Difference (tonnes)	Outerwaste Mined (tonnes)	Undermining (Ore Loss) (tonnes)	Dilution %	Ore Loss %
01/05	S1040 N1650	S	7,649	10,714	3,065	349	532	3.26	6.96
01/05	S790 N08	P	4,800	8,322	3,522		112		2.33
01/05	S900 CDN (N18-N17)	T	3,200	7,874	4,674	501		6.36	
01/05	S880 N18	BS	6,850	11,212	4,362	1,017	27	9.07	0.39
01/05	S900 S22	BS	7,068	5,461	-1,607				
01/05	S940 C04-PART 1	P	6,500	11,515	5,015		4		0.06
01/05	S940 C07-PART 1	S	6,000	5,041	-959	24	115	0.48	1.92
01/05									
	<b>SUB-TOTAL</b>		<b>42,067</b>	<b>60,139</b>	<b>18,072</b>	<b>1,891</b>	<b>790</b>	<b>5.43</b>	<b>1.88</b>
02/05	S775 N06	P	8,750	11,087	2,337		437		4.99
02/05	S790 N10	P	7,400	8,460	1,060		270		3.65
02/05	S820 S18	S	5,000	6,131	1,131	210	293	3.43	5.86
02/05	S880 N25-PART 2	BP	1,680	2,416	736		109		6.49
02/05	S880 S18	BS	3,250	4,457	1,207	139	62	3.12	1.91
02/05	S940 CDN (N18-N17)	BT	4,600	4,842	242	6	1,170	0.12	25.43
	<b>SUB-TOTAL</b>		<b>42,701</b>	<b>50,495</b>	<b>7,794</b>	<b>1,712</b>	<b>2,341</b>	<b>8.15</b>	<b>5.48</b>
03/05	S820 HWN (N08-N07)	T	4,600	7,811	3,211	650		8.32	
03/05	S880 S12	BS	8,400	14,572	6,172	1,114		7.64	
03/05	S900 CDN14E	BS	4,900	7,456	2,556	2,345		31.45	
03/05	S940 C07-PART 2	S	6,800	16,672	9,872	3,276		19.65	
03/05	S880 N20	BS	7,000	7,667	667	2,341	673	30.53	9.61
03/05	S900 S02-PART 2	BS	2,197	2,197		81		3.69	
	<b>SUB-TOTAL</b>		<b>33,897</b>	<b>56,375</b>	<b>22,478</b>	<b>9,807</b>	<b>673</b>	<b>17.40</b>	<b>1.99</b>
04/05	S775 N04	P	9,800	11,231	1,431		360		3.67
04/05	S820 S16	S	4,100	4,242	142	80	384	1.89	9.37
04/05	S880 N04-PART 2	BS	6,750	8,835	2,085	513	165	5.81	2.44
04/05	S900 HWNW (N12-N13)	BT	1,841	3,224	1,383	10	203	0.31	11.03
04/05	S960 C04-PART 1	P	4,100	9,517	5,417				
04/05	S900 S22-PART 2	BS	3,000	5,500	2,500				
	<b>SUB-TOTAL</b>		<b>29,591</b>	<b>42,549</b>	<b>12,958</b>	<b>603</b>	<b>1,112</b>	<b>3.70</b>	<b>3.76</b>
05/05	S775 N09	S	8,907	11,116	2,209	700	388	6.30	4.36
05/05	S800 N10	BP	3,500	3,183	-317		375		10.71
05/05	S840 S18-PART 1	S	5,582	5,696	114		200		3.58
05/05	S880 N23-PART 2	BP	2,750	2,663	-87				
05/05	S900 CDN14-PART 2	BS	4,300	8,965	4,665	800	477	8.92	11.09
05/05	S920 S02-PART 1	BS	7,300	6,722	-578	90	883	1.34	12.10
05/05	S940 C04-PART 2	S	2,500	7,104	4,604	140	461	1.97	18.44
05/05	S960 C07-PART 1	BS	8,100	7,104	-996	77	2,066	1.08	25.51
05/05	S880 S14-PART 1	BS	3,900	5,505	1,605	192		3.49	
	<b>SUB-TOTAL</b>		<b>46,839</b>	<b>58,058</b>	<b>11,219</b>	<b>1,999</b>	<b>4,850</b>	<b>4.30</b>	<b>10.35</b>
06/05	S775 N12	P	3,300	5,928	2,628		209		6.33
06/05	S880 N25-PART 3	P	4,300	6,131	1,831		359		8.35
06/05	S900 CDN08-PART 1	BS	3,907	4,919	1,012	490	335	9.96	8.57
06/05	S900 HWNW (N04-N03)	BT	4,900	4,750	-150	4		0.08	
06/05	S920 C01	S	9,200	11,920	2,720	718	326	6.02	3.54
06/05	S920 CDN (N14-N13)	T	6,800	10,007	3,207	774	410	7.73	6.03
06/05	S960 C04-PART 2	P	3,400	4,905	1,505		61		1.79
	<b>SUB-TOTAL</b>		<b>35,807</b>	<b>48,560</b>	<b>12,753</b>	<b>1,986</b>	<b>1,700</b>	<b>6.29</b>	<b>4.75</b>

DILUTION AND RECOVERY/ORE LOSS SUMMARY IN 2006 MINE PRODUCTION	
DILUTION	RECOVERY/ORE LOSS
Total Surveyed Stope Tonnage : 206,644 t	Total Planned Stope Tonnage : 230,902 t
Total Outer Waste Mined Tonnage : 17,998 t	Total Ore Loss Tonnage : 11,466 t
Dilution % : 8.71	Ore Loss % : 4.97
	Ore Recovery % : 95.03

**Note 1: For overall calculations, dilution calculations done for all secondary and tertiary stopes and some primary stopes where waste mined tonnage calculations available.**